

# Engineering Pore Environments of Sulfate-Pillared Metal-Organic Framework for Efficient C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> Separation with Record Selectivity

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Engineering pore environments exhibit great potential in improving gas adsorption and separation performances but require specific means for acetylene/carbon dioxide (C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub>) separation due to their identical dynamic diameters and similar properties. Herein, a novel sulfate-pillared MOF adsorbent (SOFOUR-TEPE-Zn) using 1,1,2,2-tetra(pyridin-4-yl) ethene (TEPE) ligand with dense electronegative pore surfaces is reported. Compared to the prototype SOFOUR-1-Zn, SOFOUR-TEPE-Zn exhibits a higher C<sub>2</sub>H<sub>2</sub> uptake (89.1 cm<sup>3</sup> g<sup>-1</sup>), meanwhile the CO<sub>2</sub> uptake reduces to 14.1 cm<sup>3</sup> g<sup>-1</sup>, only 17.4% of that on SOFOUR-1-Zn (81.0 cm<sup>3</sup> g<sup>-1</sup>). The high affinity toward C<sub>2</sub>H<sub>2</sub> than CO<sub>2</sub> is demonstrated by the benchmark C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> selectivity (16 833). Furthermore, dynamic breakthrough experiments confirm its application feasibility and good cyclability at various flow rates. During the desorption cycle, 60.1 cm<sup>3</sup> g<sup>-1</sup> C<sub>2</sub>H<sub>2</sub> of 99.5% purity or 33.2 cm<sup>3</sup> g<sup>-1</sup> C<sub>2</sub>H<sub>2</sub> of 99.99% purity can be recovered by stepped purging and mild heating. The simulated pressure swing adsorption processes reveal that 75.5 cm<sup>3</sup> g<sup>-1</sup> C<sub>2</sub>H<sub>2</sub> of 99.5+% purity with a high gas recovery of 99.82% can be produced in a counter-current blowdown process. Modeling studies disclose four favorable adsorption sites and dense packing for C<sub>2</sub>H<sub>2</sub>.

## 1. Introduction

High-purity acetylene (>99%) is an essential raw material for manufacturing chemical commodities such as vinyl and acrylate polymers.<sup>[1]</sup> In industry, acetylene (C<sub>2</sub>H<sub>2</sub>) is commonly produced by partial combustion of methane or thermal cracking of hydrocarbons, wherein carbon dioxide (CO<sub>2</sub>) unavoidably coexists and impairs the subsequent utilization efficiency.<sup>[2]</sup> The separation of C<sub>2</sub>H<sub>2</sub> from C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> gas-mixtures prevalently relies on cryogenic distillations associating high energy input owing to their close boiling points (189.3 K for C<sub>2</sub>H<sub>2</sub> and 194.7 K for CO<sub>2</sub>).<sup>[3,4]</sup> In contrast, adsorption technology employing porous adsorbents emerges as a promising alternative for light hydrocarbon separations that can operate at ambient conditions achieving high energy efficiency.<sup>[4,5]</sup> Nevertheless, adsorptive separation of C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> gas-mixture is recognized as one of the most challenging systems because of their identical kinetic molecular sizes (3.3 Å) and similar molecular polarizability (33.3 × 10<sup>25</sup> cm<sup>3</sup> for C<sub>2</sub>H<sub>2</sub> and 29.1 × 10<sup>25</sup> cm<sup>3</sup> for CO<sub>2</sub>).<sup>[6]</sup> Over the

last decade, metal-organic frameworks (MOFs) have shown considerable progress in hydrocarbon separations due to their structural designability and tunability on pore size/shape and functionality.<sup>[7–10]</sup> Exposing open metal sites (OMSs) is the general approach to recognizing C<sub>2</sub>H<sub>2</sub> over CO<sub>2</sub> and thus achieving improved C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> separation performances, as demonstrated in ZJU-74a,<sup>[11]</sup> MOF-74,<sup>[12]</sup> ATC-Cu,<sup>[13]</sup> and NKMOF-1-Ni.<sup>[14]</sup> Although relatively large C<sub>2</sub>H<sub>2</sub> uptakes can be obtained in this type of MOFs, enhanced CO<sub>2</sub> adsorptions concurrently occur due to electrostatic interactions, generating moderate C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> selectivity.<sup>[15]</sup> For example, the highest C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> selectivity of 185.0 on MOFs with OMSs was reported on Cu<sup>I</sup>@UiO-66-(COOH)<sub>2</sub>.<sup>[16]</sup> Recently, several flexible MOFs have realized significantly high C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> selectivity exploiting the differences in guest-host interactions and gate-open pressures.<sup>[17–19]</sup> But, in fixed adsorption columns, the possible co-adsorption will generate low-purity C<sub>2</sub>H<sub>2</sub> product in the recovery process.<sup>[20]</sup>

