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Investigating the influence of diffusional coupling on mixture permeation across porous membranes

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ABSTRACT

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Keywords: Maxwell-Stefan diffusion Correlations Zeolites Metal-organic frameworks Membrane permeation Pervaporation Hydrogen bonding A careful analysis of published experimental data on permeation of a variety of binary mixtures reveals that there are fundamentally two types of diffusional coupling effects that need to be recognized. The first type of coupling occurs when the less-mobile species slows down its more mobile partner by not vacating an adsorption site quick enough for its more mobile partner to occupy that position. Such slowing-down effects, also termed correlation effects, are quantified by the exchange coefficient D_{12} in the Maxwell–Stefan (M–S) formulation. The parameter D_1/D_{12} , quantifying the degree of correlations, is strongly dependent on the pore size, topology and connectivity and reasonable estimates are provided by molecular dynamics (MD) simulations. In cage-type structures (e.g. CHA, DDR, LTA, and ZIF-8) in which adjacent cages are separated by narrow windows correlations are weak, and $D_1/D_{12} \approx 0$ is a good approximation. On the other hand correlations are particularly strong in structures consisting of one-dimensional channels (e.g. NiMOF-74), or intersecting channels (e.g. MFI) structures; in these cases the values of D_1/D_{12} are in the range 1–5. A wide variety of experimental data on binary mixture permeation can be quantitatively modeled with the Maxwell-Stefan equations using data inputs based on unary permeation experiments, along with D_1/D_{12} values suggested by MD. The second type of coupling occurs as a consequence of molecular clustering due to hydrogen bonding. Such clustering effects, commonly prevalent in alcohol/water pervaporation, can cause mutual slowing-down of partner molecules in the mixture. When molecular clustering occurs the Maxwell–Stefan diffusivity of a species in the mixture, D_i , cannot be identified with that obtained from unary permeation.

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1. Introduction

The proper description of permeation of mixtures across porous membranes consisting of thin layers of ordered crystalline materials such as zeolites (crystalline aluminosilicates), metal-organic frameworks (MOFs), and zeolitic imidazolate frameworks (ZIFs) is important in development and design of a variety of industrially important separation processes, such as CO_2 capture, natural gas purification, fuel gas purification and pervaporation [1–8]. For separation of a binary mixture, the permeation selectivity, S_{perm} , is commonly defined as the ratio of the component permeances across the porous layer

$$S_{\text{perm}} = \frac{\Pi_1}{\Pi_2} = \frac{N_1 / \Delta p_1}{N_2 / \Delta p_2}$$
 (1)

where the fluxes N_i , are defined in terms of the cross-sectional area of the membrane (see schematic in Fig. 1). The Maxwell–Stefan

(M–S) formulation for mixture diffusion is most commonly used for modeling membrane permeation [5,9–14]. Solution of the M–S equations for steady-state binary mixture permeation results in the following set of equations for the permeation fluxes

$$N_{1} = \frac{\rho D_{1}}{\delta} \left[\frac{(1 + x_{1} D_{2} / D_{12}) \Delta q_{1} + x_{1} D_{2} / D_{12} \Delta q_{2}}{1 + x_{1} D_{2} / D_{12} + x_{2} D_{1} / D_{12}} \right]$$
(2)

and

$$N_{2} = \frac{\rho D_{2}}{\delta} \left[\frac{x_{2} D_{1} / D_{12} \Delta q_{1} + (1 + x_{2} D_{1} / D_{12}) \Delta q_{2}}{1 + x_{1} D_{2} / D_{12} + x_{2} D_{1} / D_{12}} \right]$$
(3)

In the derivations of the Eqs. (2) and (3), details of which are provided in the Supplementary Material accompanying this publication, the resistance of the support layer is ignored. Furthermore, the micro-porous crystalline layer is considered to be defect-free, and inter-grain boundary resistances have not been accounted for.

The molar loadings, q_i , in the adsorbed phase at either face of the membrane are obtained from adsorption equilibrium. In all the calculations presented is this study, the adsorption equilibrium is determined using the Ideal Adsorbed Solution Theory of

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Fig. 1. Schematic of binary mixture permeation across a porous crystalline layer.

Myers and Prausnitz [15], on the basis of pure component isotherm fits. The x_i are the component mole fractions in the adsorbed phase within the membrane

$$x_1 = q_1/(q_1 + q_2); \quad x_2 = q_2/(q_1 + q_2)$$
 (4)

The calculation of x_i using the upstream loadings is sufficiently accurate for the estimation of the permeation fluxes.

There are basically two different types of M–S diffusivities. The D_1 and D_2 characterize the interactions, in the broadest sense, with the pore walls. The D_{12} is the exchange coefficient which quantify diffusional coupling between the two components. At the molecular level, the D_{12} reflect how the facility for transport of species 1 correlates with that of species 2. In subsequent discussions, it is convenient to define the ratio (D_1/D_{12}) as a reflection of the degree of correlations. The diffusional characteristics of the porous crystalline layer is therefore described by three separate independent parameters: (a) the two membrane transport coefficients $\rho D_1/\delta$, and $\rho D_2/\delta$, and (b) the degree of correlations D_1/D_{12} .

In assessing the separation capability of any membrane for a given separation task it is useful to also define the adsorption selectivity, S_{ads} , in terms of the component loadings and partial pressures in the upstream compartment.

$$S_{\rm ads} = \frac{q_{10}/q_{20}}{p_{10}/p_{20}} \tag{5}$$

A further useful metric is the diffusion selectivity of the membrane, $S_{\rm diff}$

$$S_{\text{diff}} = \frac{S_{\text{perm}}}{S_{\text{ads}}} = \frac{D_1 \left(1 + D_2 / D_{12} \right)}{D_2 \left(1 + D_1 / D_{12} \right)}$$
(6)

where the second right member in Eq. (6) is derived for the commonly valid assumption that the downstream partial pressures, and component loadings are negligible in comparison with the corresponding upstream values (detailed derivations are provided in the Supplementary Material). For the special limiting

case for which the degree of correlations is negligible small, Eq. (6) simplifies to yield

$$S_{\text{diff}} = \frac{D_1}{D_2};$$
 negligible correlations (7)

A special distinguishing feature of membrane separations, in contrast to other competitive technologies such as pressure swing adsorption (PSA) devices, is that the permeation selectivity S_{perm} is governed not only by S_{ads} but also by the diffusional characteristics. PSA units are largely, though not exclusively, governed by S_{ads} but membrane-based separations offer the possibility of also exploiting S_{diff} to significantly enhance the obtained value of S_{perm} .

