



# A Metal–Organic Framework with Suitable Pore Size and Specific Functional Sites for the Removal of Trace Propyne from Propylene

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**Abstract:** Separation of propyne/propylene ( $C_3H_4/C_3H_6$ ) is more difficult and challenging than that of acetylene/ethylene ( $C_2H_2/C_2H_4$ ) because of their closer molecular sizes. A comprehensive screening of a series of metal–organic frameworks with broad types of structures, pore sizes, and functionalities was carried out. UTSA-200 was identified as the best separating material for the removal of trace  $C_3H_4$  from  $C_3H_4/C_3H_6$  mixtures. Gas sorption isotherms reveal that UTSA-200 exhibits by far the highest  $C_3H_4$  adsorption capacity ( $95\text{ cm}^3\text{ cm}^{-3}$  at 0.01 bar and 298 K) and record  $C_3H_4/C_3H_6$  selectivity, which was mainly attributed to the suitable dynamic pore size to efficiently block the larger  $C_3H_6$  molecule whilst the strong binding sites and pore flexibility capture smaller  $C_3H_4$ . This material thus provides record purification capacity for the removal of  $C_3H_4$  from a 1:99 (or 0.1:99.9, v/v)  $C_3H_4/C_3H_6$  mixture to produce 99.9999% pure  $C_3H_6$  with a productivity of 62.0 (or 142.8)  $\text{mmol g}^{-1}$ .

Adsorptive separation based on porous materials opens the door to enable a possible transition from traditional energy-intensive cryogenic distillation to the energy-efficient adsorbent-based separation for industrial gas separation and purification.<sup>[1]</sup> Compared to conventional activated carbons and zeolites, the emerging microporous metal–organic frame-

works (MOFs) have attracted immense attention for gas separation/purification in recent years owing to their fascinating tunability with respect to pore size, shape, and surface functionality.<sup>[2]</sup> These features have enabled us to design target materials with the on-demand pore size and functionality for diverse gas separation and purification, including separation of  $\text{CO}_2/\text{N}_2$ ,  $\text{CO}_2/\text{CH}_4$ , light hydrocarbons,  $\text{C}_2\text{H}_2/\text{CO}_2$ ,  $\text{O}_2/\text{N}_2$ ,  $\text{CO}/\text{CO}_2$ , and so on.<sup>[3]</sup>

Gas molecules with quite different molecular weights and thus vapor pressures or boiling points, for example,  $\text{CO}_2$  and  $\text{N}_2$ , can be easily separated because of their different interactions with porous materials.<sup>[4]</sup> Those gas molecules with similar molecular weights and vapor pressures are difficult and challenging to be separated.<sup>[5]</sup> Ultramicroporous MOFs are superior to well-developed porous materials for gas separation/purification; this superiority is attributed to their power of the finely tuned pores to enforce the sieving effects and the readily immobilized functional sites on the pore surfaces to introduce the specific recognition with one of the gas molecules, and the interplay of dual functionalities of both the suitable size and functional site.<sup>[6,7]</sup> Indeed, a few ultramicroporous MOFs have been discovered for the very challenging separations of  $\text{C}_2\text{H}_2/\text{C}_2\text{H}_4$ ,  $\text{C}_2\text{H}_2/\text{CO}_2$ ,  $\text{C}_2\text{H}_4/\text{C}_2\text{H}_6$ , and  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  over the past several years.<sup>[7]</sup> Compared with the separation of  $\text{C}_2\text{H}_2/\text{C}_2\text{H}_4$ , the  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  separation is more difficult and challenging. As shown in Scheme 1, acetylene and ethylene are the simplest alkyne and alkene with a three-dimensional (3D) size of  $3.32 \times 3.34 \times 5.70$  and  $3.28 \times 4.18 \times 4.84\text{ \AA}^3$ , respectively. The kinetic diameter difference between  $\text{C}_2\text{H}_2$  (3.3 Å) and  $\text{C}_2\text{H}_4$  (4.2 Å) is about 0.9 Å.<sup>[8]</sup> Propyne and propylene, also known as methylacetylene and

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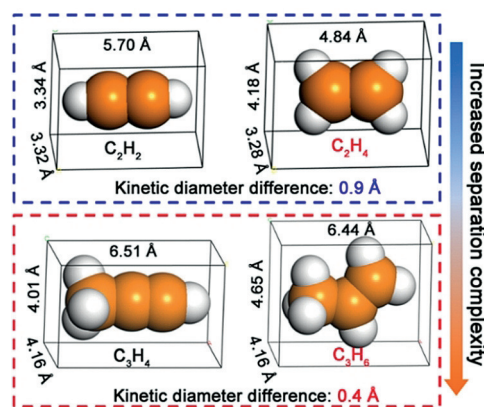
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**Scheme 1.** Comparison of molecular size and kinetic diameter difference of  $\text{C}_2\text{H}_2/\text{C}_2\text{H}_4$  and  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$ .

methylethylene, have a larger size of  $4.16 \times 4.01 \times 6.51$  and  $4.65 \times 4.16 \times 6.44 \text{ \AA}^3$ .  $\text{C}_3\text{H}_4$  is a linear molecule, and  $\text{C}_3\text{H}_6$  has a curved shape. Despite different shapes, the relatively bulky methyl group makes the kinetic diameter difference between the pair  $\text{C}_3\text{H}_4$  and  $\text{C}_3\text{H}_6$  (4.2 and 4.6  $\text{\AA}$ ) much closer (nearly 0.4  $\text{\AA}$ ) than  $\text{C}_2\text{H}_2/\text{C}_2\text{H}_4$ .<sup>[2a]</sup> The smaller the size difference between the pair of molecules is, the more difficult the separation will be.

Removal of trace  $\text{C}_3\text{H}_4$  (1000 or 10000 ppm) from  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  mixtures is one of the most important separation processes to produce polymer-grade  $\text{C}_3\text{H}_6$  gas (the  $\text{C}_3\text{H}_4$  impurity should be lower than 5 ppm), a prime olefin raw material for petrochemical production. Microporous materials for  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  separation have not been well-explored, with only the ELM-12, SIFSIX-3-Ni (SIFSIX = hexafluorosilicate ( $\text{SiF}_6^{2-}$ )) and ZU-62 having been reported.<sup>[9]</sup> While these materials exhibit high  $\text{C}_3\text{H}_4$  adsorption capacity, they only exhibit moderately high gas-separation performance because of the comparatively large pores to include both  $\text{C}_3\text{H}_4$  and  $\text{C}_3\text{H}_6$  molecules, thus limiting the productivity of the desired  $\text{C}_3\text{H}_6$  product. Targeting high performance porous materials can not only significantly enhance the  $\text{C}_3\text{H}_6$  productivity, but also increase the purity of the  $\text{C}_3\text{H}_6$  product, thus reduce the energy cost for this important industrial separation. Adsorption selectivity and uptake capacity are the two most important criteria that are directly related to productivity and purity, but it is very difficult to target materials with both high values (so-called trade-off). To realize high selectivity and adsorption uptake simultaneously, ideal MOFs should have suitable pore size and specific functionality that can discriminate the difference in size and physical properties between the two molecules. While

rational design of microporous MOFs with desired high productivity for  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  separation is quite difficult, we thus systematically screened a series of porous MOFs with different structures, pore sizes, and pore-surface functionalities for this separation. To our surprise, the material UTSA-200 ( $[\text{Cu}(\text{azpy})_2(\text{SiF}_6)]_n$ , azpy = 4,4'-azopyridine),<sup>[7b]</sup> which we recently realized for the highly efficient  $\text{C}_2\text{H}_2/\text{C}_2\text{H}_4$  separation, turned out to be very powerful as well for the more difficult  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  separation. Our detailed studies comprehensively affirm its benchmark separation performance with the record  $\text{C}_3\text{H}_4$  uptake capacity ( $95 \text{ cm}^3 \text{ cm}^{-3}$  at 0.01 bar and 298 K), gas selectivity (over 20000), and  $\text{C}_3\text{H}_6$  productivity ( $62.0$  and  $142.8 \text{ mmol g}^{-1}$  for 1:99 and 0.1:99.9 mixtures).

We first selected 20 different MOFs to examine their  $\text{C}_3\text{H}_4$  and  $\text{C}_3\text{H}_6$  adsorption properties and then superficially evaluate their separation potential (see the Supporting Information, Table S1 for detailed structural parameters). As shown in the Supporting Information, Figure S1, achieving the looked-for efficient separation is indeed very challenging for  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  separation, and the examined MOFs almost show unsatisfactory separation properties. Despite the daunting challenge, some reported MOFs with strong binding sites toward  $\text{C}_3\text{H}_4$  (SIFSIX-1-Cu, SIFSIX-2-Cu-i, SIFSIX-3-Ni, and ELM-12) exhibit steep adsorption of  $\text{C}_3\text{H}_4$  at the low-pressure region over  $\text{C}_3\text{H}_6$ , leading to the benchmark selectivity reported so far. However, their pore sizes allow the passage of both  $\text{C}_3\text{H}_4$  and  $\text{C}_3\text{H}_6$ , thus delimiting their high gas selectivities.<sup>[9]</sup> UTSA-200, with a smaller aperture size of 3.4  $\text{\AA}$ , exhibits an exceptionally high  $\text{C}_3\text{H}_4$  uptake but very little  $\text{C}_3\text{H}_6$  adsorption at the low-pressure region (Figure 1), offering the potential to be the best candidate for  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  separation.

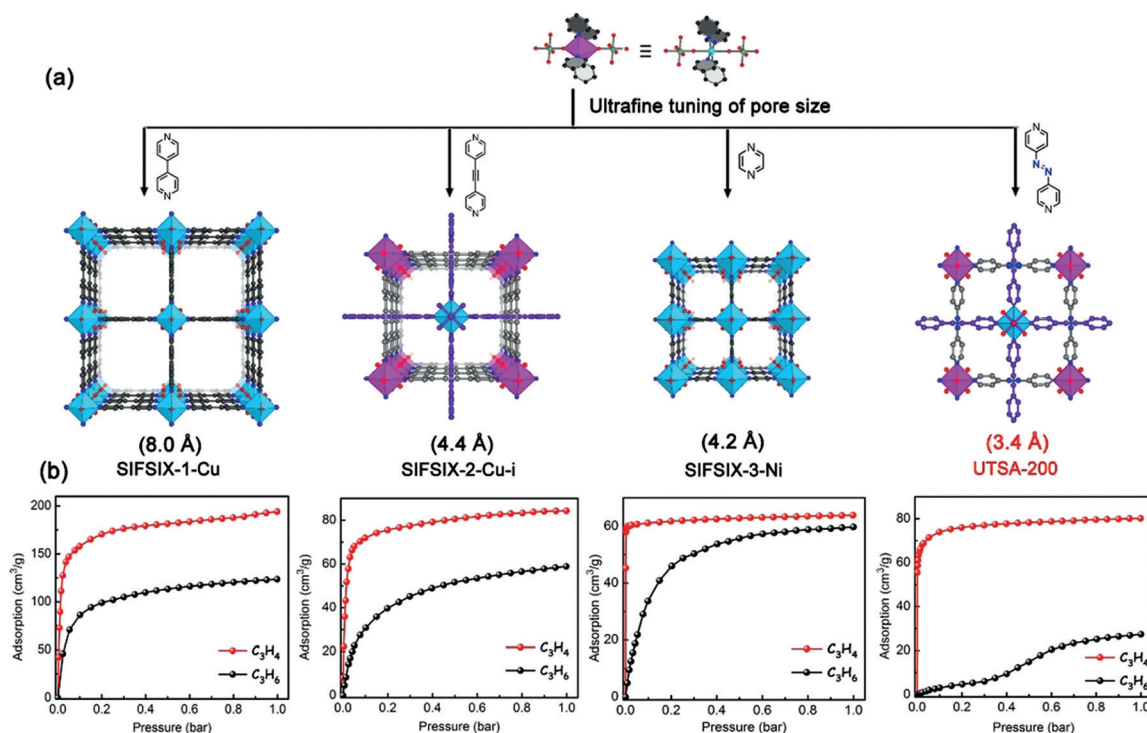


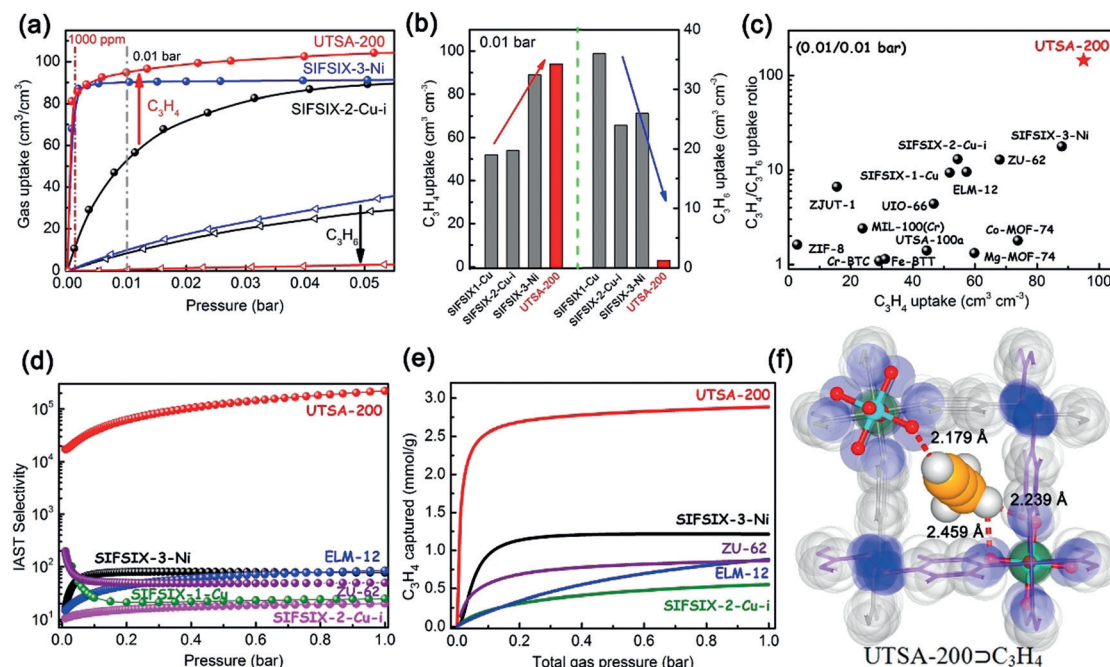
Figure 1. a) The pore aperture and pore chemistry of SIFSIX materials. b) Associated  $\text{C}_3\text{H}_4$  and  $\text{C}_3\text{H}_6$  adsorption isotherms at 298 K.