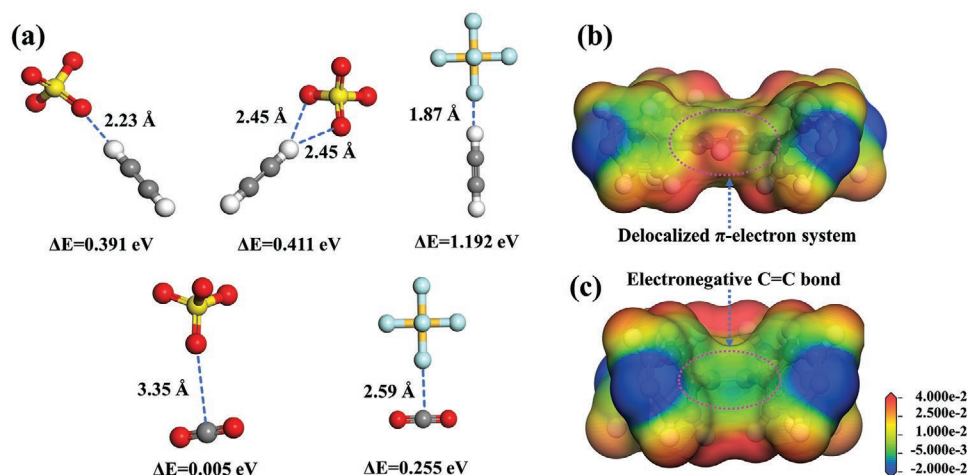
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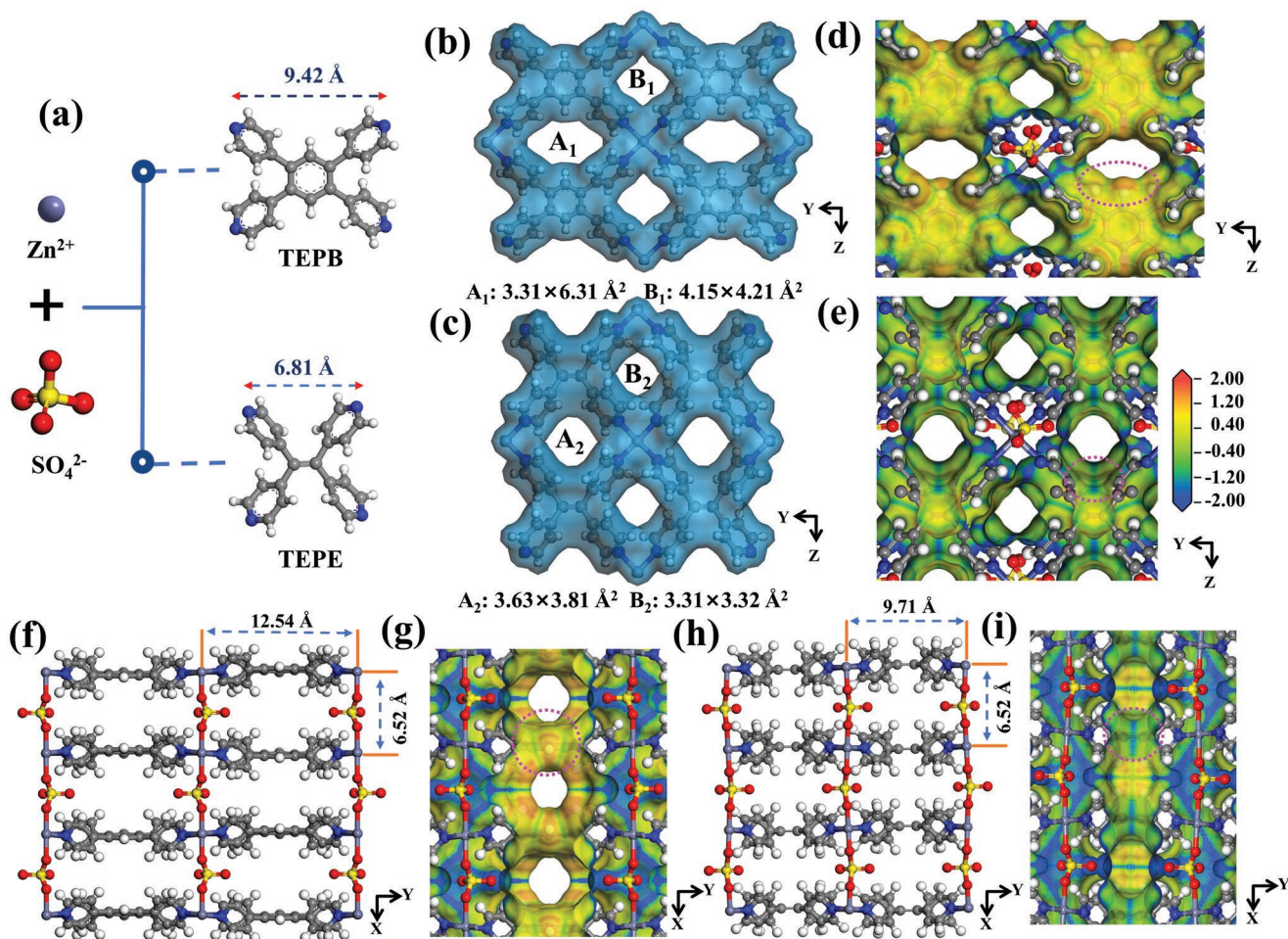
**Figure 1.** a) DFT calculated adsorption energies for  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  on  $\text{SO}_4^{2-}$  and  $\text{SiF}_6^{2-}$  anions. The molecular electrostatic potential (MESP) mapping for b) TEPB and c) TEPE organic ligands.