There are three major objectives of the investigations reported here.

The first objective is to identify conditions and systems for which the diffusional coupling effects can be assumed to be of negligible significance. This scenario corresponds to the limiting case in which $(D_1/D_{12}) \rightarrow 0$ and, as a consequence, Eqs. (2) and (3) simplify to yield

$$N_1 = \frac{\rho D_1}{\delta} \Delta q_1; \quad N_2 = \frac{\rho D_2}{\delta} \Delta q_2; \quad \text{negligible correlations}$$
(8)

The second objective is to identify and examine systems for which the correlation effects are significant. In such cases we seek to establish the applicability of M–S Eqs. (2) and (3) in describing mixture permeation characteristics by estimating the membrane transport coefficients $\rho D_1/\delta$, and $\rho D_2/\delta$ from unary permeation data. We aim to show that a clever choice of the membrane material, with the appropriate degree of correlations, will serve to significantly enhance the permeation selectivity.

The third objective is to identify systems for which the $\rho D_1/\delta$, and $\rho D_2/\delta$ characterizing mixture permeation cannot be identified with those obtained from unary permeation.

2. Comparing the degree of correlations in different host materials

There is no experimental technique for direct determination of the exchange coefficients D_{12} , that quantify molecule–molecule interactions. For this reason we use molecular dynamics (MD) simulation data from the literature [13,14,16–19] to obtain the necessary insights and inputs. For convenience, a summary of available MD simulation data, and the interpretation thereof, is provided as Supplementary Material.

For mesoporous materials, such as BTP-COF, the values of the exchange coefficient D_{12} are the nearly the same as the binary fluid phase M–S diffusivity, $D_{12, \text{ fl}}$, over the entire range of pore concentrations. A similar result holds for mesopores in the 20–100 Å size range [20]. Procedures for estimation of the $D_{12, \text{ fl}}$ are available in Poling et al. [21], and therefore this provides a convenient starting point for the estimation of the D_{12} .

For micro-porous materials, the exchange coefficient D_{12} cannot be directly identified with the corresponding fluid phase diffusivity $D_{12, \text{ fl}}$ because the molecule–molecule interactions are also significantly influenced by molecule–wall interactions. This is underscored by MD data for D_{12} for six binary mixtures, with $q_1=q_2$, in a variety of micro-porous hosts; see Fig. 2. For every guest/host combination, at any total mixture pore concentration, $c_t=(q_1+q_2)/V_p$, the D_{12} is lower than the value of $D_{12, \text{ fl}}$. The extent of lowering can be quantified by defining the fraction *F*

$$F \equiv D_{12}/D_{12, \text{ fl}}$$
 (9)

Every guest/host combination can be characterized by a constant fraction *F*, that are determined by data fitting; the complete data sets are available in the Supplementary Material



Fig. 2. The M–S binary exchange coefficients D_{12} , for diffusion of equimolar ($c_1=c_2$) binary mixtures (a) H_2/CH_4 , (b) CH_4/Ar , (c) CH_4/C_2H_6 , (d) CH_4/CO_2 , (e) H_2/CO_2 , and (f) CO_2/N_2 at 300 K in a variety of host materials as a function of the total pore concentration, c_t . The D_{12} , ff or binary fluid phase mixture diffusion, obtained from independent MD simulations, is also presented in square symbols, along with continuous solid lines that represent the fraction *F* times D_{12} , ff The MD data are culled from our previous publications [14,16–20,22,87–91]. A more complete set of data is available in the Supplementary material.

accompanying this publication. For "open" structures, with large pore volumes, V_p , the values of *F* are closer to unity. For example, for CH₄/Ar diffusion in IRMOF-1, COF-102, COF-103, and COF-108, the values are *F*=0.6, 0.65, 0.65, and 0.8, respectively, increasing with increasing pore void fractions, ϕ . Remarkably, for IRMOF-1, the factor *F* is in the narrow range of 0.6–0.7 for every guest mixture investigated.

At the other end of the spectrum, materials with low pore volumes, the values of the fraction F lie significantly below unity. In MFI that has a set of intersecting channels, F lies in the range of 0.1–0.15 for all mixtures. For BEA, also with intersecting

channels, but with a slightly higher pore void fraction, we obtain F=0.2. For materials such as FAU, NaX, NaY, LTA, and MgMOF-74 with intermediate void fractions, the values of F fall in the range 0.3–0.6.

In summary, for micro-porous materials, the D_{12} are lower than the corresponding fluid phase diffusivity $D_{12, \text{ fl}}$ by a factor, *F*, that depends on the pore volume, pore size, and connectivity of the host materials. The stronger the degree of confinement, the smaller is the value of *F* [13,20]. Within the 5.5 Å intersecting channels of MFI zeolite, the D_{12} is about a tenth of the value for the corresponding fluid mixture, when compared at the same total molar concentration $c_t = (q_1 + q_2)/V_p$ within the pores, i.e. $F \approx 0.1$. Within the 1D, 11 Å sized hexagonal-shaped channels of MgMOF-74, and NiMOF-74, the value of F is in the range of 0.4–0.6. For FAU-Si, NaY, and NaX that has 7.4 Å sized windows separating 11 Å sized cages, the values of F are in the range 0.3–0.6. For IRMOF-1, the value of F is in the range of 0.6–0.7.