Structural analysis revealed that pore sizes in SIFSIX-1-Cu, SIFSIX-2-Cu-i, and SIFSIX-3-Ni range from microporous (8.0 Å) to ultra-microporous (4.2 Å, Figure 1 a),<sup>[7a,10]</sup> indeed allowing both C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> to enter the pores. The doubly interpenetrated UTSA-200 possesses much smaller channels of 3.4 Å.<sup>[7b]</sup> This static pore size is notably less than both of C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub>, which might induce the selective sieving toward the larger C<sub>3</sub>H<sub>6</sub> molecules when the framework flexibility and thus slightly enlarged pore sizes are taken into the account. Furthermore, there exist a large number of SiF<sub>6</sub><sup>2-</sup> anions around the channels that show much stronger binding affinity toward alkynes over alkenes.<sup>[7a,9b]</sup> These structural features on UTSA-200 might be responsible for the exceptional performance for C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> separation. Bulk purity of UTSA-200 sample was confirmed by powder X-ray diffraction (PXRD) patterns and the measured surface area (Supporting Information, Figure S2).<sup>[11]</sup>

All of these SIFSIX materials show steep and high C<sub>3</sub>H<sub>4</sub> uptakes over C<sub>3</sub>H<sub>6</sub> at 298 K (Figure 1 b). When the pore size was gradually reduced from SIFSIX-1-Cu to UTSA-200, the C<sub>3</sub>H<sub>4</sub> sorption isotherms at low-pressure region (0–0.01 bar) become steeper and steeper (Figure 2 a). The C<sub>3</sub>H<sub>4</sub> capture capacity at 0.01 bar increases in the order of SIFSIX-1-Cu < SIFSIX-2-Cu-i < SIFSIX-3-Ni < UTSA-200 (Figure 2 b), wherein UTSA-200 shows the highest value of 95 cm<sup>3</sup> cm<sup>-3</sup>. Even under an ultralow C<sub>3</sub>H<sub>4</sub> partial pressure (1000 ppm), the C<sub>3</sub>H<sub>4</sub> uptake capacity of UTSA-200 can reach 83 cm<sup>3</sup> cm<sup>-3</sup>, still notably higher than SIFSIX-3-Ni (75 cm<sup>3</sup> cm<sup>-3</sup>), SIFSIX-2-Cu-i (11 cm<sup>3</sup> cm<sup>-3</sup>), and ZU-62 (5.2 cm<sup>3</sup> cm<sup>-3</sup>). In comparison to other top-performing materials, UTSA-200 also sets

new benchmarks at both 0.01 and 0.001 bar (Figure 2c; Supporting Information, Figure S3), making it the most promising material for the trace C<sub>3</sub>H<sub>4</sub> removal. In contrast, UTSA-200 shows an ignorable C<sub>3</sub>H<sub>6</sub> uptake at 0.01 bar (Figure 2 b), and little C<sub>3</sub>H<sub>6</sub> uptake up to 0.4 bar (10.5 cm<sup>3</sup> cm<sup>-3</sup>), which is dramatically lower than SIFSIX-2-Cu-i (61.2 cm<sup>3</sup> cm<sup>-3</sup>), SIFSIX-3-Ni (85.1 cm<sup>3</sup> cm<sup>-3</sup>) and ZU-62 (69.7 cm<sup>3</sup> cm<sup>-3</sup>) at 0.4 bar. The fine-tuned pore size of UTSA-200 indeed supports the molecular exclusion of C<sub>3</sub>H<sub>6</sub> at low pressures. Most importantly, the sieving effect of C<sub>3</sub>H<sub>6</sub> can be strengthened with the temperature increased to 318 K while the low-pressure C<sub>3</sub>H<sub>4</sub> uptake capacity can be retained (Supporting Information, Figure S5), indicating its bright promise for C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> separation at a broader operation temperature.

Ideal adsorbed solution theory (IAST) was utilized to calculate the adsorption selectivity of these materials for a 1:99 (v/v) C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> mixture at 298 K. UTSA-200 exhibits an extraordinary high selectivity of over 20000 (Figure 2d; Supporting Information, Figure S7), significantly higher than the previous benchmark ELM-12 (83), SIFSIX-3-Ni (76), and ZU-62 (48). It should be noted that the selectivity of UTSA-200 can be only used for the qualitative comparison. As shown in the Supporting Information, Figure S8, the uptake ratio of C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> for UTSA-200 at 0.01:0.01 and 0.01:0.99 bar can reach 149.5 and 2.49, respectively. Both values are the highest among the indicated MOFs, further confirming its best C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> selectivity. Furthermore, UTSA-200 also exhibits the record C<sub>3</sub>H<sub>4</sub> uptake (2.88 mmol g<sup>-1</sup>) for adsorption from this mixture (Figure 2 e).



**Figure 2.** a) Experimental C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> adsorption isotherms of SIFSIX-2-Cu-i (black), SIFSIX-3-Ni (blue), and UTSA-200 (red) at 298 K in the region of 0–0.05 bar. b) Comparison of C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> uptake at 0.01 bar for the SIFSIX materials. c) A comparison of C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> uptake ratio at 0.01:0.01 bar for UTSA-200 and other indicated MOFs. d) IAST selectivity and e) IAST calculated C<sub>3</sub>H<sub>4</sub> uptake capacity of the indicated MOFs from 1:99 (v/v) gas mixtures. f) DFT-D calculated structure and binding site of UTSA-200⊃C<sub>3</sub>H<sub>4</sub>. The different nets are highlighted in purple and gray for clarity. Cu cyan, Si dark green, F red, N blue, C gray, H white, C in C<sub>3</sub>H<sub>4</sub> orange.

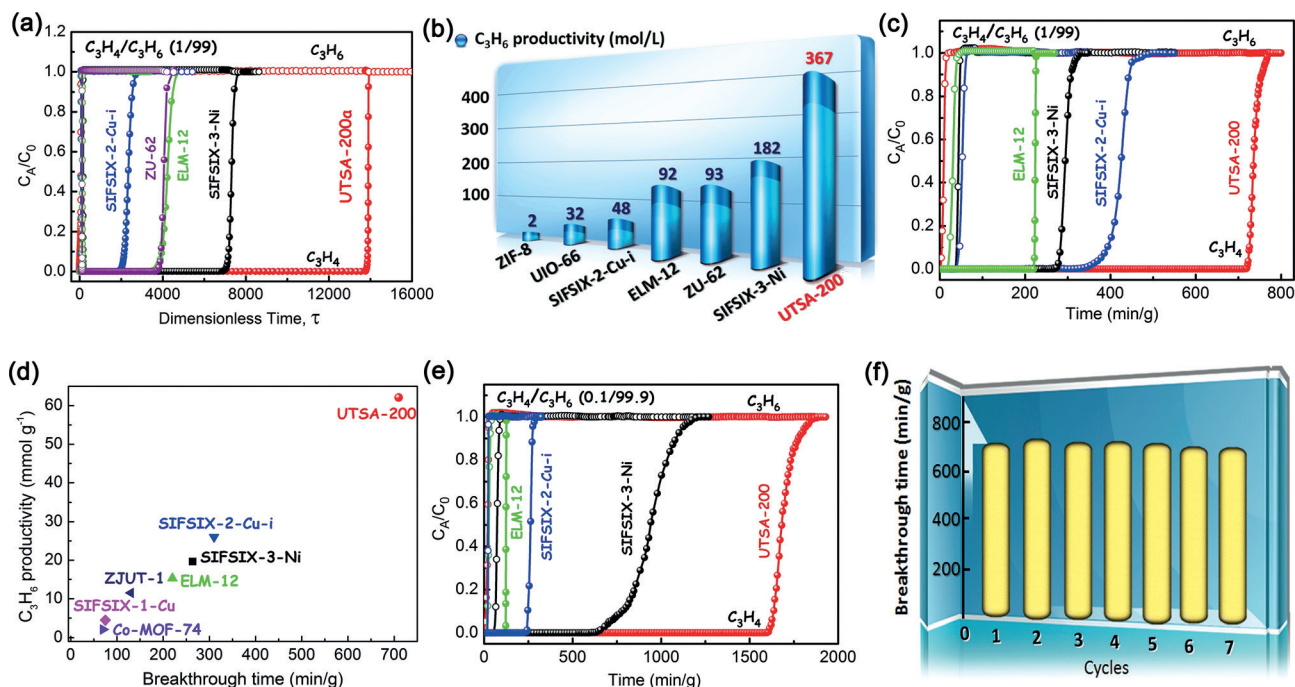


To understand the origin of the ultra strong  $C_3H_4$  adsorption and effective  $C_3H_6$  sieving, we performed detailed modeling studies using first-principles dispersion-corrected density functional theory (DFT-D) method on UTSA-200. The static pore size of UTSA-200, based on the crystal structure, is about 3.4 Å,<sup>[7b]</sup> which is much smaller than both  $C_3H_4$  (4.2 Å) and  $C_3H_6$  (4.6 Å).<sup>[2a]</sup> As shown in the Supporting Information, Figure S9, after adsorption of  $C_3H_4$  molecules, the N=N bond and pyridine rings on the azpy exhibit an obvious rotation and distortion, which enlarges the pore to about 4.2 Å, thereby allowing the passing of a  $C_3H_4$  molecule. Calculations also show that each adsorbed  $C_3H_4$  molecule is bound by two  $SiF_6^{2-}$  sites from different nets through cooperative C–H...F and C≡H...F H-bonding, with the short distance of 2.179 and 2.239/2.459 Å (Figure 2 f). Owing to the larger size of  $C_3H_6$ , the pore needs to be expanded more for the passage (Supporting Information, Figure S10). The calculated static binding energies for  $C_3H_4$  and  $C_3H_6$  are 62.3 kJ mol<sup>-1</sup> and 45.4 kJ mol<sup>-1</sup>, respectively. The framework thus has much stronger binding with  $C_3H_4$  molecule than  $C_3H_6$ , as further confirmed by the higher experimental isosteric heat of adsorption ( $Q_{st}$ ) for  $C_3H_4$  (Supporting Information, Figure S11). This kind of subtle guest-assisted pore opening is primarily dictated by the interaction strength of the adsorbate framework: the stronger the intermolecular interactions are, the lower the gate-opening pressure will be.<sup>[6b,12]</sup> Therefore, attributed to the smaller size and the stronger interactions with the framework,  $C_3H_4$  molecule might open the pore easily to result in the ultrastrong  $C_3H_4$  adsorption. Conversely, the larger size and weaker interac-

tions of  $C_3H_6$  molecule make the pore opening more difficult and thereby to be size-excluded, especially at the low-pressure region.

High-resolution neutron powder diffraction (NPD) measurements were further performed on a  $C_3D_4$ -loaded sample of UTSA-200 at 298 K to confirm the calculated  $C_3H_4$  binding sites. The data indicate that  $C_3D_4$  adsorption indeed induced a lot of local framework distortion in the sample (to accommodate the large gas molecules), resulting in lower overall crystal symmetry. Consequently, it became impractical to perform a rigorous Rietveld refinement of the NPD data. Fortunately, it is still possible to qualitatively compare the experimental data with the simulated NPD pattern based on a model structure built upon the DFT-D calculation results. As shown in the Supporting Information, Figure S12, the two agree reasonably well, and thus strongly support the validity of the DFT-D determined  $C_3H_4$  binding configuration.

Transient breakthrough simulations were first conducted for UTSA-200 and the indicated MOFs in fixed-bed adsorption processes to determine the feasibility of  $C_3H_4/C_3H_6$  separation. The 1:99 (v/v)  $C_3H_4/C_3H_6$  mixture was employed as feeds to mimic the industrial process conditions. As depicted in Figure 3 a, efficient separations were realized with all the examined MOFs, whereby  $C_3H_6$  first eluted through the bed to yield a polymer-grade gas, and then  $C_3H_4$  broke through from the bed at a certain time  $\tau_{break}$ . Owing to the record selectivity and  $C_3H_4$  uptake capacity, UTSA-200 exhibits the longest  $\tau_{break}$  value, several times higher than that in SIFSIX-3-Ni, ELM-12, and ZU-62 (Supporting Information, Figure S13). During the time 0– $\tau_{break}$ , the pure  $C_3H_6$



**Figure 3.** a) Transient breakthrough simulations of  $C_3H_4/C_3H_6$  (1:99, v/v) mixture on UTSA-200 versus some benchmark materials at 298 K. b) Plots of the productivity of pure  $C_3H_6$  from  $C_3H_4/C_3H_6$  mixtures in the simulated breakthrough for the indicated MOFs. c) Experimental breakthrough curves for 1:99 (v/v) mixture under a flow of 2.0 mL min<sup>-1</sup> at 298 K and 1.01 bar. d) The  $C_3H_6$  productivity from  $C_3H_4/C_3H_6$  mixtures of the indicated MOFs, with  $C_3H_4$  concentration less than 1 ppm. e) Experimental breakthrough curves for a 0.1:99.9 (v/v) mixture. f) Retained time of  $C_3H_6$  in cycling tests of UTSA-200 for a 1:99 (v/v) mixture.

productivity by UTSA-200 can reach  $367.2 \text{ mol L}^{-1}$  (Figure 3b), which is notably higher than that of SIFSIX-3-Ni, ZU-62, and ELM-12.

Experimental breakthrough studies were performed in a packed column of activated UTSA-200 under flow ( $2.0 \text{ mL min}^{-1}$ ) of binary  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  (1:99, v/v) mixtures at 298 K, and compared with the indicated MOFs. The breakthrough data depicted in Figure 3c clearly demonstrate that UTSA-200 can effectively separate  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  mixtures: the  $\text{C}_3\text{H}_6$  gas passed through the adsorption bed immediately, while  $\text{C}_3\text{H}_4$  was retained in the packed column over  $710 \text{ min g}^{-1}$ . This breakthrough time of  $\text{C}_3\text{H}_4$  is three times longer than that of SIFSIX-2-Cu-i, ELM-12, and SIFSIX-3-Ni. These experimental data are consistent well with the simulated results. The concentration of  $\text{C}_3\text{H}_4$  in the outlet effluent was even below 1 ppm up to 700 min (Supporting Information, Figure S14), which is notably less than the acceptable level of less than 5 ppm for polymer-grade  $\text{C}_3\text{H}_6$  gas. It is to be noted that this deep removal of  $\text{C}_3\text{H}_4$  from 1:99 (v/v) mixture is unable to be achieved for most selected MOFs (such as MOF-74 series, Cu-BTC, ZIF-8, MIL-100) owing to their unsatisfied selectivity (Supporting Information, Figure S15). Among the viable MOFs, the  $\text{C}_3\text{H}_6$  production of UTSA-200 from the outlet effluent for a given cycle was calculated to be record high of  $62.9 \text{ mmol g}^{-1}$  (Figure 3d; Supporting Information, Table S14), far exceeding those observed in SIFSIX-3-Ni ( $19.6 \text{ mmol g}^{-1}$ ) and ELM-12 ( $15.8 \text{ mmol g}^{-1}$ ). For  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  mixture containing ultralow  $\text{C}_3\text{H}_4$  concentration (1000 ppm), UTSA-200 also exhibits the best separation performance with the record  $\text{C}_3\text{H}_6$  production of  $143.8 \text{ mmol g}^{-1}$ , as illustrated in Figure 3e and the Supporting Information, Table S15. Finally, the separation performance of UTSA-200 can be recycled at least 7 times (Figure 3f; Supporting Information, Figures S17–S22).