Given the opposite electrostatic potentials of  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  molecules (Figure S2, Supporting Information), constructing negative pore environments forms electrostatic interactions to the  $\pi$ -electrons and hydrogen bonding to the acidic and positively-charged H atoms on  $\text{C}_2\text{H}_2$ .<sup>[21]</sup> Meanwhile, the electro-induced repulsion impedes the entrance of  $\text{CO}_2$  with negatively-charged ends.<sup>[22]</sup> By incorporating electronegative hydrogen-bonding acceptors such as open oxygen and fluoride sites, some MOF adsorbents showed enhanced  $\text{C}_2\text{H}_2$  capacity but with high adsorption enthalpy over  $50 \text{ kJ mol}^{-1}$ , making  $\text{C}_2\text{H}_2$  recovery and adsorbent regeneration processes energy-intensive.<sup>[6,23]</sup> To solve this problem, less negatively-charged halogen and boron atoms were incorporated to further discriminate  $\text{C}_2\text{H}_2$  over  $\text{CO}_2$ .<sup>[24,25]</sup> Compared to MOFs with fluorinated anions ( $\text{SiF}_6^{2-}$ ,  $\text{TiF}_6^{2-}$ ,  $\text{GeF}_6^{2-}$ , etc.), [Cu(TMBP)X] (TMBP = 3,3',5,5'-tetramethyl-4,4'-bipyrazole; X = Cl, Br, I),<sup>[25]</sup> and ZNU-1 [CuB<sub>12</sub>H<sub>12</sub>(dpe)<sub>2</sub>] (dpe = 1,2-di(4-pyridyl) ethylene)<sup>[24]</sup> exhibited moderate  $\text{C}_2\text{H}_2/\text{CO}_2$  selectivity of 16.9 and 56.6, respectively. Recently, our group demonstrated a novel Hofmann-type MOF adsorbent with negatively-charged pore environments, [Cu(NP)(bpy)] (NP = nitroprusside, bpy = 4,4'-bipyridine), showing leading  $\text{C}_2\text{H}_2/\text{CO}_2$  selectivity of 47.2 among rigid MOFs.<sup>[22]</sup> Note that tuning the charge distributions on pore surfaces can also reverse the adsorption precedence that favorably adsorbs  $\text{CO}_2$  over  $\text{C}_2\text{H}_2$ .<sup>[26–28]</sup> Despite the power of this strategy, elaborated modification and adjustment of pore environments are necessitated for constructing efficient MOF adsorbents with high  $\text{C}_2\text{H}_2$  capacity and  $\text{C}_2\text{H}_2/\text{CO}_2$  selectivity.<sup>[29,30]</sup>

Zaworotko's group reported the first sulfate-pillared hybrid ultramicroporous material, SOFOUR-1-Zn, [Zn(tepb)( $\text{SO}_4^{2-}$ )]<sub>n</sub> (TEPB = tetra(4-pyridyl)benzene, Figure S3a, Supporting Information), which showed smaller pore sizes with periodically expanded and contracted apertures by implanting shorter tetrahedral  $\text{SO}_4^{2-}$  rather than hexahedral  $\text{SiF}_6^{2-}$  anions.<sup>[31]</sup> Unfortunately, SOFOUR-1-Zn exhibited a lower uptake for  $\text{C}_2\text{H}_2$  ( $69.4 \text{ cm}^3 \text{ g}^{-1}$ ) than  $\text{CO}_2$  ( $81.0 \text{ cm}^3 \text{ g}^{-1}$ ) at 1 bar, rendering a relatively low  $\text{C}_2\text{H}_2/\text{CO}_2$  selectivity of 6.6. We further conducted density functional theory (DFT) calculations for adsorption

energies of  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  on  $\text{SO}_4^{2-}$  and  $\text{SiF}_6^{2-}$  anions. As shown in Figure 1a,  $\text{SO}_4^{2-}$  anion could interact with  $\text{C}_2\text{H}_2$  with two configurations but show lower binding energy than  $\text{SiF}_6^{2-}$  anion. It is worth noting that  $\text{SO}_4^{2-}$  anion displays negligible interaction for  $\text{CO}_2$  with a binding energy of 0.005 eV compared to  $\text{SiF}_6^{2-}$  (0.255 eV). Although these results seem contradictory to the adsorption capacity of  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  on SOFOUR-1-Zn, further highlighting that judicious choice of organic ligands also determines  $\text{C}_2\text{H}_2/\text{CO}_2$  separation performances by impacting electro-environments on pore surfaces.<sup>[32]</sup> The center benzene ring in TEPB ligand contains delocalized  $\pi$ -electron systems that can accept or donate electrons (Figure 1b and Figure S3a, Supporting Information), thus we speculate that replacing the benzene ring with higher electronegative moieties will significantly enhance  $\text{C}_2\text{H}_2$  adsorption while remaining low  $\text{CO}_2$  uptake in sulfate-pillared MOFs.