For the purposes of interpreting experimental data on membrane permeation we need information on the degrees of correlation, D_1/D_{12} . Fig. 3 shows MD data on D_1/D_{12} for diffusion of six

different mixtures in a variety of host materials, expressed as a function of the total concentration, c_t , of the adsorbed mixture within the pores. The use of pore concentrations c_t rather than the molar loadings affords a fairer comparison of different host materials as explained in previous works [20]. For any guest/host combination, D_1/D_{12} is seen to increase as the pore concentration increases; this implies that correlation effects are expected to be stronger for membrane separations operating at higher pressures. The degree of correlations is weakest in cage-type structures such as



Fig. 3. MD simulation data for the degree of correlations, D_1/D_{12} , for diffusion of equimolar binary mixtures ($c_1=c_2$) (a) H_2/CO_2 , (b) CO_2/CH_4 , (c) H_2/CH_4 , (d) CH_4/nC_4H_{10} , (e) CH_4/C_2H_6 , and (f) CH_4/C_3H_8 at 300 K in a variety of host materials, as a function of the total pore concentration, $c_t=(q_1+q_2)/V_p$. As explained in previous works, the comparisons of diffusivities in different host materials is best done in terms of pore concentrations, expressed in terms of the accessible pore volume V_p [20]. A more detailed data set on the D_1/D_{12} is provided as Supplementary Material.

CHA, DDR and LTA; the reason is that the molecules jump one-at-atime across the narrow windows separating adjacent cages. To visualize the inter-cage hopping, video animations of the MD simulations for diffusion of H_2/CO_2 and CH_4/CO_2 mixtures in LTA zeolite is provided as Supplementary Material. These animations also clearly demonstrate that CO_2 molecules jump length-wise across the windows. At the other end of the spectrum, correlations are strongest in one-dimensional (1D) channel structures (e.g. NiMOF-74), intersecting channels (e.g. MFI), and "open" structures (e.g. IRMOF-1, FAU, NaX) consisting of large cages separated by wide windows.

3. Systems with negligible degree of correlations

We first examine mixture permeation across structures such as CHA, DDR, LTA, ITQ-29, SAPO-34, and ZIF-8 that consist of cages separated by narrow windows in the 3.2–4.2 Å range. We shall analyze experimental mixture permeation data to examine whether the uncoupled Eq. (8) is of sufficient accuracy for use in practice.

Consider permeation of CO₂/CH₄ separation using a membrane made up of thin layers of SAPO-34 that consists of 316 Å³ sized cages separated by 3.8 Å × 4.2 Å sized windows. Experimental

data on permeances Π_i of CO₂ and CH₄ determined from unary and binary permeation experiments are compared in Fig. 4a. We note that while the permeance of CO₂ in the mixture remains unchanged from that of the pure component, the permeance of CH₄ in the mixture is lower in the mixture than the pure component value. Consequently, the value of S_{perm} from mixture permeation experiments is higher than those determined from unary permeation; see Fig. 4b. The differences in the two sets S_{perm} values are primarily because the adsorption selectivity, S_{ads} , determined from IAST calculations, is significantly higher for mixture adsorption; Fig. 4b also indicates that the S_{perm} value is significantly higher than the corresponding value of S_{ads} . The rationale is that CO₂ molecules jump length-wise across the windows (see snapshot in Fig. 4c) and have a significantly higher diffusivity than that of CH₄; this is verified by molecular dynamics (MD) simulations for the structural analog CHA [22]. As stressed in the literature [22,23], kinetic diameters are insufficient indicators of the hierarchy of diffusivity values; molecular configurations, bond length and bond angles are also important determinants. Indeed, an important advantage of SAPO-34 in CO₂/CH₄ mixture separation is that the diffusion selectivity favors CO₂; S_{ads} and S_{diff} complement each other. Therefore, SAPO-34 membranes have significant potential for use in natural gas purification applications that operate at high pressures.



Fig. 4. (a) Permeances of CO₂ (1) and CH₄ (2) determined for unary and binary mixture permeation across SAPO-34 membrane [24–26]. (b) Comparison of S_{perm} and S_{ads} values for CO₂/CH₄ mixtures compared with corresponding values determined from unary experiments. (c) Snapshot, obtained from molecular simulation, showing adsorbed CO₂ and CH₄ molecules in SAPO-34. (d) Experimental data on permeances of CO₂ and CH₄ compared with the estimations of Eq. (8). The estimations are based on the values of $\rho D_1 / \delta = 0.035$ kg m⁻² s⁻¹, and $\rho D_2 / \delta = 0.005$ kg m⁻² s⁻¹, both determined from unary permeation data. Further details of the model calculations, including isotherm fits, are provided in the Supplementary Material.

We now attempt quantitative modeling of mixture permeation using uncoupled Eq. (8). For this purpose, the transport coefficients $\rho D_1/\delta$, and $\rho D_2/\delta$, are first determined from unary permeation experiments for conditions corresponding to the lowest upstream pressures. The values thus obtained are subsequently used in the Eq. (8) for estimation of N_i , and Π_i in the mixture. These estimations are in reasonable agreement with the experimental data; see Fig. 4d. More detailed modeling [24–26], accounting rigorously for the loading dependence of the M–S diffusivities, D_1 and D_2 leads to improved agreement between model calculations and experiment, but does not alter the conclusion that correlation effects are of negligible significance in this case and that $(D_1/D_{12}) \rightarrow 0$ is a good assumption to make.

The interpretation of the experimental data on H₂/CO₂ separation with SAPO-34 membrane [26] is somewhat different in detail. The permeance of H₂ in the mixture is considerably lower, by about order of magnitude, than the unary permeance value; see Fig. 5a. This order-of-magnitude decrease in the permeance of H_2 is primarily attributable to the fact that the value of S_{ads} for mixture adsorption is about an order of magnitude higher than S_{ads} calculated from pure component isotherm data; see Fig. 5b. Another point to note is that the Sperm value is significantly lower than the corresponding value of S_{ads} ; this is because S_{diff} favors the significantly smaller H_2 molecule. The S_{ads} and S_{diff} characteristics of H₂/CO₂ mixtures do not complement each other. SAPO-34 membrane is CO₂-selective because the adsorption favors CO₂ and overcomes the diffusional disadvantages. Calculations based on Eq. (8) result in reasonably good agreement with the mixture permeation experiments; see Fig. 5c. A more detailed modeling exercise, based on exact numerical solution of the M-S equations accounting rigorously for the loading dependence of the M-S diffusivities, is available in an earlier publication [26].