Through a comprehensive screening of broad types of MOFs, we demonstrated herein an ultra-microporous MOF, UTSA-200, as the best separating material for the removal of trace  $\text{C}_3\text{H}_4$  from  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  mixtures. The foregoing results revealed that UTSA-200 exhibits both the unprecedented high  $\text{C}_3\text{H}_4$  capture capacity and separation selectivity, setting new benchmarks for any material reported so far. This exceptional separation performance is attributed to the framework flexibility originated from the rotation of pyridine rings inside the pores and the strong binding sites that can selectively block the larger  $\text{C}_3\text{H}_6$  but capture large amount of the preferred smaller  $\text{C}_3\text{H}_4$  at low-pressure region. Breakthrough experiments confirmed that UTSA-200 can completely remove trace  $\text{C}_3\text{H}_4$  from 1:99 and 0.1:99.9 (v/v) mixtures, affording the record-high  $\text{C}_3\text{H}_6$  production scale with 99.9999% purity. This work not only reports the best porous material for  $\text{C}_3\text{H}_4/\text{C}_3\text{H}_6$  separation, but also demonstrates that framework flexibility can be utilized to target some very challenging gas separations, thus fully fulfilling the promise of emerging microporous MOFs for gas separations in the future.

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## Conflict of interest

The authors declare no conflict of interest.

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## Supporting Information

### **A Metal–Organic Framework with Suitable Pore Size and Specific Functional Sites for the Removal of Trace Propyne from Propylene**

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3. Isosteric heat of adsorption
4. Density functional theory (DFT) calculations
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## SUPPORTING INFORMATION

## Experimental Procedures

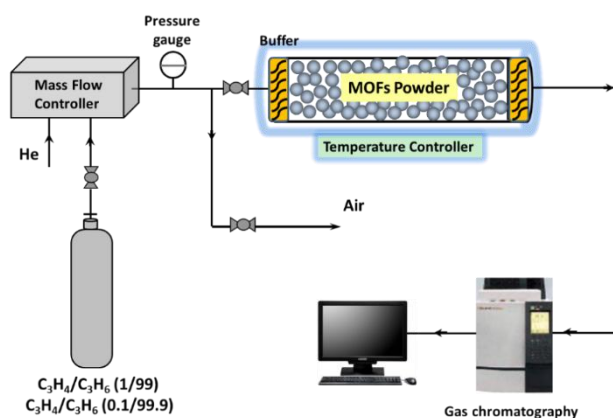
## General Materials and MOF Synthesis

The selected SIFSIX materials (SIFSIX-1-Cu, SIFSIX-2-Cu-i, SIFSIX-3-Ni, and UTSA-200) were synthesized using methods reported in the corresponding literatures.<sup>[1-4]</sup> The phase purity of the bulk materials was confirmed by PXRD (Figure S2). Powder X-ray diffraction (PXRD) patterns were measured by a BRUKER D8 ADVANCE diffractometer employing Cu-K $\alpha$  radiation operated at 30 kV and 15 mA, scanning over the range 5-40° (2 $\theta$ ) at a rate of 1°/min. **Note that the synthesis of UTSA-200 needs careful control of the reaction condition; because a small amount of impurities are easily produced during the production of UTSA-200,<sup>[5,6]</sup> which would greatly affect the separation performance.** In this work, the bulk purity of UTSA-200 was undoubtedly confirmed by PXRD patterns and the measured surface area/pore volume (617 m<sup>2</sup> g<sup>-1</sup> and 0.27 cm<sup>3</sup> g<sup>-1</sup>, Figure S2), which is consistent well with the theoretical ones calculated from the crystal structure (597 m<sup>2</sup> g<sup>-1</sup> and 0.26 cm<sup>3</sup> g<sup>-1</sup>). C<sub>3</sub>H<sub>4</sub> (99.99%), C<sub>3</sub>H<sub>6</sub> (99.99%), He (99.999%) and mixed gases of C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> = 1/99 (v/v), C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> = 0.1/99.9 (v/v) were purchased from Beijing Special Gas Co. LTD (China). All starting chemicals and solvents were purchased from commercial companies and used without further purification.

## Gas sorption measurements

An Intelligent Gravimetric Analyzer (IGA 001, Hiden, UK) was used to measure gas adsorption isotherms. ThermoFisher water bath is used to keep the adsorption tube at a constant temperature of 273, 298, 308, and 318 K. The samples were activated to remove all the guest solvents according to the reported literatures.<sup>34,35</sup>

## Breakthrough experiments



The breakthrough experiments for C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> (1/99 and 0.1/99.9) mixtures were carried out at a flow rate of 2 mL/min (298 K, 1.01 bar). Activated MOF powder was packed into  $\Phi$  4 × 150 mm stainless steel column under pure N<sub>2</sub> atmosphere (Table S13). The sample in each column was compressed as much as possible to obtain the best separation performance, and column voidages are similar for different samples. The experimental set-up consisted of two fixed-bed stainless steel reactors. One reactor was loaded with the adsorbent, while the other reactor was used as a blank control group to stabilize the gas flow. The horizontal reactors were placed in a temperature controlled environment, maintained at 298 K. The flow rates of all gases mixtures were regulated by mass flow controllers, and the effluent gas stream from the column is monitored by a gas chromatography. Prior to the breakthrough experiment, we activated the sample by flushing the adsorption bed with helium gas for 2 h at 323 K. The adsorption bed was regenerated by He flow (100 mL/min) for 1 h at 298 K.

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## Neutron diffraction experiment

Powder neutron diffraction data were collected using the BT-1 neutron powder diffractometer at the National Institute of Standards and Technology (NIST) Center for Neutron Research. A Ge(311) monochromator with a 75° take-off angle,  $\lambda = 2.0787(2)$  Å, and in-pile collimation of 60 minutes of *arc* was used. Data were collected over the range of 1.3-166.3° (2 $\theta$ ) with a step size of 0.05°. Fully activated UTSA-200 sample was loaded in a vanadium can equipped with a capillary gas line. A closed-cycle He refrigerator was used to control the sample temperature. The bare MOF sample was measured first at the temperatures of 298 K. To probe the C<sub>3</sub>H<sub>4</sub> adsorption locations, a pre-determined pressure (1 bar) of C<sub>3</sub>D<sub>4</sub> were loaded into the sample at room temperature. Diffraction data were then collected on the C<sub>3</sub>D<sub>4</sub>-loaded UTSA-200 samples. (Note: deuterated gas C<sub>3</sub>D<sub>4</sub> was used to avoid the large incoherent neutron scattering background that would be produced by the hydrogen in C<sub>3</sub>H<sub>4</sub>.)

## Fitting of pure component isotherms

To calculate the C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> adsorption selectivity for UTSA-200, SIFSIX-3-Ni, SIFSIX-2-Cu-i, and ELM-12 at 298 K, pure component isotherms of these four MOFs were fitted with Dual-site Langmuir-Freundlich model.

$$q = q_{A,sat} \frac{b_A p^{v_A}}{1 + b_A p^{v_A}} + q_{B,sat} \frac{b_B p^{v_B}}{1 + b_B p^{v_B}} \quad (1)$$

with T-dependent parameters  $b_A$ , and  $b_B$

$$b_A = b_{A0} \exp\left(\frac{E_A}{RT}\right); \quad b_B = b_{B0} \exp\left(\frac{E_B}{RT}\right) \quad (2)$$

The fitting parameters for C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> are provided in Table S3-S11. Figure S6 presents a comparison of experimental data for adsorption isotherms C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> in UTSA-200, SIFSIX-3-Ni, SIFSIX-2-Cu-i, and ELM-12 with dual-site Langmuir model fits. The fits are of good accuracy for both guest molecules.

In order to compare the C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> separation potential of various MOFs, IAST calculations of mixture adsorption were performed. For separation of a binary mixture of components A and B, the adsorption selectivity is defined by

$$S_{ads} = \frac{q_A/q_B}{y_A/y_B} \quad (3)$$

where the  $q_A$ , and  $q_B$  represent the molar loadings within the MOF that is in equilibrium with a bulk fluid mixture with mole fractions  $y_A$ , and  $y_B = 1 - y_A$ . The molar loadings, also called *gravimetric uptake capacities*, are usually expressed with the units mol kg<sup>-1</sup>. The IAST calculations of C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> adsorption selectivities taking the mole fractions  $y_A = 0.01$  and  $y_B = 1 - y_A = 0.99$  for a total pressure of 100 kPa and 298 K.

The separations in fixed bed absorbers are also influenced by the uptake capacities. The *volumetric uptake capacities* are

$$Q_A = \rho q_A; \quad Q_B = \rho q_B \quad (4)$$

where  $\rho$  is the crystal framework density of the MOF, expressed say in units of kg m<sup>-3</sup>, or kg L<sup>-1</sup>. The objective of C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> separations is to obtain pure C<sub>3</sub>H<sub>6</sub>. Krishna has defined a combined selectivity/capacity metric, called the *separation potential*<sup>[7]</sup>

$$\Delta Q = Q_A \frac{y_B}{1 - y_B} - Q_B \quad (5)$$

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The physical significance of  $\Delta Q$ , conveniently expressed in the units of mol per L of adsorbent, is that it represents the *maximum* amount of pure component B (less strongly adsorbed component) that can be recovered during the *adsorption* phase of fixed bed separations. The quantity  $Q$  is an appropriate combination of selectivity and uptake capacity that is reflective of the separations in fixed beds packed with a specific adsorbent.

**Isosteric heat of adsorption**

The binding energies of  $C_3H_4$  and  $C_3H_6$  in the MOFs are reflected in the isosteric heat of adsorption,  $Q_{st}$ , defined as

$$Q_{st} = RT^2 \left( \frac{\partial \ln p}{\partial T} \right)_q \quad (6)$$

These values were determined using the pure component isotherm fits using the Virial equation (Figure S11).  $Q_{st}$  is the coverage-dependent isosteric heat of adsorption and  $R$  is the universal gas constant. The heat enthalpy of  $C_3H_4$  adsorption for UTSA-200 are determined by the adsorption data measured from 0-1 bar at 298, 308, and 318 K.

**Density functional theory (DFT) calculations**

First-principles density-functional theory (DFT) calculations were performed using the Quantum-Espresso package.<sup>48</sup> A semi-empirical addition of dispersive forces to conventional DFT was included in the calculation to account for van der Waals interactions.<sup>49</sup> We used Vanderbilt-type ultrasoft pseudopotentials and generalized gradient approximation (GGA) with Perdew-Burke-Ernzerhof (PBE) exchange correlation. A cutoff energy of 544 eV and a  $2 \times 2 \times 4$  k-point mesh (generated using the Monkhorst-Pack scheme) were found to be enough for the total energy to converge within 0.01 meV/atom. We first optimized the structure of UTSA-200. The optimized structures are good matches for the experimentally determined crystal structures of the coordination networks. Various guest gas molecules were then introduced to various locations of the channel pore, followed by a full structural relaxation. To obtain the gas binding energy, an isolated gas molecule placed in a supercell (with the same cell dimensions as the MOF crystal) was also relaxed as a reference. The static binding energy (at  $T = 0$  K) was then calculated using:  $E_B = E(\text{MOF}) + E(\text{gas}) - E(\text{MOF}+\text{gas})$ .

**Transient breakthrough of  $C_3H_4/C_3H_6$  mixtures in fixed bed adsorbents**

The performance of industrial fixed bed adsorbents is dictated by a combination of adsorption selectivity and uptake capacity. Transient breakthrough simulations were carried out for 1/99  $C_3H_4/C_3H_6$  mixtures operating at a total pressure of 100 kPa and 298 K, using the methodology described in earlier publications. For the breakthrough simulations, the following parameter values were used: length of packed bed,  $L = 0.3$  m; voidage of packed bed,  $\varepsilon = 0.4$ ; superficial gas velocity at inlet,  $u = 0.04$  m/s. The transient breakthrough simulation results are presented in terms of a *dimensionless* time,  $\tau$ , defined by dividing the actual time,  $t$ , by the characteristic time,  $L\varepsilon u^{-1}$ .

We investigated the separation performance of UTSA-200 and the indicated MOFs for the separation of 1/99  $C_3H_4/C_3H_6$  feed mixtures. The transient breakthrough simulations in Figure 3a show the molar concentrations of  $C_3H_4/C_3H_6$  in the gas phase exiting the adsorbent packed with MOF adsorbents as a function of the dimensionless time,  $\tau$ . In these simulations, the total bulk gas phase is at 298 K and 100 kPa; the partial pressures of  $C_3H_4$ , and  $C_3H_6$  in the inlet feed gas mixture are, respectively,  $p_1 = 1$  kPa,  $p_2 = 99$  kPa. Analogous breakthrough simulations were performed for UTSA-200 and the other indicated MOFs. On the basis of the gas phase concentrations, we can calculate the impurity level of  $C_3H_4$  in the gas mixture exiting the fixed bed packed with adsorbents; see Figure S13. At a certain time,  $\tau_{\text{break}}$ , the impurity level will exceed the desired purity level of 5 ppm that corresponds to the purity requirement of the feed to the

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polymerization reactor. The adsorption cycle needs to be terminated at that time break and the regeneration process needs to be initiated. From a material balance on the adsorber, the amount of  $C_3H_4$  captured during the time interval  $0 - \tau_{break}$  can be determined. Figure 3d presents a plot of the amount of  $C_3H_4$  captured plotted as a function of the time interval  $\tau_{break}$ . The hierarchy of capture capacities is directly related to the corresponding hierarchy of breakthrough times,  $\tau_{break}$ . UTSA-200 has a significantly higher capture capacity, by more than a factor two, than other MOFs. In addition, we also determined the volumetric productivity of  $C_3H_6$  containing  $< 5$  ppm  $C_3H_4$  (Figure 3b). These volumetric productivities are presented in Table S12. The productivities are linearly related to the IAST calculations of the separation potential  $\Delta Q$ . The highest productivity is achieved with UTSA-200. Cu-BTC is unable to produce the product with the desired purity of  $< 5$  ppm  $C_3H_4$ .