Herein, we report a novel sulfate-pillared MOF adsorbent using 1,1,2,2-tetra(pyridin-4-yl) ethene (TEPE) ligand with higher electronegative ethylene linkage (C=C, Figure 1c and Figure S3b, Supporting Information). As a result, the obtained SOFOUR-TEPE-Zn, [Zn(TEPE)( $\text{SO}_4^{2-}$ )]<sub>n</sub>, shows more electron-rich pore surfaces than the prototype SOFOUR-1-Zn, rendering a higher  $\text{C}_2\text{H}_2$  uptake ( $89.1 \text{ cm}^3 \text{ g}^{-1}$ ) than that of SOFOUR-1-Zn ( $69.4 \text{ cm}^3 \text{ g}^{-1}$ ). Noticeably, the  $\text{CO}_2$  adsorption capacity significantly reduces to  $14.1 \text{ cm}^3 \text{ g}^{-1}$  on SOFOUR-TEPE-Zn, which is only 17.4% to that of SOFOUR-1-Zn ( $81.0 \text{ cm}^3 \text{ g}^{-1}$ ). The high affinity toward  $\text{C}_2\text{H}_2$  than  $\text{CO}_2$  is further demonstrated by the benchmark  $\text{C}_2\text{H}_2/\text{CO}_2$  (50:50, v/v) selectivity (16833) at ambient conditions. Furthermore, dynamic breakthrough experiments with equimolar  $\text{C}_2\text{H}_2/\text{CO}_2$  gas-mixtures confirm the application feasibility and good cyclability of SOFOUR-TEPE-Zn. During the desorption cycle,  $60.1 \text{ cm}^3 \text{ g}^{-1}$   $\text{C}_2\text{H}_2$  of 99.5% purity or  $33.2 \text{ cm}^3 \text{ g}^{-1}$   $\text{C}_2\text{H}_2$  of 99.99% purity can be recovered from a single adsorption column by stepped purging and mild heating. The simulated pressure swing adsorption (PSA) processes reveal that  $75.5 \text{ cm}^3 \text{ g}^{-1}$   $\text{C}_2\text{H}_2$  of 99.5%+ purity with a high recovery of 99.82% could be recovered in counter-current blowdown process. Modeling studies disclose four favorable adsorption sites for  $\text{C}_2\text{H}_2$ , which are missing for  $\text{CO}_2$ .



**Figure 2.** a) The building blocks of SOFOUR-1-Zn and SOFOUR-TEPE-Zn. Structure of SOFOUR-1-Zn viewed along the b) X-axes and f) Z-axes. Structure of SOFOUR-TEPE-Zn viewed along the c) X-axes and h) Z-axes. The Electrostatic surface potential of d, g) SOFOUR-1-Zn and e, i) SOFOUR-TEPE-Zn.

## 2. Results and Discussion

### 2.1. Sample Synthesis and Characterizations

The reaction of equal molar  $ZnSO_4 \cdot 7H_2O$  and TEPE at room temperature afforded microcrystalline powder of SOFOUR-TEPE-Zn (Figure 2a). Despite extensive attempts, it was not successful in obtaining high-quality single crystals for single-crystal X-ray diffraction studies. The structure of SOFOUR-TEPE-Zn was determined by Rietveld refinement of powder X-ray diffraction (PXRD) pattern (Figure S4 and Tables S1–S3, Supporting Information), which crystallized in the  $Cmm2$  space group, same as the prototype SOFOUR-1-Zn.<sup>[31]</sup> Structure analysis revealed that each Zn(II) atom was coordinated by four terminal nitrogen atoms of independent TEPE/TEPB ligands, generating 2D  $[Zn (TEPB/TEPE)]_n$  layers (Figure 2b,c), which were further pillared by  $SO_4^{2-}$  anions to form 3D networks without interpenetration (Figure 2f,h). Owing to the smaller size of TEPE, the Zn–Zn distance reduced from 12.54 to 9.71 Å along the Y-axis. Consequently, the two distinct pores contracted from  $3.31 \times 6.31$  and  $4.15 \times 4.21 \text{ \AA}^2$  on SOFOUR-1-Zn to  $3.63 \times 3.81$  and  $3.31 \times 3.32 \text{ \AA}^2$  on SOFOUR-TEPE-Zn, respectively. The phase purity of bulk SOFOUR-TEPE-Zn was confirmed by comparing the

as-synthesized sample with the simulated pattern, meanwhile, the unchanged PXRD pattern of the activated sample indicated the structural rigidity (Figure S5, Supporting Information). The simulated and experimental XRD patterns of SOFOUR-1-Zn were presented in Figure S6, Supporting Information. We further mapped the electrostatic surface potential distributions of the cavities by DFT calculations. After ligand substitution, the C=C moieties in SOFOUR-TEPE-Zn draw more electrons than the benzene ring in SOFOUR-1-Zn along the X-axis due to its higher electronegativity (Figure 2d,e). Meanwhile, along the Z-axis, the negatively-charged C atoms of ethylene linkages were unmasked (Figure 2i), in contrast to the exposed positively-charged H atoms of benzene rings (Figure 2g). Therefore, the interlayer spaces sandwiched by organic ligands also showed electronegative pore surfaces. Combined with the smaller pore sizes, a much denser electronegative pore environment was successfully constructed in SOFOUR-TEPE-Zn.