The 3.65 Å × 4.4 Å windows of DDR have a more oblong shaped aperture compared to that of SAPO-34. One important consequence is that the window regions of DDR are preferred locations for CO₂ molecules [27]; see snapshot in Fig. 6a. Experimental data [28,29] on component permeances across a DDR membrane shows that the Π_i values in the mixture are nearly the same as for pure components (cf. Fig. 6b and c), implying a negligible degree of correlations, i.e. $(D_1/D_{12}) \rightarrow 0$. Rigorous modeling of the DDR permeation data also reveals that the preferential location of CO₂ at the window regions has the effect of hindering the inter-cage hopping of CH₄ [17,27,30]. One important consequence of such hindering is that the CO₂/CH₄ permeation selectivity with DDR is about 1000, which is significantly higher than that obtained with SAPO-34.

The size of the window aperture of ZIF-8 (see landscape in Fig. 7a) from crystallographic data is 3.26 Å, but the lattice framework flexibility is such that molecules as large as 2,2 dimethylbutane can be transported for one cage (approximately 1170 Å³ in size) to an adjacent cage [23,31,32]. By contrast, lattice flexibility has little influence on the inter-cage hopping across narrow 8-ring windows of CHA, LTA, ITQ-29, SAPO-34, and DDR zeolites [33,34]. Experimental data for Π_i of CO₂ and CH₄ determined for unary and binary mixture permeation experiments [35] are shown in Fig. 7b. We note that the permeance of each component is the practically the same in the mixture as for the pure component, suggesting that diffusional coupling effects are of negligible importance. The lattice flexibility of ZIF-8 is most likely the reason that the CO₂/CH₄ permeation selectivity with ZIF-8 is only in the range of 2–4, significantly lower than S_{perm} values obtained with DDR and SAPO-34.

The transient uptake data of Li et al. [36] for ZIF-8 show propene diffusivity to be 125 times that of propane; the higher alkene diffusivity must be ascribed to subtle differences in bond lengths and bond angles [22,23]. This would suggest that ZIF-8



Upstream partial pressure, pi0/ MPa

Fig. 5. (a) Permeances of H₂ (1) and CO₂ (2) determined for unary and binary mixture permeation across SAPO-34 membrane [26]. (b) Comparison of S_{perm} and S_{ads} values for H₂/CO₂ mixtures compared with corresponding unary values. (c) Experimental data on permeances of H₂ and CO₂ compared with the estimations of Eq. (8). The estimations are based on the values of the membrane transport coefficients $\rho D_1/\delta = 0.3$ kg m⁻² s⁻¹, and $\rho D_2/\delta = 0.035$ kg m⁻² s⁻¹, both determined from unary permeation data. Further details of the model calculations, including isotherm fits, are provided in the Supplementary Material.

has the potential for diffusion-selective separation of propene/ propane mixtures. This expectation is fulfilled by the data of Pan et al. [37] on propene/ propane permeances across a ZIF-8





Fig. 6. (a) Snapshot, obtained from molecular simulation, showing adsorbed CO_2 and CH_4 molecules in DDR. (b, c) Permeances of CO_2 and CH_4 determined for unary and binary mixture permeation across DDR membrane at (b) 253 K, and (c) 303 K [28,29].

membrane; see Fig. 7c. The magnitude of Π_i is hardly influenced by the mixture composition in the upstream compartment; this implies that correlation effects have negligible influences and Eq. (8) is of adequate accuracy. The value of S_{perm} is about 35, lower than the value of 125 anticipated from the uptake data of Li et al. [36]. The reason for the lower permeation selectivity is that the adsorption selectivity is in favor of the saturated propane [38].

Fig. 7. (a) Snapshot, obtained from molecular simulation, showing adsorbed CO_2 and CH_4 molecules in the cages of ZIF-8. (b) Permeances of CO_2 and CH_4 determined for unary and binary mixture permeation by Bux et al. [35] with an upstream pressure of 100 kPa. (c) Permeances of propene and propane across a ZIF-8 membrane, determined as a function of the mole fraction of propene in the gas phase in the upstream compartment in the experiments reported by Pan et al. [37]. Further details on adsorption and diffusion are provided in the Supplementary Material.

Analogously, the membrane permeation experiments of Bux et al. [39] demonstrate that the permeation selectivity favors ethene; the rationale for this is traceable to the significantly higher diffusivities of the unsaturated species, as determined from Infra-Red Microscopy measurements. A further confirmation of the subtle influence of bond lengths and bond angles on diffusivities of alkenes and alkanes is provided by Ruthven and Reyes [40] who report S_{diff} values for propene/propane mixtures in excess of 1000 for CHA and DDR zeolites.

4. Systems with significant degree of correlations

We now investigate membranes made up of thin layers of materials such as MFI, FAU, NaX, IRMOF-1, and Matrimid for which correlation effects exert a strong influence causing the mixture permeation characteristics to be significantly different from unary permeation. Such effects are best illustrated by considering the experimental data of Sandström et al. [41] for permeances of H_2 and CO_2 in a MFI membrane, determined both from unary and binary mixture permeation data; see Fig. 8a. We note that the permeance of the tardier CO_2 in the mixture is practically the same as that for unary permeation for the entire



Fig. 8. (a) Permeances of H₂ and CO₂ determined for unary and binary mixture permeation across MFI membrane; data of Sandström et al. [41]. (b) Comparison of S_{perm} and S_{ads} values for CO₂/H₂ mixtures compared with corresponding unary values.



Fig. 9. (a) Snapshot showing the location of H₂ (1) and CO₂ (2) adsorbates within the intersecting channel structures of MFI. Video animations of the motion of the molecules is provided as Supplementary Material. (b) MD simulation data for D_1 , D_2 , and D_{12} for diffusion of equimolar $(q_1=q_2)$ H₂ (1)/CO₂ (2) mixtures in MFI as a function of the total mixture loading, q_t . (c) Experimental data on permeatores of H₂ and CO₂ compared with the estimations of Eqs. (2) and (3). The estimations are based on the values of $\rho D_1/\delta = 80$ kg m⁻² s⁻¹, $\rho D_2/\delta = 2.7$ kg m⁻² s⁻¹, both determined from unary permeation data. Furthermore, the degree of correlations, including isotherm fits, are provided in the Supplementary Material.

range of upstream (feed) partial pressures. For H_2 , the permeance in the mixture is about an order of magnitude lower than from unary experiments. This implies that mixture permeation is CO₂selective, whereas the data based on unary permeation demonstrates H_2 -selective performance; see S_{perm} data in Fig. 8b. This reversal of selectivity is only partly attributable to the fact that S_{ads} for mixture adsorption is much more strongly in favor of CO₂. For a proper modeling of the permeation experiments we need to have a clear understanding, and quantification, of correlation effects.