## Notation

$b_A$	Langmuir-Freundlich constant for species $i$ at adsorption site A, $Pa^{-\nu}$
$b_B$	Langmuir-Freundlich constant for species $i$ at adsorption site B, $Pa^{-\nu}$
$E$	energy parameter, $J mol^{-1}$
$p_i$	partial pressure of species $i$ in mixture, Pa
$p_t$	total system pressure, Pa
$q_i$	component molar loading of species $i$ , $mol kg^{-1}$
$Q_{st}$	isosteric heat of adsorption, $J mol^{-1}$
$t$	time, s
$T$	absolute temperature, K

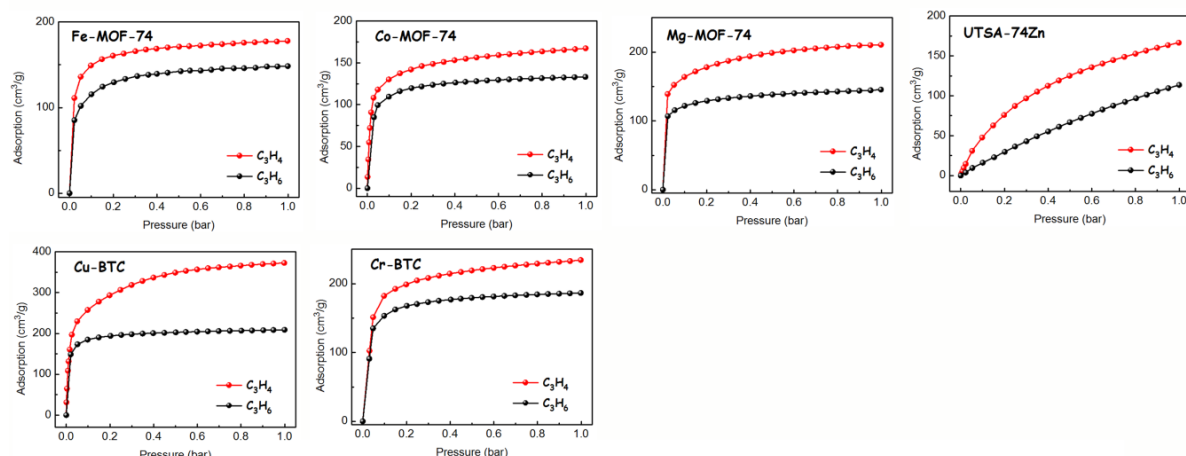
## Greek letters

$\nu$	Freundlich exponent, dimensionless
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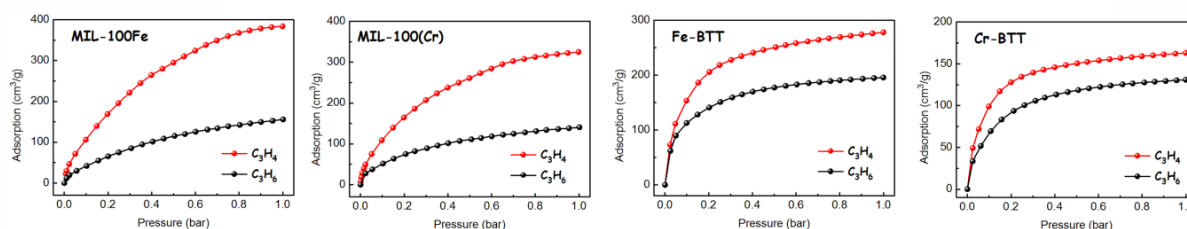


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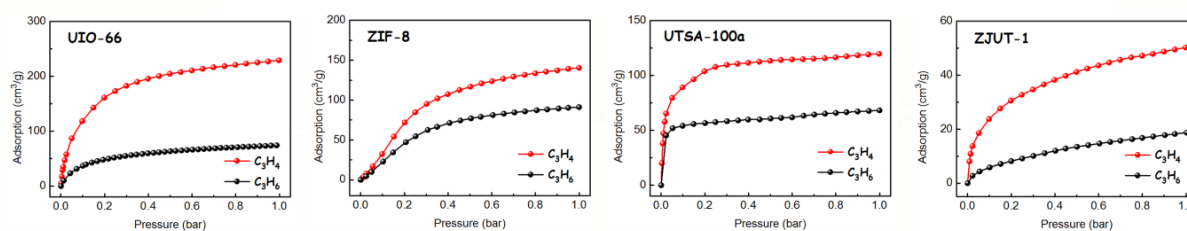
## MOFs with high density of open metal sites:



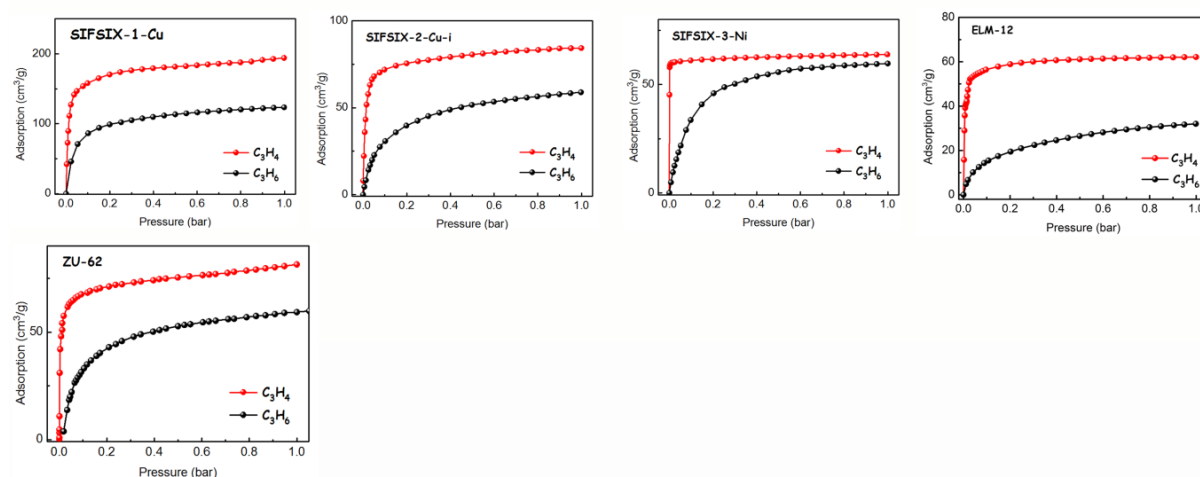
## MOFs with large porosities:



## Small-pore MOFs:



## MOFs with functional groups:



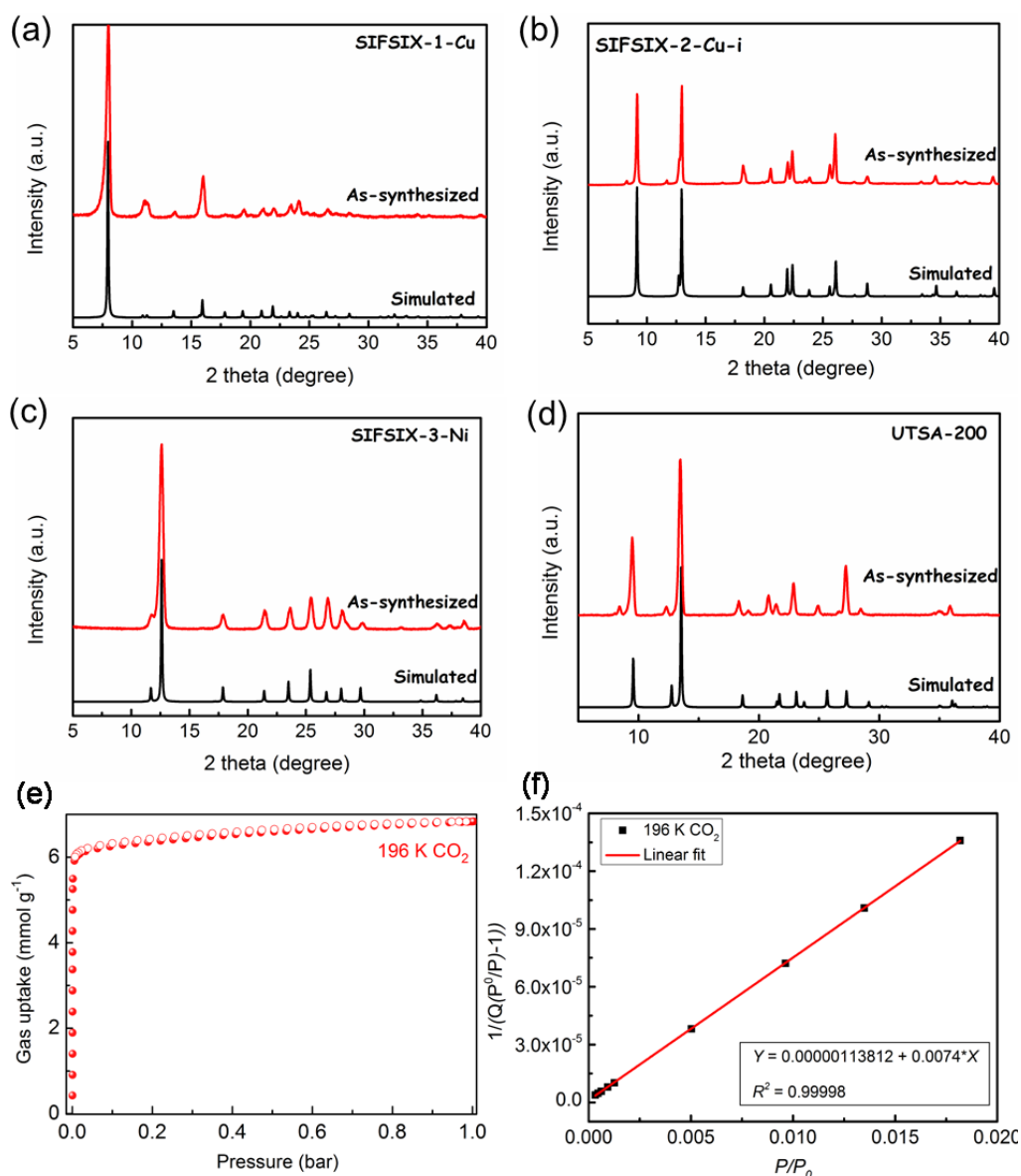
**Figure S1.** Experimental  $C_3H_4$  (red) and  $C_3H_6$  (black) adsorption isotherms of the selected MOF materials at 298 K, including some MOFs with high density of open metal sites (Fe-MOF-74, Co-MOF-74, Mg-MOF-74, UTSA-74, Cu-BTC, and Cr-BTC), some MOFs with high porosities (MIL-100(Fe), MIL-100(Cr), Fe-BTT, and Cr-BTT), some small-pore MOFs (UIO-66, ZIF-8, UTSA-100, and ZJUT-1), and MOFs with functional  $SiF_6^{2-}$  or OTF<sup>-</sup> sites (SIFSIX-1-Cu, SIFSIX-2-Cu-i, SIFSIX-3-Ni, ELM-12, and ZU-62). The detailed structural information of these selected MOFs are summarized in Table S1. It was found that achieving the looked-for efficient separation is indeed very challenging for  $C_3H_4/C_3H_6$  separation, and the examined MOFs almost show unsatisfied separation properties. For instance, MOF-74

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series render steep and high  $C_3H_4$  adsorption at low pressure, but their selectivity of  $C_3H_4$  over  $C_3H_6$  are quite low because of the equal affinity for both gas molecules toward open metal sites. High porosities in MOFs (such as MIL-100 and Fe-BTT) facilitate high total  $C_3H_4$  uptake amounts at 1 bar, but a slow increase of  $C_3H_4$  adsorption at low pressure and the absence of sieving effect which are detrimental to achieve high selectivity. Further, some ultra-small pore MOFs (3.5–4.0 Å range) without functional sites (such as ZIF-8, UTSA-100) also show unsatisfied adsorption selectivity due to the moderate strong  $C_3H_4$  capture capacity. It is to be noted that those MOFs with strong binding sites toward  $C_3H_4$  (SIFSIX-1-Cu, SIFSIX-2-Cu-i, SIFSIX-3-Ni, ZU-62, and ELM-12) exhibit steep adsorption of  $C_3H_4$  at low-pressure region over  $C_3H_6$ , leading to the benchmark selectivity reported so far. However, their pore sizes allow the passage of both  $C_3H_4$  and  $C_3H_6$ , thus delimiting their high gas selectivities.

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**Experimental values:**

$$S_{\text{BET}} = (1/(0.0074 - 1.13812 \times 10^{-6}))/22414 \times 6.023 \times 10^{23} \times 0.170 \times 10^{-18} = 617 \text{ m}^2 \text{ g}^{-1}$$

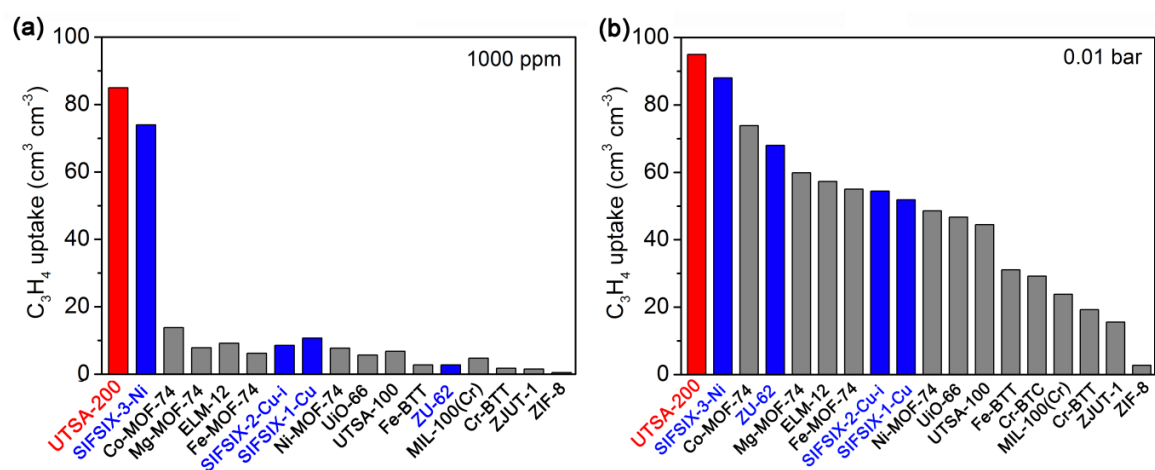
$$V_p = 0.27 \text{ cm}^3 \text{ g}^{-1}$$

**Theoretical values calculated from the crystal structure:**

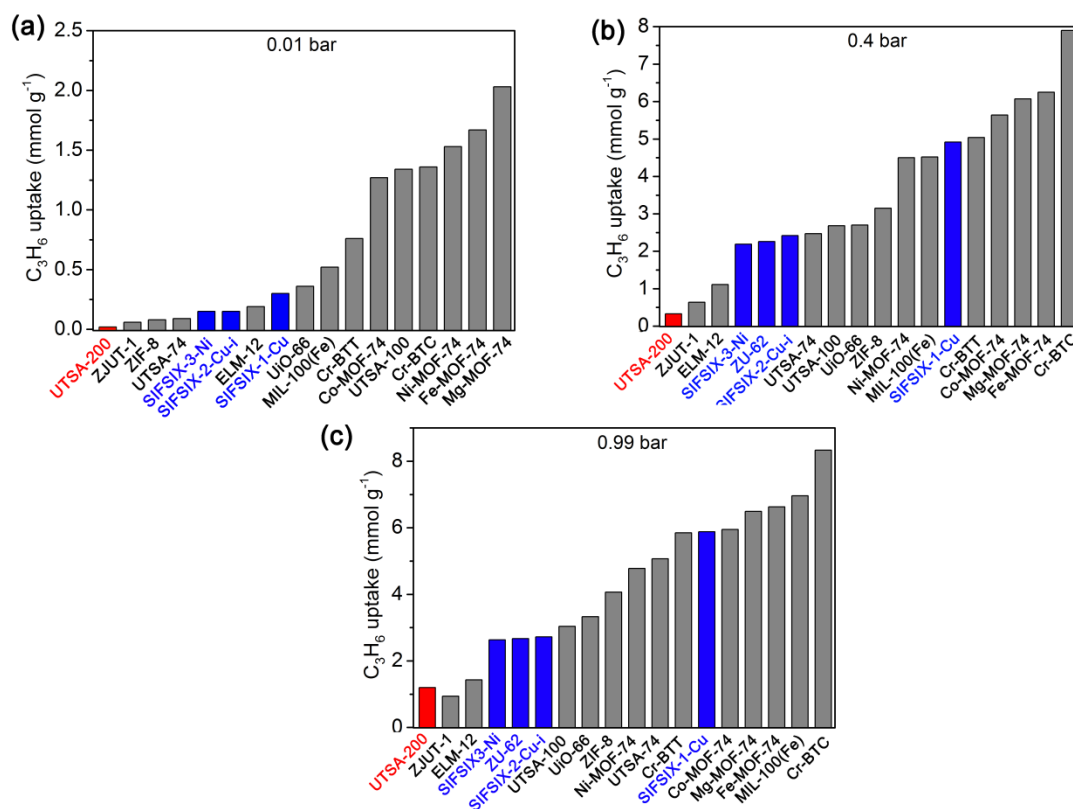
$$S_{\text{BET}} = 597 \text{ m}^2 \text{ g}^{-1}; V_p = 0.26 \text{ cm}^3 \text{ g}^{-1}$$

**Figure S2.** PXRD patterns of as-synthesized sample SIFSIX-1-Cu (a), SIFSIX-2-Cu-i (b), SIFSIX-3-Ni (c), and UTSA-200 (d), along with the simulated XRD pattern from the single-crystal X-ray structure. (e,f) Gas adsorption isotherms of UTSA-200a for CO<sub>2</sub> at 196 K, and the BET surface area and pore volume of UTSA-200 obtained from the 196 K CO<sub>2</sub> isotherms, which is in good agreement with the theoretical values calculated from the crystal structure.