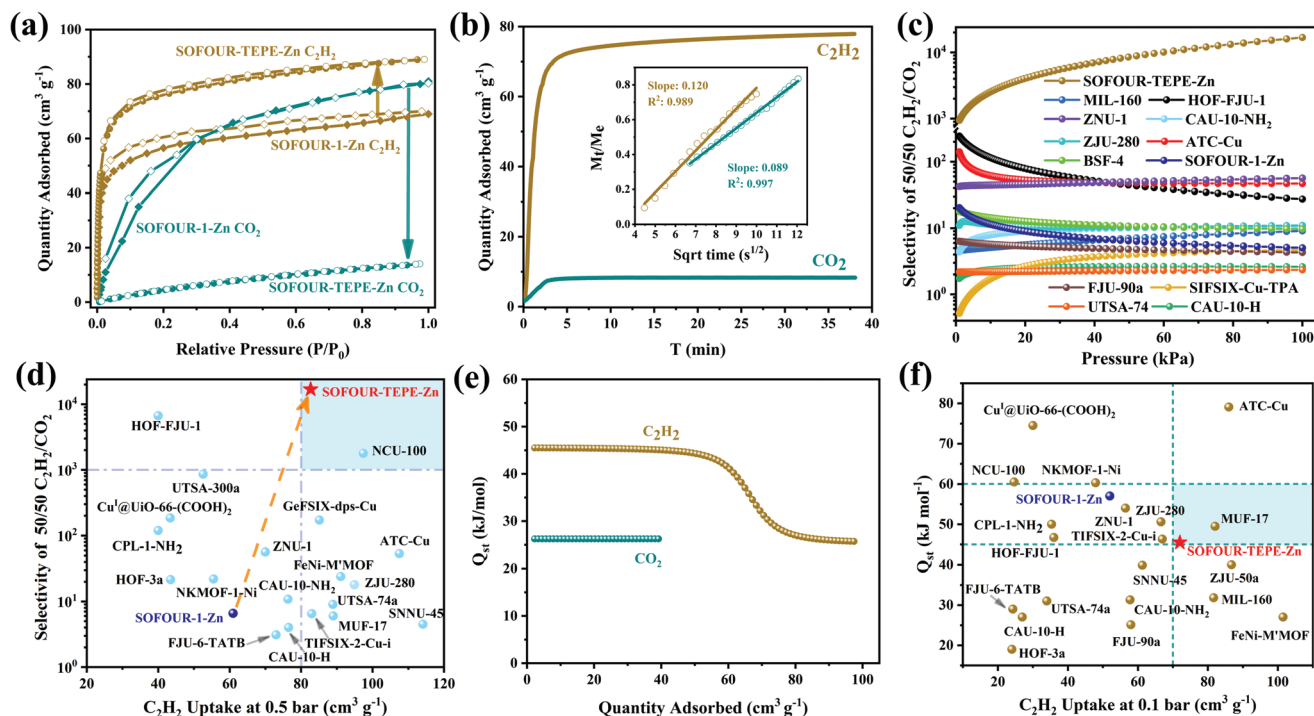
To further confirm the purity of as-synthesized SOFOUR-TEPE-Zn,  $^1H$  nuclear magnetic resonance spectroscopy (NMR) and  $^{13}C$  NMR spectra of digested SOFOUR-TEPE-Zn exhibited identical characteristic peaks of carbon and hydrogen with TEPE ligand (Figures S7 and S8, Supporting Information). The ultimate elemental analysis showed that

the content of each element matched well the theoretical formula of SOFOUR-TEPE-Zn ( $C_{22}H_{16}N_4O_4SZn$ , Table S4, Supporting Information). The characteristic content ratio of N/S in as-synthesized SOFOUR-TEPE-Zn (1.69) was also close to the theoretical value (1.75). The scanning electron microscopy (SEM) image showed the uniform thin-plate morphology of SOFOUR-TEPE-Zn with a thickness of 50–60 nm. (Figure S9, Supporting Information), consistent with the results of transmission electron microscopy (Figure S10, Supporting Information). The energy dispersive X-ray spectroscopy (EDX) demonstrated the even distributions of C, N, O, S, and Zn elements (Figure S11, Supporting Information), which was further confirmed by the X-ray photoelectron spectroscopy (Figure S12, Supporting Information). Fourier transform infrared spectroscopy (FT-IR) spectra showed the characteristic peaks of stretching vibrations of S=O in  $SO_4^{2-}$  pillars at 1116.6 and 1071.0  $cm^{-1}$  and Zn-O stretching vibrations at 589.3 and 469.3  $cm^{-1}$  (Figure S13, Supporting Information). The permanent porosity was probed by  $CO_2$  adsorption at 195 K (Figure S14, Supporting Information), SOFOUR-TEPE-Zn showed a smaller Brunauer–Emmett–Teller (BET) specific surface area of 410.96  $m^2 g^{-1}$  than SOFOUR-1-Zn (612.1  $m^2 g^{-1}$ ) with a total pore volume of 0.14  $cm^3 g^{-1}$ . The negligible  $N_2$  adsorption at 77 K and Ar adsorption at 87 K confirmed its ultramicroporous nature (Figure S15, Supporting Information). The structural stability was examined by immersing SOFOUR-TEPE-Zn in various organic solvents for 10 days and boiling water for 72 h, intact PXRD patterns were maintained (Figure S16, Supporting Information). Thermogravimetric

analysis disclosed that the thermal stability of SOFOUR-TEPE-Zn reached ca. 330 °C (Figure S17, Supporting Information).