MFI zeolite consists of a set of intersecting channels of approximately 5.5 Å in size; Fig. 9a shows snapshot showing the location of H₂ and CO₂ adsorbates within the intersecting channels. The presence of strongly adsorbed CO₂ serves to hinder the motion of H₂; a qualitative appreciation of such hindering is evident by visual examination of the video animations of H₂/CO₂ mixture diffusion, uploaded as Supplementary Material. Indeed, Sandström et al. [41] consider the reduction in the H₂ permeance to be a result of "blocking" by the partner CO₂ molecules.

Fig. 9b presents MD simulation data for the M–S diffusivities, D_1 , D_2 , and D_{12} for diffusion of equimolar H₂ (1)/CO₂ (2) mixtures in MFI as a function of the total mixture loading, q_t . In the experiments of Sandström et al. [41], the total mixture loadings q_t are in the range 2–4 mol kg⁻¹. In this range of loadings the MD data show $D_1/D_{12} \approx 10-20$, and $D_1/D_{12} \approx 0.5-1$. Calculations using Eqs. (2) and (3) taking $D_1/D_{12} = 20$, along with the values of $\rho D_1/\delta = 80$ kg m⁻² s⁻¹ and $\rho D_2/\delta = 2.7$ kg m⁻² s⁻¹, both determined from unary permeation data are shown in Fig. 9c. There is a good agreement of model calculations with the experimentally

determined permeances. In order to underscore the significant influence of correlations, Fig. 9c also present the model calculations using Eq. (8) in which correlations are considered negligible. This simplified scenario over-estimates the H₂ permeance by about an order of magnitude; in sharp contrast, the simplified model predictions for CO₂ are indistinguishable from those obtained taking correlations into account. Generally speaking, correlation effects have a strong retarding influence of the permeation of more-mobile-less-strongly-adsorbed molecules. Conversely, correlation effects are of lesser importance for tardier-more-stronglyadsorbed species. Slowing-down effects cause of the decrease in the H₂/CO₂ selectivity of Matrimid membrane with increasing proportion of CO₂ in the upstream membrane compartment [42].

We now re-analyze the experimental data of van de Graaf et al. [9] for permeation of CH₄, C₂H₆, and C₃H₈ across an MFI membrane at 303 K. The values of the membrane transport coefficients $\rho D_i / \delta$ for each alkane are obtained from fitting the unary permeance data (cf. Fig. 10a). These values are used for estimations of the permeances in CH₄/C₂H₆, and CH₄/C₃H₈ mixtures. The two sets of experiment permeance data for CH₄/C₂H₆ mixtures (cf. Fig. 10b), and with varying feed composition (cf. Fig. 10c), can be described reasonably well taking $D_1/D_{12} = 1$; this value is within the range of values obtained from MD simulations presented in Fig. 3e,



Fig. 10. (a) Experimental data of van de Graaf et al. [9] for unary permeances of CH₄, C₂H₆, and C₃H₈ across an MFI membrane at 303 K. The continuous solid lines represent model calculations with the values of the membrane transport coefficients $\rho D_1/\delta = 0.08 \text{ kg m}^{-2} \text{ s}^{-1}$, 0.016 kg m⁻² s⁻¹, and 0.005 kg m⁻² s⁻¹, respectively; these values are used in the estimations of permeances in mixtures. (b, c) Experimental data for permeances of (b, c) CH₄/C₂H₆, and (d) CH₄/C₃H₈ mixtures. In (b) the upstream membrane compartment contains equimolar gas mixtures. In (c) and (d), the proportion of CH₄ in the feed compartment is varied, keeping the total pressure at 101 kPa. The continuous solid lines in (b), (c) and (d) are obtained using Eqs. (2) and (3) with the transport coefficient values as above, along with the value of the degree of correlations for CH₄: In (b) and (c) the degree of correlations $D_1/D_{12} = 1$, and $D_1/D_{12} = 5$ in (d). Further details of the model calculations, including isotherm fits, are provided in the Supplementary Material.

when determined at the experimental mixture loadings. For CH₄/ C₃H₈ mixtures, the adsorbate loadings are higher because of the stronger adsorption of propane; consequently the degree of correlations is stronger (cf. Fig. 3f). The CH₄/C₃H₈ mixture permeances are reasonably well described by taking $D_1/D_{12} = 5$; see comparisons of model calculations with experiments in Fig. 10d. It is encouraging to note that Eqs. (2) and (3) cover the essential features of mixture permeation, albeit with assumed inputs on values of D_1/D_{12} .

An important feature of MFI membrane separation of H_2/CO_2 , CH_4/C_2H_6 , and CH_4/C_3H_8 mixtures is that in all three cases the high degree of correlations within the intersecting channels serve to enhance the S_{perm} values which favor the more strongly adsorbed species in each case. Estimating the membrane performance by ignoring correlations and using the simplified Eq. (6) for S_{diff} will provide pessimistic estimates of membrane performance.

Let us now consider the influence of operating temperature, *T*, on mixture permeation characteristics. Vroon et al.[43] report data on permeation of CH_4/nC_4H_{10} mixtures in MFI membranes. Over the entire range of *T*, the permeance of nC_4H_{10} determined from mixture permeation is practically the same as for the pure component; see Fig. 11a. The situation with regard to the more mobile CH_4 is entirely different. At 298 K, the CH_4 permeance in the mixture is significantly lower, by a factor about 40, than that from unary permeation. As the temperature increases, the extent of lowering is considerably reduced, and at a temperature of

473 K, the lowering in CH₄ permeance is only about 20%. The rationale for this observation can be traced to the increase of the degree of correlations with increasing pore concentrations (cf. Fig. 3d); the pore concentrations are significantly lowered with increasing *T*.