## SUPPORTING INFORMATION



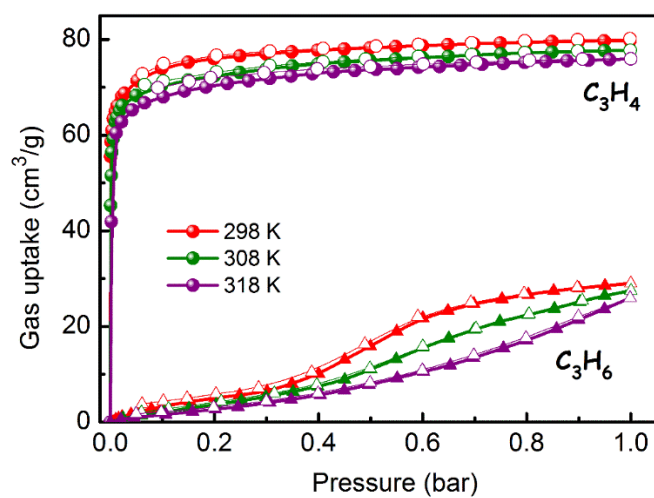
**Figure S3.** Comparison of  $C_3H_4$  uptake for UTSA-200 and other examined materials at ultralow  $C_3H_4$  partial pressure of 1000 ppm or 0.01 bar and 298 K, indicating that UTSA-200 exhibits the highest  $C_3H_4$  uptake capacity at both 1000 ppm and 0.01 bar.



**Figure S4.** Comparison of  $C_3H_6$  uptake for UTSA-200 and other examined materials at the partial pressure of (a) 0.01 bar; (b) 0.4 bar; (c) 0.99 bar (at 298 K), indicating that UTSA-200 exhibits the lowest  $C_3H_6$  uptake in the entire range of 1.0 bar.

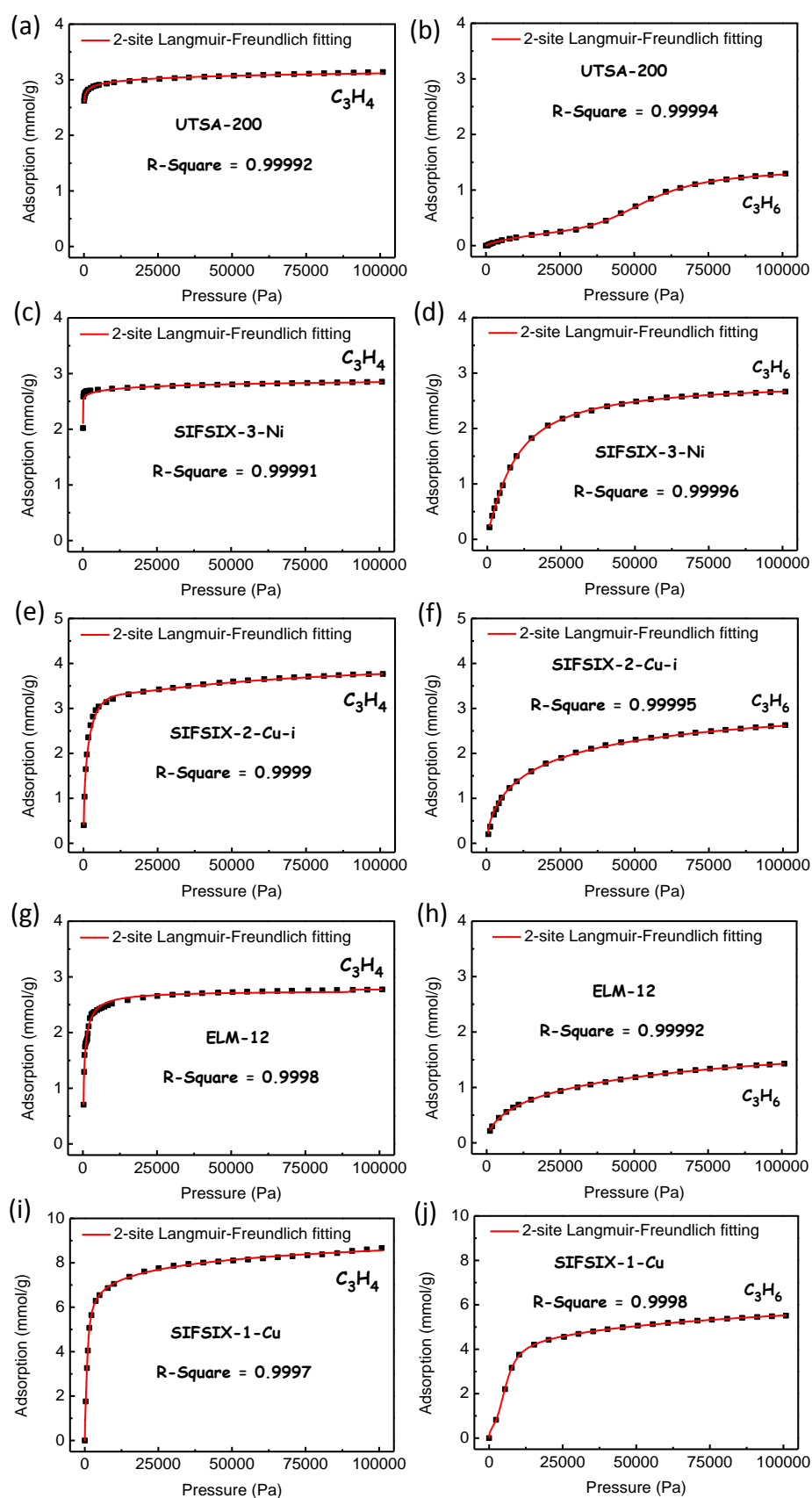


## SUPPORTING INFORMATION



**Figure S5.** Gas sorption isotherms of C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> for UTSA-200 at 298-318 K. The entrance of C<sub>3</sub>H<sub>6</sub> molecule can be efficiently blocked under the pressure lower than 0.4 bar. When the pressure was further increased to 1 bar, C<sub>3</sub>H<sub>6</sub> adsorption isotherm slopes up all the time. This is because the N=N bond and the pyridine rings in the MOF linker have certain rotational flexibility, so the pore sizes can be slightly enlarged under higher pressure (larger than 0.4 bar) to take up more C<sub>3</sub>H<sub>6</sub> molecules.

## SUPPORTING INFORMATION



## SUPPORTING INFORMATION

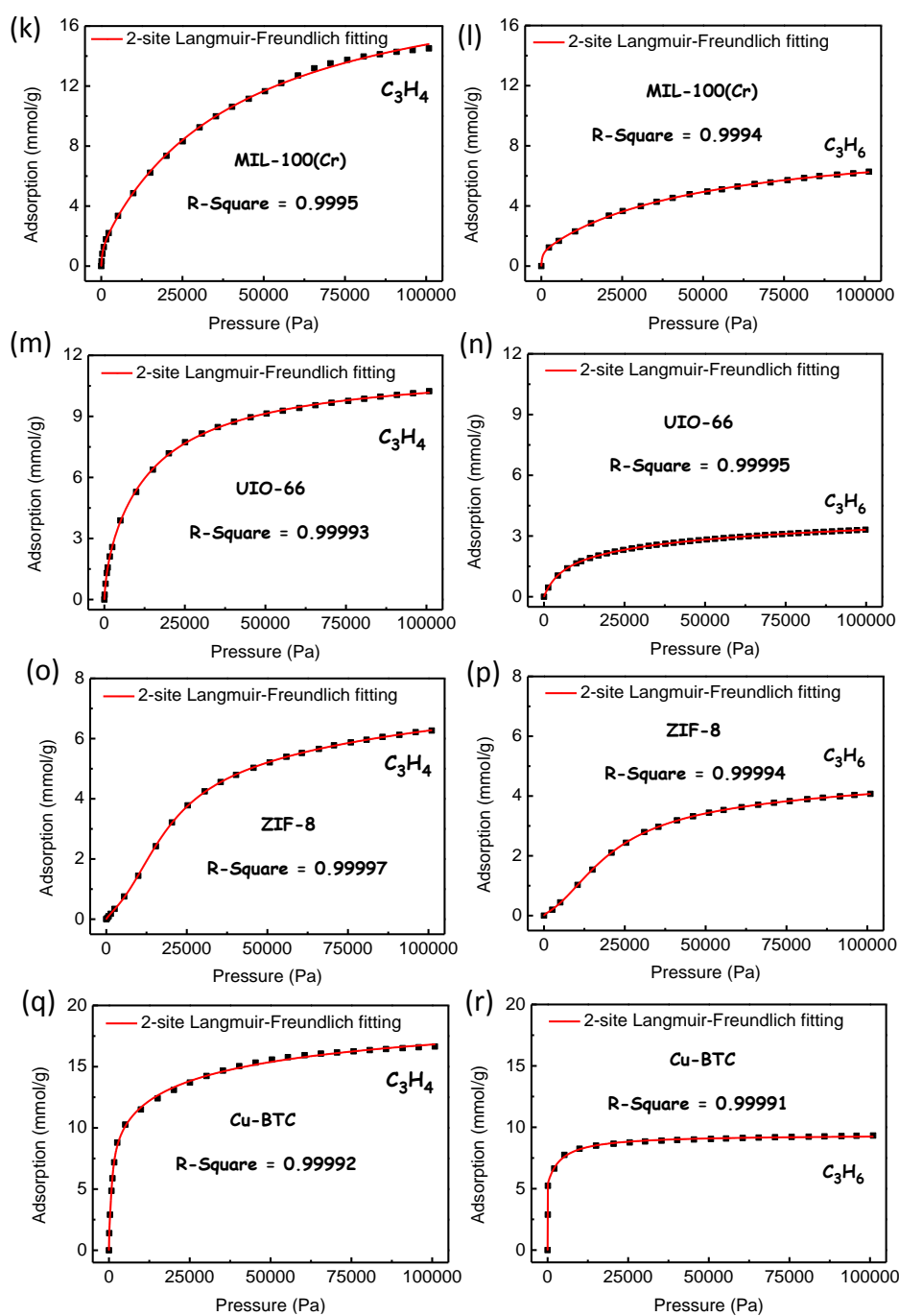


Figure S6.  $C_3H_4$  and  $C_3H_6$  adsorption isotherms at 298 K in selected MOFs with dual-site Langmuir-Freundlich model fits.

## SUPPORTING INFORMATION

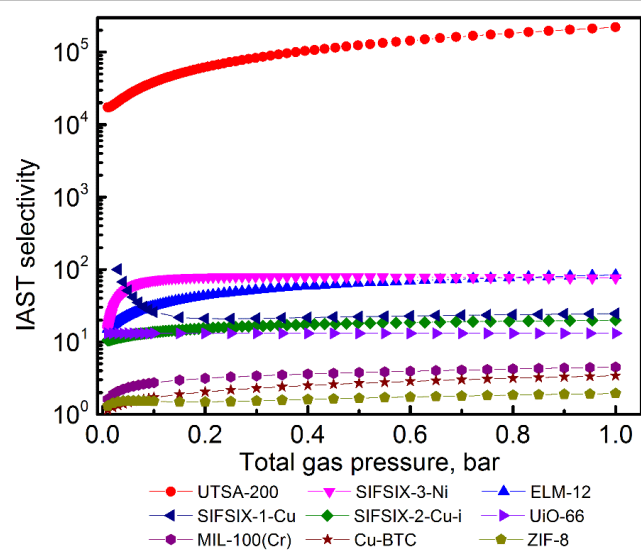


Figure S7. IAST selectivity of UTSA-200 versus the indicated MOF materials.

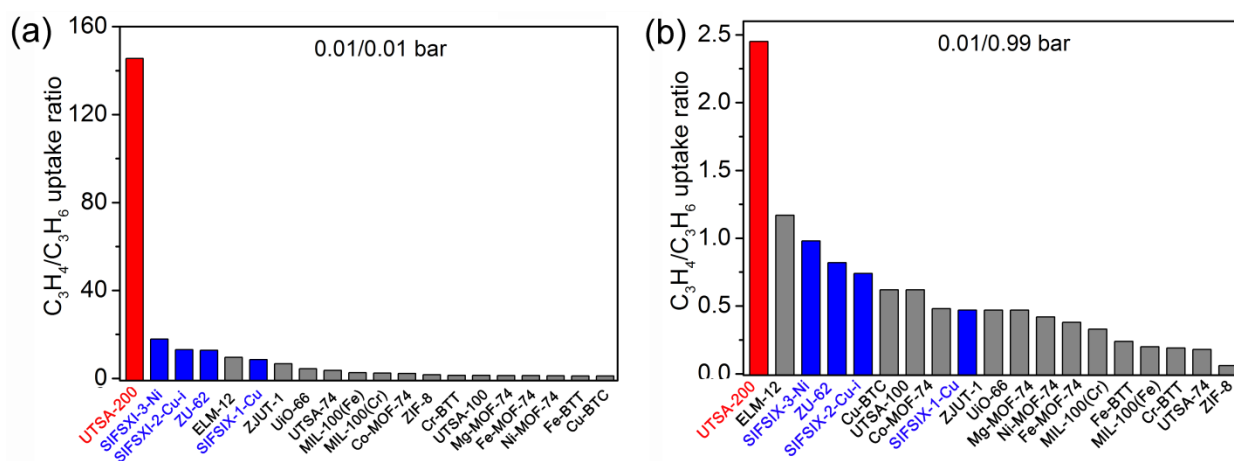
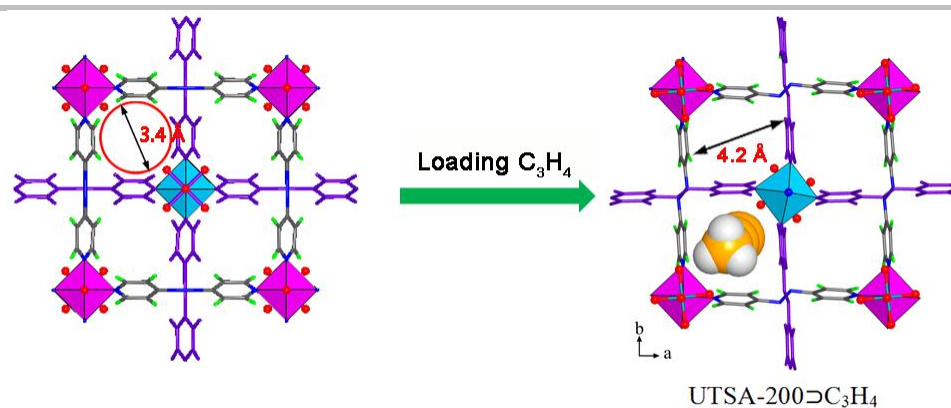


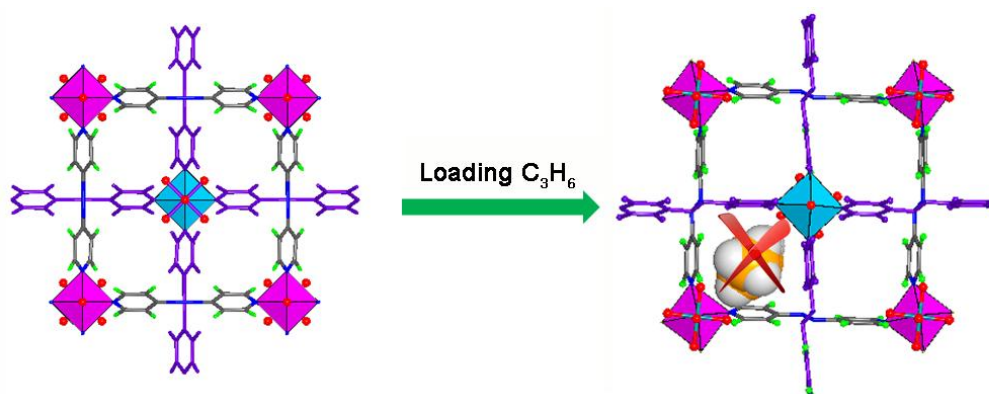
Figure S8. Comparison of  $C_3H_4/C_3H_6$  uptake ratio at 0.01/0.01 bar (a) and 0.01/0.99 bar (b) for UTSA-200 with respect to other top-performing MOF materials as indicated.