## 2.2. Adsorption and Separation Performances

Considering the unique pore chemistry and suitable aperture sizes, single-component  $C_2H_2$  and  $CO_2$  equilibrium sorption isotherms were collected, and notable differences in adsorption capacities were observed (Figure 3a). SOFOUR-TEPE-Zn exhibited steep  $C_2H_2$  adsorption in low-pressure regions and reached a total  $C_2H_2$  uptake of 89.1  $cm^3 g^{-1}$  at 298 K and 1.0 bar, higher than that of SOFOUR-1-Zn (69.4  $cm^3 g^{-1}$ ). Intriguingly, the  $CO_2$  adsorption capacity significantly decreased to 14.1  $cm^3 g^{-1}$  on SOFOUR-TEPE-Zn, which was only 17.4% of that on SOFOUR-1-Zn (81.0  $cm^3 g^{-1}$ ). The adsorption results implied potent  $C_2H_2/CO_2$  separation performances, therein the  $C_2H_2$  uptake at practical partial pressure (0.5 bar) should also be concerned. In this regard, the  $C_2H_2$  adsorption capacity was measured to be 82.7  $cm^3 g^{-1}$  at 0.5 bar and 298 K on SOFOUR-TEPE-Zn (Figure 3d), outperforming that of many top-ranking adsorbents, including NKMOF-1-Ni (55.5  $cm^3 g^{-1}$ ),<sup>[14]</sup> ZNU-1 (70.0  $cm^3 g^{-1}$ ),<sup>[24]</sup> CAU-10-NH<sub>2</sub> (76.3  $cm^3 g^{-1}$ ),<sup>[33]</sup> FJU-6-TATB (73.0  $cm^3 g^{-1}$ ),<sup>[34]</sup> and Cu@UiO-66-(COOH)<sub>2</sub> (43.4  $cm^3 g^{-1}$ ).<sup>[16]</sup> Furthermore, adsorption kinetics should be particularly emphasized in adsorptive processes, the time-dependent gas uptake profiles of  $C_2H_2$  and  $CO_2$  were recorded (Figure 3b). The adsorption kinetic curves disclosed that  $C_2H_2$  and  $CO_2$  reached the equilibrium at almost the same time ( $\approx 4.1$  min), but the



**Figure 3.** a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for SOFOUR-1-Zn and SOFOUR-TEPE-Zn at 298 K. b) Kinetic adsorption profiles of SOFOUR-TEPE-Zn for  $C_2H_2$  and  $CO_2$  at an equilibrium pressure of 500 mbar (Pressure rise rate: 200 mbar  $min^{-1}$ , 298 K). c) IAST adsorption selectivity curves and comparison of SOFOUR-TEPE-Zn for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. d) Comparison of  $C_2H_2$  uptake at 0.5 bar versus  $C_2H_2/CO_2$  selectivity and e)  $Q_{st}$  of  $C_2H_2$  and  $CO_2$  for SOFOUR-TEPE-Zn. f) Comparison plot for  $Q_{st}$  of  $C_2H_2$  and  $C_2H_2$  uptake at 0.1 bar and 298 K.

difference in adsorption capacities was also apparent ( $779 \text{ cm}^3 \text{ g}^{-1}$  for  $\text{C}_2\text{H}_2$  vs  $8.3 \text{ cm}^3 \text{ g}^{-1}$  for  $\text{CO}_2$ ). The diffusional time constant ( $D'$ ,  $D/r^2$ ) of  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  was calculated to be  $1.3 \times 10^{-3} \text{ s}^{-1}$  and  $6.9 \times 10^{-4} \text{ s}^{-1}$ , respectively. The low  $\text{C}_2\text{H}_2/\text{CO}_2$  kinetic separation selectivity of 1.9 indicated its negligible kinetic separation performances.