Further evidence of the increasing importance of correlations with increasing pore concentrations is available in the experimental data of Bakker [44] for the permeation selectivity of CH_4/nC_4H_{10} mixtures in MFI membrane as a function of the upstream partial pressure of nC_4H_{10} , p_{20} ; see Fig. 11b. While the model calculations assuming $D_1/D_{12} = 5$, on basis of the data presented in Fig. 3d, is able to adequately capture the dependence of S_{perm} on p_{20} ; neglecting correlations anticipates significantly lower selectivities; the deviations become larger with increasing proportion of nC_4H_{10} . This implies that slowing-down effects improve selectivities in favor of the tardier *n*-butane.

Another illustration of the increase in the significance of correlation effects with increasing proportion of the tardier species is provided by simulations of transient permeation of CH_4/C_3H_8 mixtures across MFI membrane with $p_{10}=95$ kPa, $p_{20}=5$ kPa. Fig. 11c shows the component fluxes calculated for the two scenarios, both including and neglecting correlation effects. In the initial phase, the pores of the membrane are predominantly occupied by the more mobile CH_4 molecule and the downstream compartment contains almost exclusively CH_4 molecules. With the ingress of the tardier C_3H_8 into the pores, slowing-down effects



Fig. 11. (a) Component permeances for CH_4/nC_4H_{10} mixtures in MFI membranes as a function of the operating temperature; the experimental data are from Vroon et al. [43]. (b) Permeation selectivity of CH_4/nC_4H_{10} mixtures in MFI membrane as a function of the upstream partial pressure of nC_4H_{10} . (c) Transient permeation of CH_4/nC_4H_{10} mixtures across MFI membrane with $p_{10}=95$ kPa, $p_{20}=5$ kPa. The simulation results are for the two scenarios: including correlations (with data inputs the same as used in Fig. 10d), and ignoring correlations. (d) Experimental data for nC6-22DMB binary mixture permeation across MFI membrane, with upstream partial pressures $f_2=4f_1$ [46].

а

b

 $\rm H_2/CO_2$ selectivity, $\rm S_{perm}$ and $\rm S_{ads}$

С

come into play and the CH₄ flux suffers a reduction with increasing C₃H₈ ingress. Use of Eq. (8) predicts that the flux of CH₄ remains higher than that of C₃H₈ till steady-state is reached. Taking into account of correlations, results in the steady-state flux being lower than that of C₃H₈, in conformity with the experimental data shown in Fig. 10d. Experimental evidence of the curious maximum in the transient flux of the more mobile partner species is provided by Bakker [44] for MFI permeation.

Branched and cyclic hydrocarbons locate preferentially at the intersections of the channel structures of MFI zeolite [45]. There are four intersection sites per unit cell of MFI zeolites, and as a consequence the pure component isotherms of branched and cvclic hydrocarbons exhibit strong inflection characteristics at a loading, $\Theta = 4$ molecules per unit cell. Linear alkanes, on the other hand, can locate anywhere along the channels. The preferential location of branched alkanes at the intersections of MFI leads to other unusual adsorption and diffusion phenomena that can be exploited to achieve separation of hydrocarbon isomers [45]. For loadings $\Theta_t > 4$ molecules per unit cell, the adsorption is strongly in favor of the linear alkanes. For permeation of n-hexane(nC6)/ 2,2 dimethylbutane (22DMB) mixtures across an MFI membrane, the flux of 22DMB decreases when the upstream hydrocarbons pressures $p_t > 2$ kPa as observed in one set of the experiments of Gump et al. [46]; see Fig. 11d. At $p_t \approx 2$ kPa, the total loading in the zeolite ≈ 4 molecules per unit cell, and all the intersection sites are fully occupied and no more 22DMB can be adsorbed, causing the curious maximum in the 22DMB flux.

We believe that the proper appreciation, and quantification, of correlation effects can lead to the optimum choice of membrane materials. To demonstrate this, we consider separation of H₂/CO₂ and CH₄/CO₂ mixtures using NiMOF-74 membranes, that has been recently prepared using a layer-by-layer seeding technique [47]. NiMOF-74 has 1D hexagonal-shaped channels of 11 Å size (cf. Fig. 12a). From the unary permeance data at an upstream pressure of 0.1 MPa, the S_{perm} values for H_2/CO_2 mixture is 9.1, leading Lee et al. [47] to conclude: "high H₂/CO₂ ideal selectivity can be obtained for NiMOF-74 membranes". We shall demonstrate that an analysis of permeation of H₂/CO₂ mixtures across NiMOF-74 will lead us to entirely different conclusions due to a combination of two separate factors: (1) the mixture adsorption being strongly in favor of CO₂ by a factor of 100–500 (see IAST calculation data for S_{ads} in Figs. 12b) and (2) strong correlation effects within the 1D channels will have the effect of slowing-down the considerably more mobile H_2 . Estimation of S_{perm} assuming the value of $D_1/D_{12} = 20$, based on the MD simulation data for the structural analog MgMOF-74 with same channel size (cf. Fig. 3a) are shown in Fig. 12b. We note that the permeation selectivity is strongly in favor of CO₂, by a factor of 2–10, depending on the upstream pressure. If correlation effects are completely ignored, and the uncoupled Eq. (8) are used, then the separations are indeed H₂-selective as concluded by Lee et al. [47]. Experimental verifications of our predictions are warranted, in view of significantly higher permeabilities of NiMOF-74 membranes, by about two orders of magnitude, than materials such as ZIF-8, SAPO-34, and DDR [18].