## SUPPORTING INFORMATION

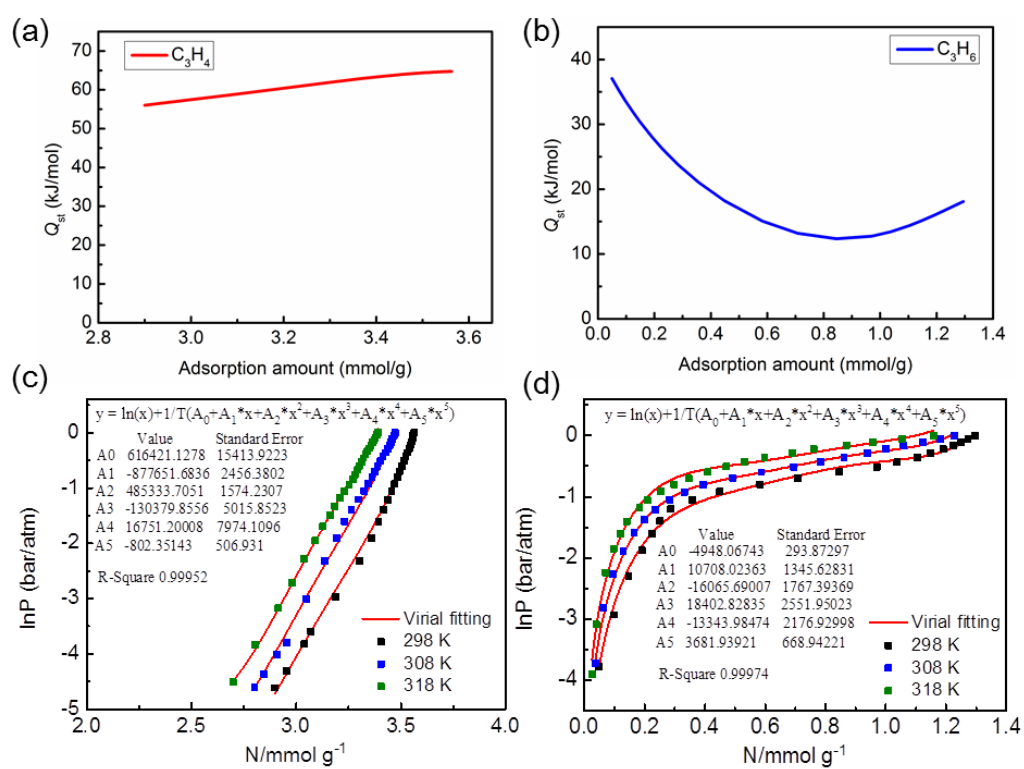


**Figure S9.** DFT-D-calculated C<sub>3</sub>H<sub>4</sub> adsorption configuration in UTSA-200 (right structure), indicating that the N=N bond and pyridine rings on the linker would be rotated and distorted to expand the dynamic pore size from 3.4 Å to 4.2 Å after adsorbing C<sub>3</sub>H<sub>4</sub> molecule. The different net is highlighted in purple for clarity. Color code: Cu (turquoise), Si (dark green), F (red), N (blue), C (grey), and H (green spheres).



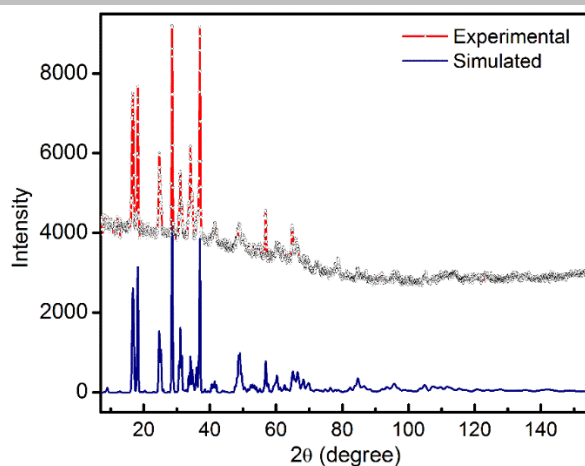
**Figure S10.** Hypothetical C<sub>3</sub>H<sub>6</sub> adsorption configuration in the same framework model with UTSA-200  $\supset$  C<sub>3</sub>H<sub>4</sub> (right structure). It is revealed that the C<sub>3</sub>H<sub>6</sub> molecule would have inevitable space overlapping with the pore walls of UTSA-200, indicating that the pore needs to be expanded more for the passage of C<sub>3</sub>H<sub>6</sub> molecule.

## SUPPORTING INFORMATION

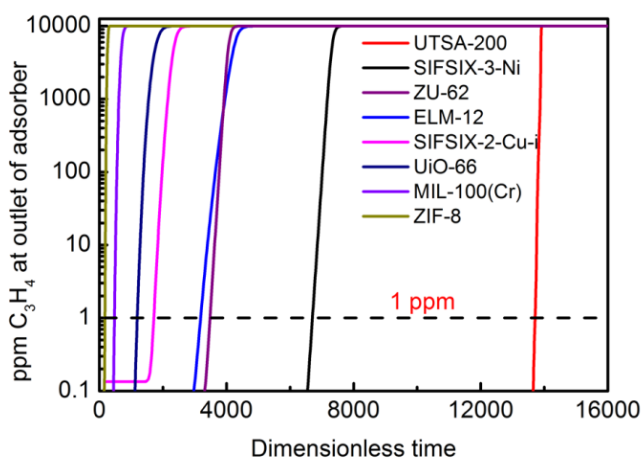


**Figure S11.** Adsorption heat and Virial fitting of the  $C_3H_4$  (a and c) and  $C_3H_6$  (b and d) adsorption isotherms for UTSA-200 (points) at 298 K (black), 308 K (blue), and 318 K (green).

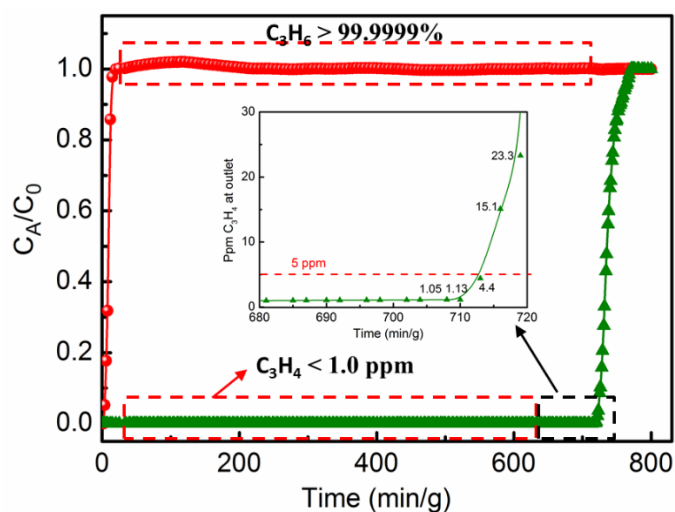
## SUPPORTING INFORMATION



**Figure S12.** Neutron powder diffraction pattern of the  $C_3D_4$ -loaded UTSA-200 along with the simulated pattern based on a model structure built upon the DFT-D calculation results. The agreement between the two is reasonably well..

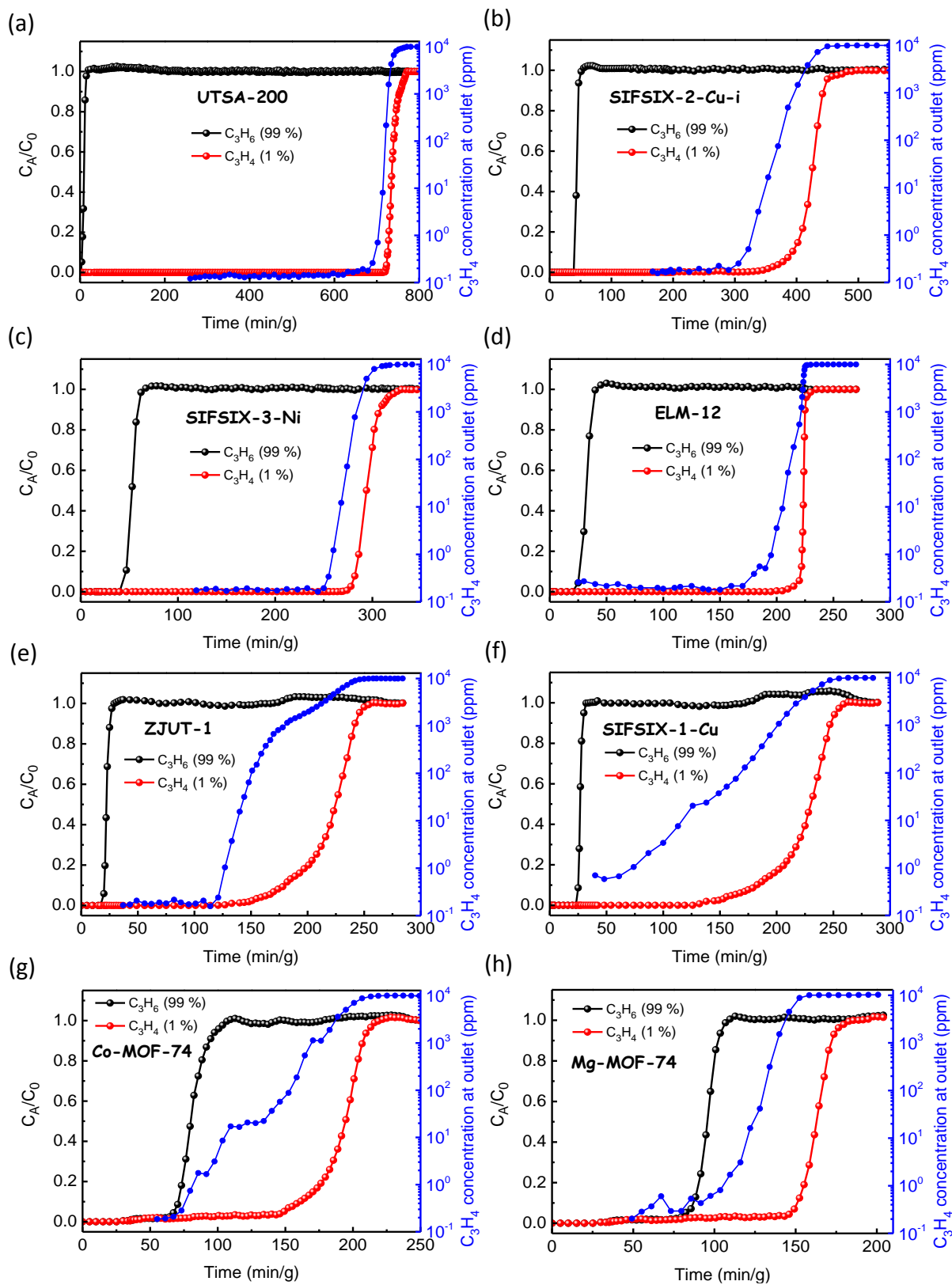


**Figure S13.** Ppm  $C_3H_4$  in the outlet gas of transient breakthrough of  $C_3H_4/C_3H_6$  mixture containing 1%  $C_3H_4$  mixture in an adsorber bed packed with various MOFs. At a certain time,  $\tau_{break}$ , the impurity level will exceed the desired purity level of 1 ppm.

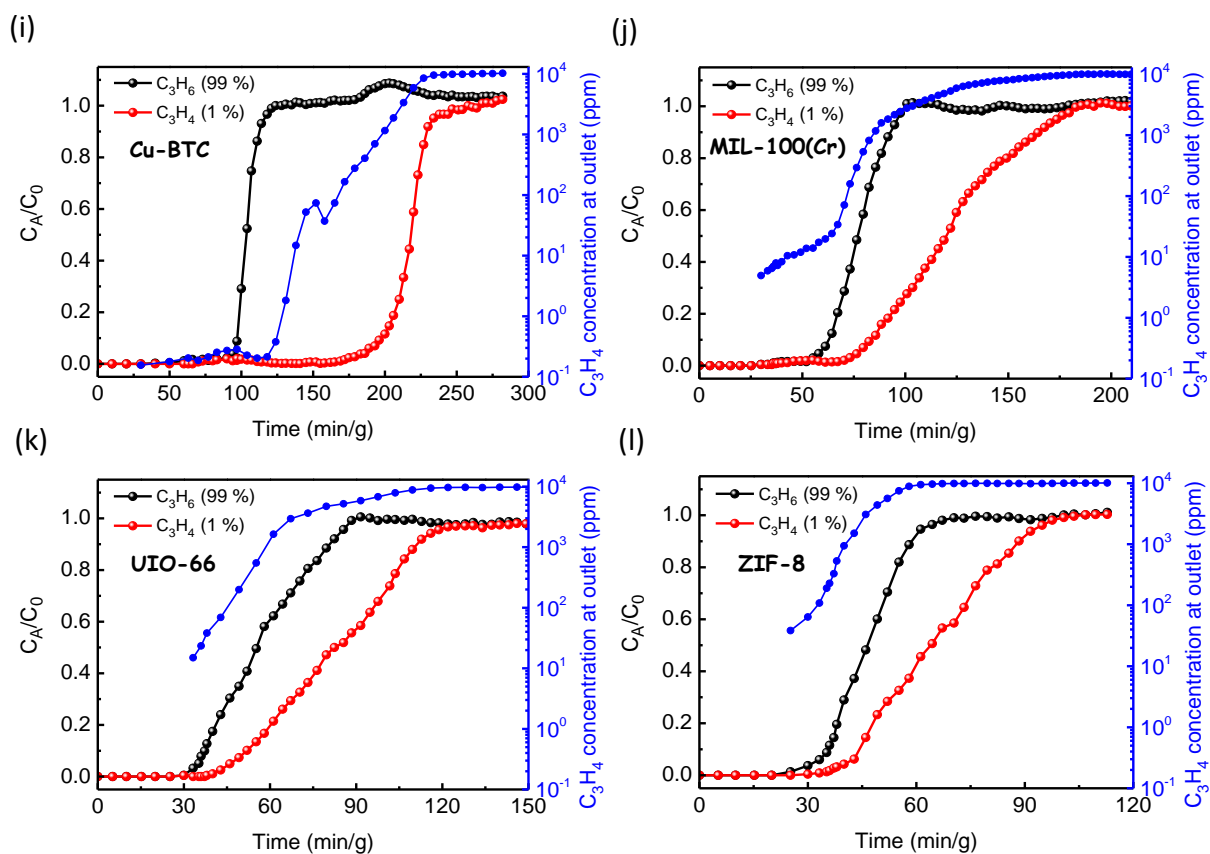


**Figure S14.** The concentration of  $C_3H_4$  and the purity of  $C_3H_6$  in the outlet gas of the adsorber. The inserted figure shows the  $C_3H_4$  content in the outlet gas in ppm. Experimental breakthrough was conducted on a stainless steel column packed with UTSA-200 ( $\Phi$  4x150 mm) with  $C_3H_4/C_3H_6$  mixture (1/99) as feed gas at 2.0 mL/min and 298 K.