To assess the separation potential of SOFOUR-TEPE-Zn for  $\text{C}_2\text{H}_2/\text{CO}_2$  gas-mixtures, ideal adsorbed solution theory (IAST) was applied to quantitatively evaluate the separation selectivity. The dual-site Langmuir (DSL) model fitted the adsorption isotherms with excellent accuracy (Table S5, Supporting Information). SOFOUR-TEPE-Zn showed a record-high IAST  $\text{C}_2\text{H}_2/\text{CO}_2$  (50:50, v/v) selectivity of 16833 at 298 K (Figure 3c), 2250-times higher than SOFOUR-1-Zn (6.6)<sup>[31]</sup> and surpassing other best-performing adsorbents such as ZNU-1(56.6),<sup>[24]</sup> CPL-1-NH<sub>2</sub> (119),<sup>[35]</sup> ATC-Cu (53.6),<sup>[13]</sup> Cu@Uio-66-(COOH)<sub>2</sub> (73.9),<sup>[16]</sup> FJU-HOF-1 (6675.0 at 323 K),<sup>[21]</sup> UTSA-300a (860.0),<sup>[17]</sup> and NCU-100a (1786.6).<sup>[36]</sup> The record separation selectivity accompanied with high  $\text{C}_2\text{H}_2$  uptake at 0.5 bar suggested SOFOUR-TEPE-Zn as a new benchmark adsorbent for  $\text{C}_2\text{H}_2/\text{CO}_2$  separation (Figure 3d). Moreover, the maximum amount of  $\text{C}_2\text{H}_2$  that can be recovered from  $\text{C}_2\text{H}_2/\text{CO}_2$  gas-mixture represented by the separation potentials ( $\Delta q_{\text{IAST}}$ ) was calculated.<sup>[37,38]</sup> SOFOUR-TEPE-Zn exhibited a superior  $\Delta q_{\text{IAST}}$  of  $82.7 \text{ cm}^3 \text{ g}^{-1}$  (Figure S19, Supporting Information), almost double the value on SOFOUR-1-Zn ( $44.6 \text{ cm}^3 \text{ g}^{-1}$ ) and higher than most  $\text{C}_2\text{H}_2/\text{CO}_2$  adsorbents such as ZJU-280 ( $79.4 \text{ cm}^3 \text{ g}^{-1}$ ), CAU-10-NH<sub>2</sub> ( $75.9 \text{ cm}^3 \text{ g}^{-1}$ ), ZNU-1 ( $67.9 \text{ cm}^3 \text{ g}^{-1}$ ), HOF-FJU-1 ( $39.9 \text{ cm}^3 \text{ g}^{-1}$ ), and BSF-4 ( $37.9 \text{ cm}^3 \text{ g}^{-1}$ , Figures S21–S31, Supporting Information).