CO₂-selective membranes having high permeabilities are particularly attractive in natural gas purification processes that operate on an extremely large scale at pressures ranging to 6 MPa. The unary permeance data for NiMOF-74 of Lee et al. [47] indicate that the selectivity is favor of CH₄ by a factor of 3.1. The lower permeance of CO₂ is caused primarily due its lower diffusivity within the channels caused by its higher binding energy [22]. However, our predictions of CH₄/CO₂ mixture permeation (cf. Fig. 12c) shows that the selectivities favor CO_2 by a factor of about 20. This selectivity is somewhat lower than that achieved with SAPO-34 (cf. Fig. 4b), but outweighing this is the significantly





Fig. 12. (a) Pore landscapes showing the 1D hexagonal-shaped channels of NiMOF-74. (b) Comparison of H₂/CO₂ S_{perm} values determined from the unary permeance experiments of Lee et al. [47] with the estimations of Eqs. (2) and (3) for mixture permeation. (c) Comparison of CH₄/CO₂ S_{perm} values determined from the unary permeance experiments of Lee et al. [47] with the estimations of Eqs. (2) and (3) for mixture permeation. The estimations in (b) and (c) are based on the membrane transport coefficients for H₂, CH₄, and CO₂ of $\rho D_i / \delta = 17$ kg m⁻² s⁻¹ and 0.3 kg m⁻² s⁻¹. Also shown in (b) and (c) are IAST calculations of S_{ads} . Further details of the model calculations, including isotherm fits, are provided in the Supplementary Material.

higher permeability in NiMOF-74 that is desirable in practice. For the same reason, membranes made of M-MOF-74 (M=Mg, Fe, Co, Ni, Zn) are attractive for alkene/alkene separations [48], affording high permeation selectivities favoring the unsaturated species.

5. Systems exhibiting molecular clustering

Pervaporation of water/alcohol mixtures is an important process in the processing industry, and a wide variety of membrane materials has been used, including polymeric (e.g. PERVAP, Chitosan, PDMS), zeolites (e.g. CHA, LTA, MFI, FAU, DDR), zeolitic imidazolate frameworks (e.g. ZIF-8) and mixed matrix membranes [49–51]. There is considerable evidence in the literature to indicate that hydrogen bonding, and consequent cluster formation manifests in LTA-4A [52,53], MFI [54–64],

ZIF-8 [65], Nafion [66], PDMS [67], NaX [68–72], and Chitosan [73].

For water/alcohol mixture diffusion, the diffusivity of each component is lowered due to molecular clusters being formed as a consequence of hydrogen bonding. This is illustrated in Fig. 13 that present MD simulations of D_1 , and D_2 for water/alcohol mixture diffusion in FAU, MFI, LTA, DDR, and CHA zeolites. In all cases, the diffusivity of water is reduced with increasing proportion of alcohol. Hydrogen bonding between water and alcohol molecule pairs serves to act as a "flexible leash" linking the



Fig. 13. Maxwell–Stefan diffusivities, D_{i} , in water/methanol, and water/ethanol mixtures of varying composition in (a, b) FAU, (c) MFI, (d) LTA, (e) DDR, and (f) CHA zeolites. The data are compiled from MD simulation results published in the literature [92–94]. In all cases the MD simulations were carried out under conditions in which the total concentration within the pores, c_t is held constant; the values c_t are specified in each case and are based on the accessible pore volume in the various zeolites. In some cases the corresponding loadings per unit, Θ_t are also specified. For CHA, DDR, and LTA the plotted diffusivities are the self-diffusivities, D_{i} , self, that are more accurate to determine and provide good approximations of the M–S diffusivities, i.e. D_{i} , self $\approx D_i$. The MD data are culled from our previous publications [92–97].

motion of the more mobile (water) and tardier (alcohol) species. The net result is that the motion of water is retarded due to cluster formation. For MFI, the diffusivity of methanol is practically independent of composition, while that for water shows a dramatic decrease with increasing methanol concentration (cf. Fig. 13c): this trend is the same as determined in the NMR experiments data of Caro et al. [74]. For LTA, and DDR the D_{i, self} of methanol decreases with increasing proportion of water; see Fig. 13d and e. For CHA, the self-diffusivities for methanol show a decreasing trend for low water concentrations, until a minimum is reached: see Fig. 13f. A similar minimum in the alcohol selfdiffusivity is observed for FAU zeolite; see Fig. 13a, and b. The general conclusion to be drawn from the MD data in Fig. 13 is that at either ends of the composition range, there is slowing-down of either component, due to increasing proportion of its partner species.

The clearest evidence of the strong influence of hydrogen bonding on diffusivities is demonstrated by comparing the experimental data [75] for the diffusivity of water in *n*-alkanes with those in *n*-alcohols of the same chain length; see Fig. 14a. We note that the diffusivity in the *n*-alcohols is lower by an order of magnitude. A part of this lowering is attributable to the higher alcohol viscosities but the major reduction is caused by hydrogen bonding.

A number of experimental data on pervaporation of water/ alcohol, mixtures can be interpreted using the MD data presented in Fig. 13. In the discussions of their Chitosan pervaporation experimental results (plotted in Fig. 14b), Srinivasa Rao et al. [73] remark "The hydrogen bond interaction between water and ethylene glycol forms a cluster, which has the formula $(ROH)_x$. yH_2O , so that separation by a hydrophobic membrane is difficult due to the relatively large coupling of the diffusion." The increase in the water diffusivity with increasing feed concentration of water, evident from the experimental data of Srinivasa Rao et al. [73], is similar to that observed in Fig. 13 for FAU. For water/isobutanol transport across PERVAP membranes, we note also that Valentínyi et al. [76] have adopted a diffusivity model in which the water diffusivity is an exponential function of the mole fraction of water in the feed mixture. For transport across a Nafion membrane in methanol fuel cell applications, strong hydrogen bonding between water and methanol is evidenced by molecular simulations [66], and NMR data on self-diffusivities in water/methanol mixtures provide further experimental confirmation of mutual slowing-down effects [77].

The experimental data of Khajavi et al. [78] for water–alcohol permeation across an H-SOD membrane show a significant increase in the water flux with increasing water concentrations in the feed mixture (see Fig. 14c), suggesting an increase in the water diffusivity with increasing proportion of water in the feed mixture.