## SUPPORTING INFORMATION

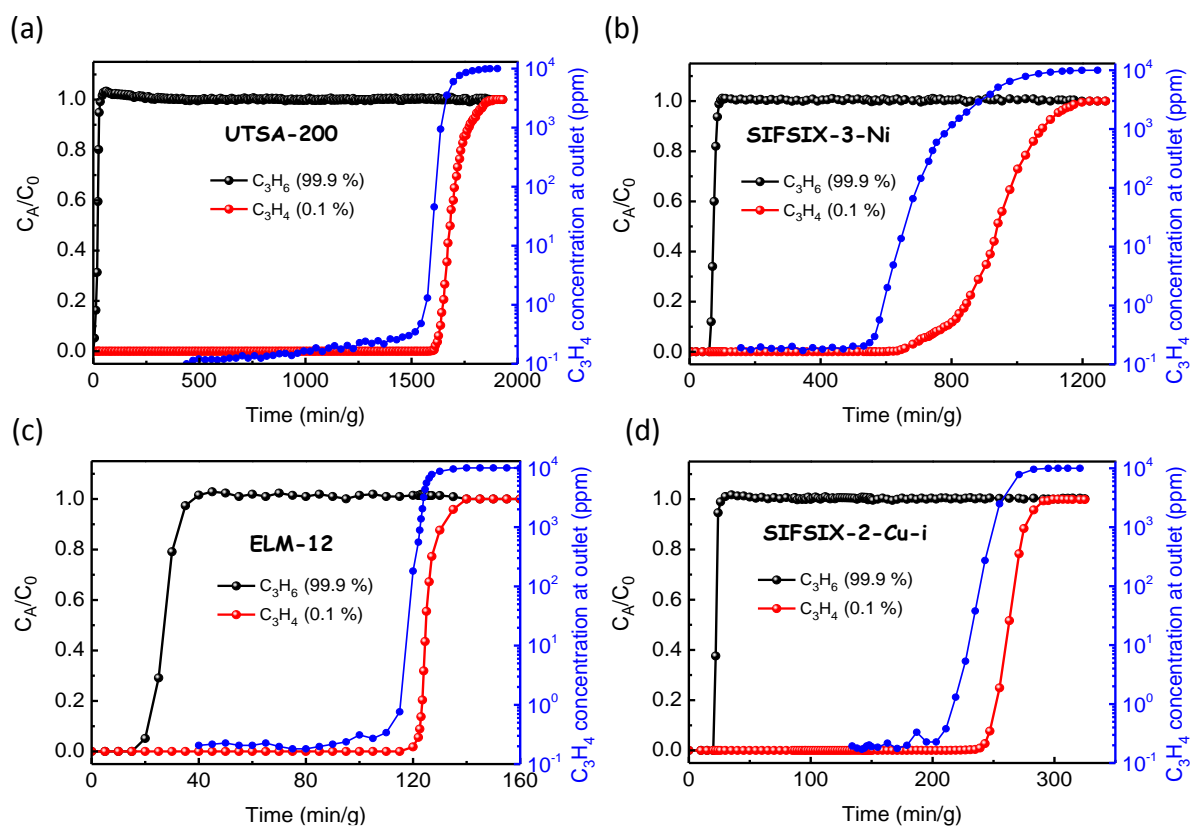


## SUPPORTING INFORMATION



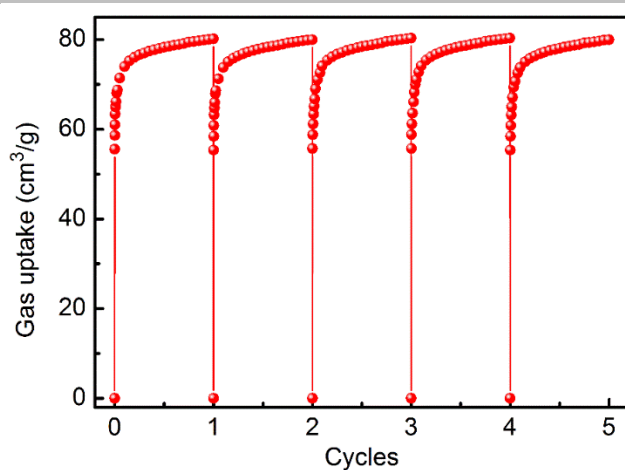
**Figure S15.** Breakthrough curves of the selected MOFs for separation of  $C_3H_4/C_3H_6$  (1/99) mixtures at 298 K and 1.01 bar. Most traditional MOFs cannot meet the requirement for removal low concentration of  $C_3H_4$  (< 1 ppm) from  $C_3H_4/C_3H_6$  (1/99) mixtures.

## SUPPORTING INFORMATION

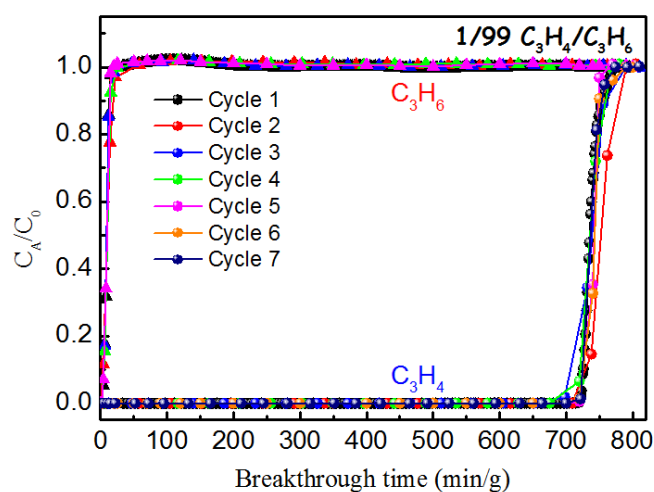


**Figure S16.** Breakthrough curves of the selected MOFs for separation of  $C_3H_4/C_3H_6$  (0.1/99.9) mixture at 298 K and 1.01 bar. These indicated MOFs can remove trace  $C_3H_4$  from  $C_3H_4/C_3H_6$  (0.1/99.9) mixtures to meet the requirement of  $C_3H_4 < 1$  ppm.

## SUPPORTING INFORMATION



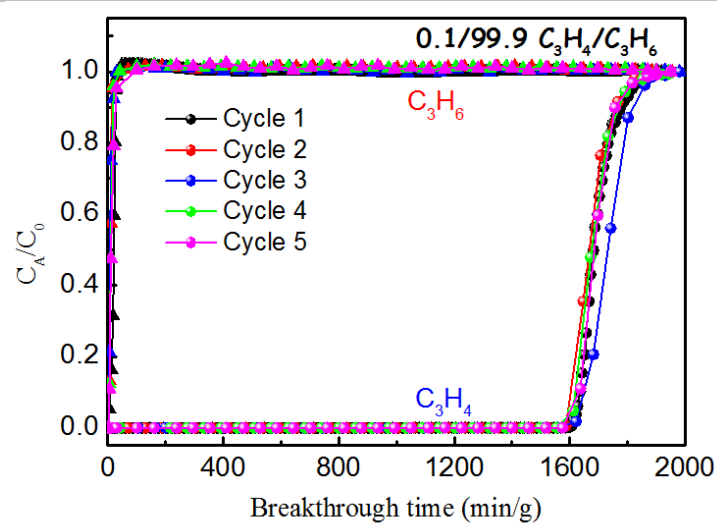
**Figure S17.** Cyclic  $C_3H_4$  adsorption measurements on UTSA-200 at 298 K and 1 bar, indicating that UTSA-200 can maintain its high  $C_3H_4$  uptake capacity over five cycles.



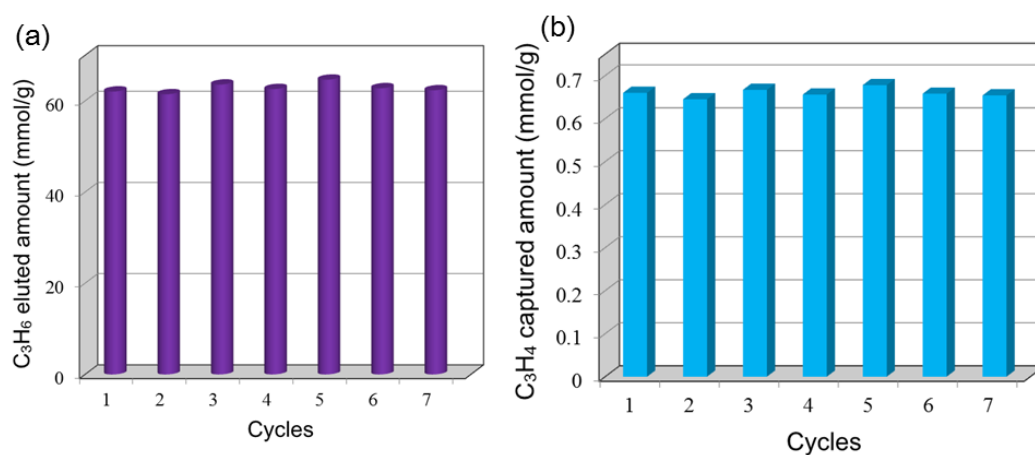
**Figure S18.** Cycling column breakthrough curves for  $C_3H_4/C_3H_6$  (1/99) separations with UTSA-200 at 298 K and 1.01 bar. The breakthrough experiments were carried out in a column packed with UTSA-200 ( $\Phi$  4x150 mm) at a flow rate of 2.0 mL/min.



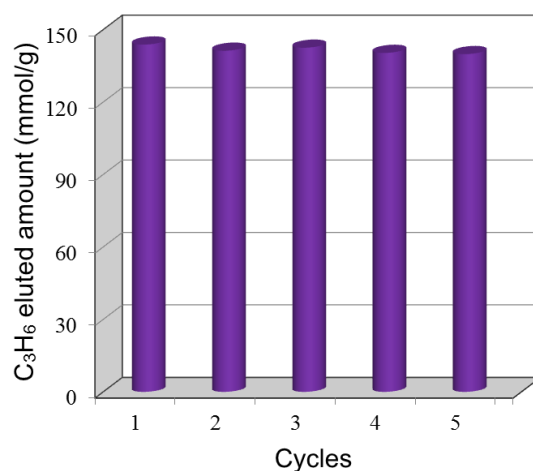
## SUPPORTING INFORMATION



**Figure S19.** Cycling column breakthrough curves for  $C_3H_4/C_3H_6$  (0.1/99.9) separations with UTSA-200 at 298 K and 1.01 bar. The breakthrough experiments were carried out in a column packed with UTSA-200 ( $\Phi$  4x150 mm) at a flow rate of 2.0 mL/min.

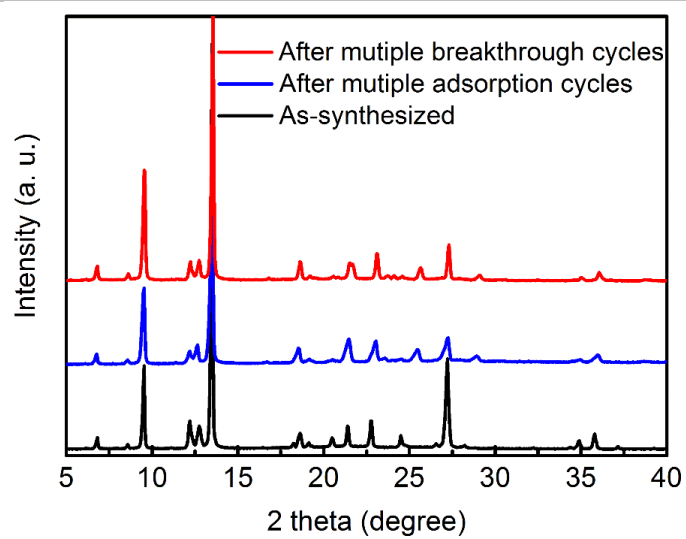


**Figure S20.** Cyclic breakthrough experiments for  $C_3H_4/C_3H_6$  (1/99 v/v) separation on UTSA-200, indicating that UTSA-200 maintained the  $C_3H_6$  eluted amount from the outlet effluent (a) and the  $C_3H_4$  captured amount (b) during the separation processes over at least 7 times.



**Figure S21.** Cyclic breakthrough experiments for  $C_3H_4/C_3H_6$  (0.1/99.9) separation on UTSA-200, indicating that UTSA-200 maintained the  $C_3H_6$  eluted amount during the separation processes over at least 7 times.

## SUPPORTING INFORMATION



**Figure S22.** PXRD patterns of as-synthesized UTSA-200 sample (black) and the samples after the multiple adsorption tests (blue) and breakthrough tests (red).

## SUPPORTING INFORMATION

**Table S1.** The BET surface, pore size and crystal density of the selected MOF materials.

MOF Types	Materials	BET surface (m <sup>2</sup> /g)	Pore size (Å)	Crystal density (g/cm <sup>3</sup> )	Ref.
MOFs with open metal sites	Mg-MOF-74	1415	11	0.920	[8]
	Co-MOF-74	1080	11	1.169	[8]
	Ni-MOF-74	1070	11	1.203	[8]
	Fe-MOF-74	1360	11	1.126	[9]
	UTSA-74	830	8	1.340	[10]
	Cu-BTC	1850	7-10	0.879	[11]
	Cr-BTC	1810	7-10	0.799	[12]
MOFs with high porosities	Fe-BTT	2200	10.3	0.797	[13]
	Cr-BTT	2293	10.3	0.832	[14]
	MIL-100(Cr)	3100	29	0.784	[15]
	MIL-100(Fe)	2800	32	1.064	[16]
Small-pore MOFs	UIO-66	1390	6	1.198	[17]
	ZIF-8	1630	3.5	1.067	[18]
	UTSA-100	970	4.0	1.146	[19]
	ZJUT-1	222	3.7	1.738	[20]
MOFs with strong functional sites	SIFSIX-1-Cu	1178	8.0	0.864	[21]
	SIFSIX-2-Cu-i	735	4.4	1.247	[22]
	SIFSIX-3-Ni	250	4.2	1.570	[23]
	UTSA-200	612	3.4	1.417	[24]
	ELM-12	740	4.3	1.406	[25]
	ZU-62	476	3.2	1.378	[26]

Note: the crystal density of UTSA-200 used for the unit conversion is based on the activated framework. Although the structure of UTSA-200 would be changed upon gas adsorption (mainly originated from the rotation of pyridine rings), this change is very tiny that would have a negligible impact on the crystal density, as supported by the very similar cell parameters between the activated UTSA-200 ( $a = b = 13.0469$ ,  $c = 7.9013$ ;  $\alpha = \beta = \gamma = 90.00$ )<sup>[24]</sup> and UTSA-200  $\rightarrow$  C<sub>3</sub>H<sub>4</sub> model ( $a = b = 13.0600$ ,  $c = 8.0680$ ;  $\alpha = \beta = \gamma = 90.00$ ).