For water/alcohol pervaporation across CHA zeolite membrane, the experimental data of Hasegawa et al. [79] show that the alcohol fluxes decrease with increasing water composition in the feed. Indeed, both water and alcohol fluxes are reduced with increasing concentrations of partner species in the mixture. Similar experimental data for water/alcohol pervaporation across DDR membranes are reported [80]. The decrease in the alcohol fluxes with increasing water concentration in the feed mixture



Fig. 14. (a) Comparison of the diffusivity of water in *n*-alkanes with those in *n*-alcohols of the same chain length; experimental data from Su et al. [75]. (b) Experimental data of Khajavi et al. [78] for water flux across a H-SOD membrane as a function of the water mole fraction in water/methanol, and water/ethanol mixtures. (c) Influence of wt% water in feed mixture on permeation flux, and diffusivity of water across Chitosan membrane; experimental data from Srinivasa Rao et al. [73]. (d) Experimental data of Sato et al. [51] for permeances for water/NMP pervaporation across CHA membrane.

observed experimentally in the CHA pervaporation experiments, must be ascribed, in part at least, to a reduction in the alcohol diffusivities observed in the MD simulation results presented in Fig. 13f.

The somewhat more complex dependence of the alcohol diffusivity on mixture composition observed in Fig. 13f is verified in the experimental data of Sato et al. [51] for industrial scale water/NMP pervaporation across CHA membrane. The NMP permeance decreases for water concentrations < 10 wt%, and tends to increase when the water feed concentrations > 15 wt%; see Fig. 14d. Since permeances are closely related to the diffusivities, the NMP diffusivities either decrease or increase depending on the feed composition.

An important consequence of molecular clustering is that the transport coefficients $\rho D_1/\delta$, and $\rho D_2/\delta$, cannot be estimated on the basis of unary pervaporation data. Furthermore, mutual slowing-down effects cannot be captured by the choice of D_{12} . In the study by Kuhn et al. [80] for water/alcohols pervaporation across a DDR membrane, it was found that the use of uncoupled Eq. (8) with the D_1 , and D_2 determined from unary permeation data, lead to a severe overestimation of the permeation fluxes. Molecular simulations have demonstrated cluster formation for acetone/methanol mixtures [81], and this rationalizes finding of Yu et al. [82] that their experimental data on permeation of this mixture across an MFI membrane can only be rationalized if both the components D_i , are lowered when compared to the unary permeation values.

Mutual slowing-down effects have been commonly ignored in the published Maxwell–Stefan model implementations for mixture transport in water–alcohols pervaporation across DDR [80], LTA [11], MFI [82], methylated silica [83,84] membranes, and in methanol fuel cells [85,86]. Further research is necessary to generalize the Maxwell–Stefan formulation in a manner that explicitly allows for cluster formation, by defining a cluster to be a pseudo-species in the mixture. A step in this direction has been taken by Nasiri and Aroujalian [67] who model water/ ethanol pervaporation across PDMS membrane by explicitly allowing for dimer formation.

6. Conclusions

By analyzing experimental data on permeation of a variety of mixtures across membrane materials with different characteristics we have discerned two types of coupling effects.

The first type of coupling occurs when the less-mobile species slows down its more mobile partner by not vacating an adsorption site quick for its more mobile partner to occupy that position. The Maxwell-Stefan formulation for mixture permeation, expressed in Eqs. (2) and (3), allows a quantitative prediction of mixture permeation using unary permeance data for estimation of the two membrane transport coefficients $\rho D_1/\delta$, and $\rho D_2/\delta$. The parameter D_1/D_{12} quantifies the slowing-down effects; this parameter must be estimated on the basis of MD data. The degree of correlations, D_1/D_{12} , is strongly dependent on the pore size, topology and connectivity. In cage-type structures (e.g. CHA, DDR, LTA, and ZIF-8) in which adjacent cages are separated by narrow windows, correlation effects are weak. On the other hand the extent of correlations is particularly strong in structures consisting of one-dimensional channels (e.g. NiMOF-74), or intersecting channels (e.g. MFI) structures. Our work demonstrates the possibility of enhancing permeation selectivities by appropriate choice of materials with high degree of correlations. For example, the efficacy of NiMOF-74 membranes in natural gas purification applications hinges on the high degree of correlations within the 1D channels.

The second type of coupling occurs as a consequence of molecular clustering due to hydrogen bonding. Such clustering effects, commonly prevalent in alcohol/water pervaporation, can cause mutual slowing-down of partner molecules in the mixture. A priori predictions of mixture permeation is not possible on the basis of unary permeation data alone. In view of the significant importance of membrane pervaporation processes, there is a need to develop better understanding and models to describe the influence of molecular clustering on both mixture adsorption and diffusion.

Notation

с.	nore concentration of species $i c_{-a}/V$ mol m ⁻³
-	por concentration of species i, $c_1 = q_1/v_p$, mor m
C _t	total pore concentration in mixture, $c_t = q_t/V_p$, mol m
D_i	M–S diffusivity of species <i>i</i> , $m^2 s^{-1}$
D _{i,self}	Self-diffusivity of species <i>i</i> , $m^2 s^{-1}$
D_{12}	M–S exchange coefficient, $m^2 s^{-1}$
F	factor defined by Eq. (9), dimensionless
p _i	partial pressure of species <i>i</i> in upstream compartment, Pa
p_t	total pressure in upstream compartment, Pa
q_i	molar loading of species <i>i</i> , mol kg ^{-1}
q_t	total molar loading of mixture, mol kg^{-1}
N _i	molar flux of species <i>i</i> defined in terms of the membrane
	area, mol m ⁻² s ⁻¹
S _{ads}	adsorption selectivity defined by Eq. (5), dimensionless
S _{diff}	diffusion selectivity defined by Eq. (6), dimensionless
Sperm	permeation selectivity defined by Eq. (1), dimensionless
Т	temperature, K
V_p	pore volume, $m^3 kg^{-1}$
x _i	mole fraction of species i in the adsorbed phase, dimen-
	sionless

Greek letters

- δ thickness of membrane, m
- Π_i permeance of species *i* in mixture, mol m⁻² s⁻¹ Pa⁻¹
- ϕ fractional pore volume of microporous material, dimensionless
- Θ_t total molar loading of mixture, molecules per unit cell or per cage
- ρ framework density, kg m⁻³

Subscripts

- 0 referring to upstream membrane compartment
- *i* referring to component *i*
- *t* referring to total mixture
- δ referring to downstream membrane compartment

Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at http://dx.doi.org/10.1016/j.memsci.2012.12.004.

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