## SUPPORTING INFORMATION

**Table S2.** Comparison of C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> uptake (mmol/g, mmol/cm<sup>3</sup> and cm<sup>3</sup>/cm<sup>3</sup>) from gas adsorption isotherms at various pressures, and the C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> uptake ratio at 0.01/0.01 bar and 0.01/0.99 bar for various MOF materials at 298 K.

MOFs	C <sub>3</sub> H <sub>4</sub> adsorption (mmol g <sup>-1</sup> /mmol cm <sup>-3</sup> /cm <sup>3</sup> cm <sup>-3</sup> )			C <sub>3</sub> H <sub>6</sub> adsorption (mmol g <sup>-1</sup> /mmol cm <sup>-3</sup> /cm <sup>3</sup> cm <sup>-3</sup> )			C <sub>3</sub> H <sub>4</sub> /C <sub>3</sub> H <sub>6</sub> adsorption ratio	
	0.01 bar	0.1 bar	0.99 bar	0.01 bar	0.4 bar	0.99 bar	0.01/0.01	0.01/0.99
<b>UTSA-200</b>	<b>2.99/4.24/95</b>	<b>3.30/4.68/105</b>	<b>3.58/5.07/114</b>	<b>0.02/0.03/0.67</b>	<b>0.33/0.47/10.5</b>	<b>1.20/1.70/38.0</b>	<b>149.5</b>	<b>2.49</b>
SIFSIX-3-Ni	2.56/4.02/90	2.73/4.29/96	2.85/4.47/100	0.15/0.24/5.3	2.42/3.80/85.1	2.72/4.27/95.6	17.87	0.98
ZU-62	2.19/3.02/68	3.01/4.15/93	3.64/5.02/112	0.17/0.23/5.2	2.26/3.11/69.7	2.67/3.68/82.4	12.9	0.82
SIFSIX-2-Cu-i	1.96/2.44/55	3.22/4.01/90	3.77/4.70/105	0.15/0.19/4.3	2.19/2.73/61.2	2.63/3.28/73.5	13.07	0.74
SIFSIX-1-Cu	2.57/2.22/50	6.79/5.87/131	8.63/7.46/167	0.30/0.26/5.8	4.92/4.25/95.2	5.88/5.08/113.8	8.54	0.44
ELM-12	1.82/2.56/57	2.54/3.57/80	2.77/3.89/87	0.19/0.27/6.0	1.11/1.56/35.0	1.43/2.01/45.0	9.57	1.27
ZJUT-1	0.40/0.69/15	1.07/1.86/42	2.24/3.89/87	0.06/0.10/2.24	0.54/0.94/21.0	0.84/1.46/32.7	6.67	0.47
Mg-MOF-74	2.71/2.49/56	7.32/6.73/151	9.40/8.65/194	2.03/1.87/41.9	6.07/5.58/125.0	6.49/5.97/133.7	1.33	0.42
Co-MOF-74	2.85/3.33/75	5.80/6.78/152	7.47/8.73/196	1.27/1.48/33.2	5.64/6.59/147.6	5.95/6.96/155.9	2.24	0.48
Ni-MOF-74	1.80/2.16/48	4.68/5.63/126	5.51/6.63/149	1.53/1.84/41.2	4.50/5.41/121.2	4.78/5.75/128.8	1.18	0.38
Fe-MOF-74	2.18/2.45/55	6.67/7.51/168	7.94/8.94/200	1.67/1.88/42.1	6.25/7.04/157.7	6.63/7.47/167.3	1.31	0.33
Cu-BTC	1.47/1.29/29	8.17/7.18/161	10.47/9.20/206	1.36/1.19/26.7	7.90/6.94/155.4	8.33/7.32/164.0	1.08	0.18
Fe-BTT	1.74/1.32/30	6.87/5.20/117	12.41/9.39/210	1.52/1.15/25.8	8.03/6.08/136.2	8.74/6.62/148.3	1.14	0.20
Cr-BTT	1.08/0.82/18	4.42/3.34/75	7.28/5.51/123	0.76/0.58/13.0	5.04/3.81/85.3	5.85/4.43/99.2	1.42	0.18
MIL-100(Cr)	1.52/1.11/25	4.98/3.64/82	14.51/10.62/238	0.63/0.46/10.3	4.53/3.32/74.4	6.25/4.58/102.6	2.41	0.24
MIL-100(Fe)	1.34/0.98/22	4.74/3.47/78	17.14/12.55/281	0.52/0.38/8.5	4.52/3.31/74.1	6.96/5.09/114.0	2.58	0.19
UIO-66	1.58/1.89/42	5.29/6.34/142	10.23/12.26/275	0.36/0.43/9.6	2.70/3.23/72.3	3.33/3.99/89.4	4.39	0.47
ZIF-8	0.13/0.14/3.1	1.44/1.54/35	6.27/6.69/150	0.08/0.09/2.0	3.15/3.36/75.3	4.07/4.34/97.2	1.62	0.03
UTSA-74-Zn	0.33/0.44/9.8	2.13/2.85/64	7.43/9.96/223	0.09/0.12/2.7	2.47/3.31/74.1	5.07/6.79/152.1	3.67	0.06
UTSA-100	1.87/2.14/48	4.01/4.59/103	5.35/6.13/137	1.34/1.54/34.5	2.68/3.07/68.8	3.04/3.48/77.9	1.40	0.62

## SUPPORTING INFORMATION

**Table S3.** Dual-Langmuir-Freundlich fitting parameters for C<sub>3</sub>H<sub>4</sub>, and C<sub>3</sub>H<sub>6</sub> in UTSA-200.

	Site A				Site B			
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_A</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>v_B</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	0.8	2.53E-14	56	1	2.8	4.36E-07	30.6	1
C <sub>3</sub> H <sub>6</sub>	1.9	1.91E-15	17	0.33	1.56	2.49E-28	92	2.44

**Table S4.** Dual-Langmuir-Freundlich fitting parameters for C<sub>3</sub>H<sub>4</sub>, and C<sub>3</sub>H<sub>6</sub> in SIFSIX-3-Ni.

	Site A				Site B			
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_A</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>v_B</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	0.6	6.72E-08	27	0.42	2.65	2.52E-12	48	2
C <sub>3</sub> H <sub>6</sub>	2.8	2.71E-13	43	1.27	0.12	3.42E-05	49	1

**Table S5.** Dual-Langmuir-Freundlich fitting parameters for C<sub>3</sub>H<sub>4</sub>, and C<sub>3</sub>H<sub>6</sub> in SIFSIX-2-Cu-i.

	Site A				Site B			
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_A</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>v_B</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	3.9	1.18E-05	10.3	1.08	2.1	1.01E-07	23.2	0.5
C <sub>3</sub> H <sub>6</sub>	2.2	4.63E-10	32	1	1.8	6.76E-12	36	1

**Table S6.** Dual-Langmuir-Freundlich fitting parameters for C<sub>3</sub>H<sub>4</sub>, and C<sub>3</sub>H<sub>6</sub> in ELM-12.

	Site A				Site B			
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_A</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>v_B</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	2.2	2.07E-05	5	1.45	1.2	4.47E-12	52	0.45
C <sub>3</sub> H <sub>6</sub>	1.5	6.62E-12	36	1	0.6	1.46E-6	14	1

**Table S7.** Dual-Langmuir-Freundlich fitting parameters for C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> in SIFSIX-1-Cu.

	Site A			Site B		
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_A$ Pa <sup>-<math>v_A</math></sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_B$ Pa <sup>-<math>v_B</math></sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	6.6	2.21E-02	0.39	4.2	1.54E-6	2
C <sub>3</sub> H <sub>6</sub>	5.7	2.76E-3	0.5	2.9	7.43E-13	3.2

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**Table S8.** Dual-Langmuir-Freundlich fitting parameters for C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> in UIO-66.

	Site A				Site B			
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_A</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>v_B</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	8	2.02E-08	19	1	3.8	1.01E-06	15	1
C <sub>3</sub> H <sub>6</sub>	2.5	9.13E-11	35.5	1	2.3	2.70E-11	31	1

**Table S9.** Dual-Langmuir-Freundlich fitting for C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> in MIL-100(Cr).

	Site A				Site B			
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_A</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>v_B</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	18.5	4.19E-08	15.7	1	1.7	4.52E-07	20	1
C <sub>3</sub> H <sub>6</sub>	8.2	2.95E-10	27	1	1.3	4.25E-08	25	1

**Table S10.** Dual-Langmuir-Freundlich fitting parameters for C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> in ZIF-8.

	Site A				Site B			
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_A</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>v_B</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	5.9	1.47E-10	28.6	1	3	1.59E-15	41	1.8
C <sub>3</sub> H <sub>6</sub>	4.9	2.28E-13	38	1.35	0.3	6.00E-19	29	0.75

**Table S11.** Dual-Langmuir-Freundlich fitting parameters for C<sub>3</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> in Cu-BTC.

	Site A				Site B			
	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_A</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless	$q_{B,sat}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>v_B</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$v_B$ dimensionless
C <sub>3</sub> H <sub>4</sub>	20	4.55E-04	7.2	0.44	5.5	9.58E-11	23	2
C <sub>3</sub> H <sub>6</sub>	1.4	4.81E-12	36	1	8.7	2.79E-08	27	1

## SUPPORTING INFORMATION

**Table S12.** Breakthrough calculations for separation of C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> (1/99) mixture at 298 K.

	Separation potential $\Delta Q$ (mol/L)	Breakthrough productivity of C <sub>3</sub> H <sub>6</sub> (mol/L)
<b>UTSA-200</b>	<b>404.5</b>	<b>367.2</b>
SIFSIX-3-Ni	210.1	182.2
ZU-62	118.9	92.8
SIFSIX-2-Cu-i	64.8	47.7
ELM-12	121.2	92.2
Cu-BTC	18.7	/
MIL-100(Cr)	15.8	9.9
UIO-66	47.4	31.8
ZIF-8	3.6	1.6

**Table S13.** Comparisons of the breakthrough columns parameters studied in this work.

	Sample weight (g)	Crystal density (g/cm <sup>3</sup> )	Packing density <sup>[a]</sup> (g/cm <sup>3</sup> )	Column voidage <sup>[b]</sup>	Column free space (cm <sup>3</sup> ) <sup>[c]</sup>
UTSA-200	<b>2.028</b>	<b>1.417</b>	<b>1.152</b>	<b>0.187</b>	<b>0.329</b>
SIFSIX-3-Ni	2.411	1.570	1.430	0.192	0.338
SIFSIX-2-Cu-i	2.054	1.247	1.167	0.180	0.317
ELM-12	2.017	1.406	1.146	0.185	0.326
ZJUT-1	2.360	1.738	1.401	0.194	0.341
Cu-BTC	1.197	0.879	0.692	0.213	0.375
Co-MOF-74	1.466	1.169	0.927	0.207	0.364
Mg-MOF-74	1.302	0.920	0.740	0.195	0.342
SIFSIX-1-Cu	1.258	0.864	0.706	0.183	0.322
MIL-100(Cr)	1.034	0.732	0.588	0.196	0.345
UIO-66	1.723	1.198	0.979	0.183	0.322
ZIF-8	1.387	1.067	0.830	0.222	0.391

[a] Packing density = Sample weight/Column volume

[b] Column voidage = 1 - Sample weight/Crystal density/Column volume

[c] Column free space = Column volume × Column voidage



## SUPPORTING INFORMATION

**Table S14.** Comparisons of C<sub>3</sub>H<sub>6</sub> productivities in a single breakthrough operation using C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> (1/99) mixture as input.

	Crystal density (g/cm <sup>3</sup> )	Gravimetric/Volumetric Productivity (mmol/g and mmol/cm <sup>3</sup> ) with different purities	
		C <sub>3</sub> H <sub>6</sub> (C <sub>3</sub> H <sub>4</sub> < 1 ppm)	C <sub>3</sub> H <sub>6</sub> (C <sub>3</sub> H <sub>4</sub> < 5 ppm)
UTSA-200	1.417	<b>62.05 / 87.92</b>	<b>62.94 / 89.19</b>
SIFSIX-3-Ni	1.570	19.02 / 33.66	19.60 / 34.69
SIFSIX-2-Cu-i	1.247	26.34 / 37.48	27.68 / 39.39
ELM-12	1.406	15.36 / 21.60	15.80 / 22.21
ZJUT-1	1.738	17.86 / 31.04	19.28 / 33.51
Cu-BTC	0.879	2.77 / 2.43	2.91 / 2.56
Co-MOF-74	1.169	2.11 / 2.47	2.32 / 2.71
Mg-MOF-74	0.920	1.78 / 1.64	2.47 / 2.27
SIFSIX-1-Cu	0.864	4.46 / 3.85	6.69 / 5.78
MIL-100(Cr)	0.732	NA	NA
UIO-66	1.198	NA	NA
ZIF-8	1.067	NA	NA

**Table S15.** Comparisons of C<sub>3</sub>H<sub>6</sub> productivities in a single breakthrough operation using C<sub>3</sub>H<sub>4</sub>/C<sub>3</sub>H<sub>6</sub> (0.1/99.9) mixture as input.

	Crystal density (g/cm <sup>3</sup> )	Gravimetric/Volumetric Productivity (mmol/g and mmol/cm <sup>3</sup> ) with different purities	
		C <sub>3</sub> H <sub>6</sub> (C <sub>3</sub> H <sub>4</sub> < 1 ppm)	C <sub>3</sub> H <sub>6</sub> (C <sub>3</sub> H <sub>4</sub> < 5 ppm)
UTSA-200	1.417	<b>142.86 / 202.43</b>	<b>143.75 / 203.69</b>
SIFSIX-3-Ni	1.570	47.32 / 83.76	49.11 / 86.92
SIFSIX-2-Cu-i	1.247	8.48 / 12.07	8.75 / 12.45
ELM-12	1.406	17.86 / 25.11	18.93 / 26.62

## SUPPORTING INFORMATION

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## Author Contributions

J.L., B.L., and B.C. contributed to conceive and design the experiments. L.L., H.M.W., and B.L. synthesized the compounds and collected the gas adsorption data. L.L., R.B.L., B.L., and B.C. analyzed all adsorption data. R.K. conducted IAST calculations and transient breakthrough simulations. H.W. and W.Z. collected and analyzed the powder X-ray diffraction data. H.W. and W.Z. performed the first-principles DFT-D calculations and neutron diffraction. L.L., C.H., and B.L. collected the experimental breakthrough data. L.L., B.L., and B.C. analyzed the data and wrote the manuscript. All authors discussed the results and commented on the manuscript.