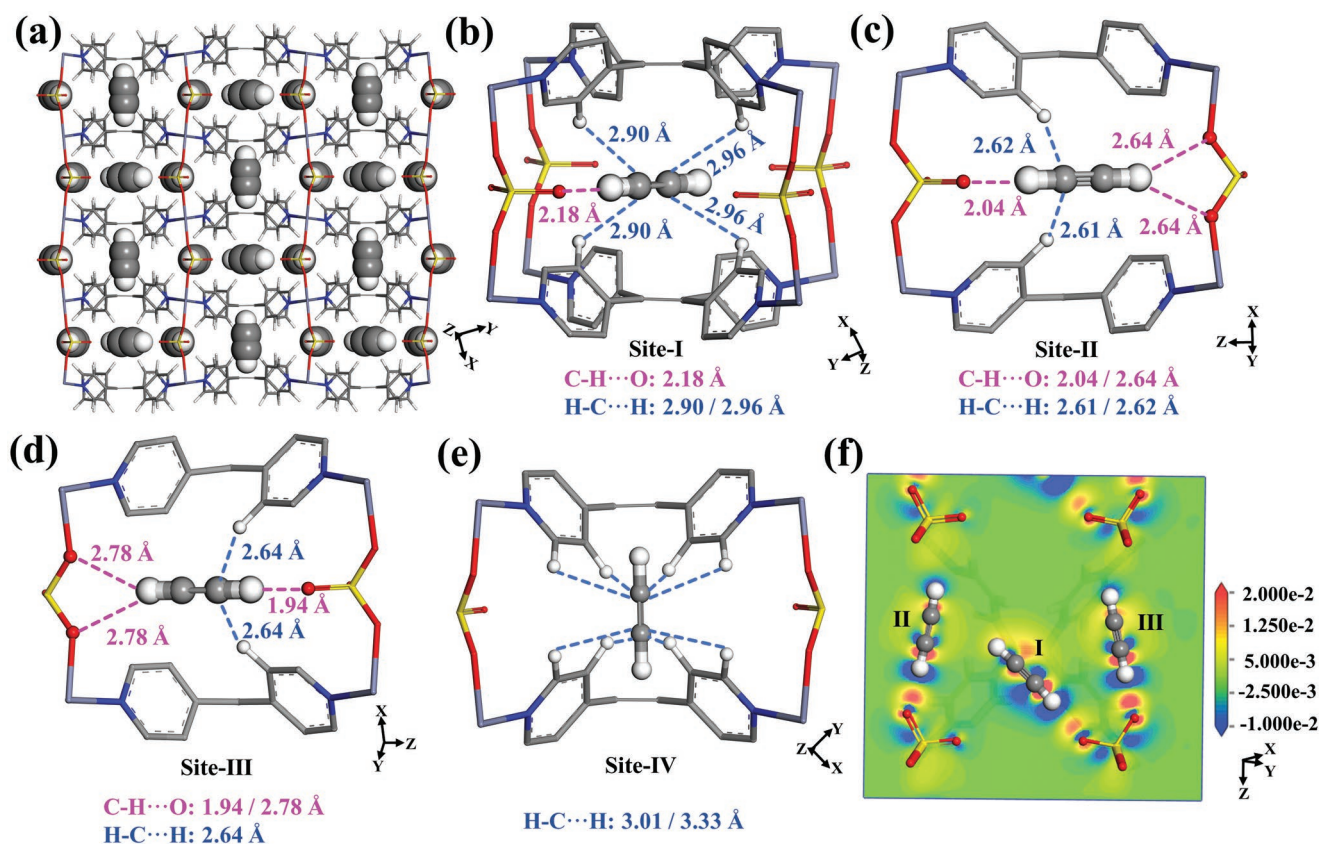
The isosteric heat of adsorption ( $Q_{\text{st}}$ ) was calculated to evaluate the binding affinity between adsorbent and adsorbates. The  $Q_{\text{st}}$  of  $\text{C}_2\text{H}_2$  at near-zero loading of  $45.6 \text{ kJ mol}^{-1}$  belonged to the “sweet spot” region ( $45\text{--}60 \text{ kJ mol}^{-1}$ ) that allows both firm binding and energy-efficient regeneration (Figure 3e).<sup>[31,39]</sup> The ten consecutive cycles of  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  adsorptions verified the facile and complete reversible adsorption behaviors on SOFOUR-TEPE-Zn (Figure S20, Supporting Information). In contrast, the  $Q_{\text{st}}$  of  $\text{CO}_2$  was calculated to be  $26.3 \text{ kJ mol}^{-1}$ , such distinct  $Q_{\text{st}}$  values supported the preferential  $\text{C}_2\text{H}_2$  adsorption and high  $\text{C}_2\text{H}_2/\text{CO}_2$  selectivity. The steep  $\text{C}_2\text{H}_2$  uptake at low-pressure ranges on SOFOUR-TEPE-Zn also evidenced the strong  $\text{C}_2\text{H}_2$  affinity.<sup>[13]</sup> On the other hand, the  $\text{C}_2\text{H}_2$  yields of different industrial production routes are variable, for instance, high-temperature plasma pyrolysis of  $\text{CH}_4$  yields 80–90%  $\text{C}_2\text{H}_2$  and 10–20%  $\text{CO}_2$ .<sup>[40,41]</sup> As expected, SOFOUR-TEPE-Zn exhibited a high  $\text{C}_2\text{H}_2$  uptake of  $72.01 \text{ cm}^3 \text{ g}^{-1}$  at 0.1 bar and 298 K, surpassing most  $\text{C}_2\text{H}_2$  adsorbents such as SOFOUR-1-Zn ( $52.0 \text{ cm}^3 \text{ g}^{-1}$ ), NKMOF-1-Ni ( $48.0 \text{ cm}^3 \text{ g}^{-1}$ ),<sup>[14]</sup> CPL-1-NH<sub>2</sub> ( $35.4 \text{ cm}^3 \text{ g}^{-1}$ ),<sup>[35]</sup> ZNU-1 ( $56.4 \text{ cm}^3 \text{ g}^{-1}$ ),<sup>[24]</sup> FJU-90a ( $58.0 \text{ cm}^3 \text{ g}^{-1}$ ),<sup>[42]</sup> and SNNU-45 ( $61.3 \text{ cm}^3 \text{ g}^{-1}$ ).<sup>[43]</sup> Note that SOFOUR-TEPE-Zn was one of two exceptional adsorbents showing suitable  $Q_{\text{st}}$  of  $\text{C}_2\text{H}_2$  and high  $\text{C}_2\text{H}_2$  uptake ( $>70 \text{ cm}^3 \text{ g}^{-1}$ , Figure 3f).

### 2.3. Modeling Simulation Studies

To gain precise insights into the binding sites of  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  in SOFOUR-TEPE-Zn, modeling studies using first-principles dispersion-corrected density functional theory (DFT-D) and

grand canonical Monte Carlo (GCMC) simulations were carried out. The dense  $\text{C}_2\text{H}_2$  packing pattern showed four distinct adsorption sites in SOFOUR-TEPE-Zn (Figure 4a and Figure S32, Supporting Information). In Site-I,  $\text{C}_2\text{H}_2$  was firmly captured by the O atom of  $\text{SO}_4^{2-}$  pillar through C–H $\cdots$ O bond with a distance of 2.18 Å. Besides, four H–C $\cdots$ H bonds were formed between  $\text{C}_2\text{H}_2$  and neighboring pyridine rings showing distances of 2.90–2.96 Å (Figure 4b). In Site-II and Site-III, similar binding patterns existed as three C–H $\cdots$ O bonds with distances of 2.04–2.78 Å and two H–C $\cdots$ H bonds with distances of 2.61–2.64 Å (Figure 4c,d). Whereas the  $\text{C}_2\text{H}_2$  was cooperatively interacted by four H–C $\cdots$ H bonds in Site-IV with distances of 3.01–3.33 Å (Figure 4e). Meanwhile, due to the dense distributions of  $\text{C}_2\text{H}_2$ , guest-guest interactions were also observed in pore channels (Figure S33a, Supporting Information). For the  $\text{C}_2\text{H}_2$  packing pattern in SOFOUR-1-Zn, the distances of C–H $\cdots$ O (2.02–2.63 Å) and H–C $\cdots$ H (2.55–3.70 Å) bonds between  $\text{C}_2\text{H}_2$  and SOFOUR-1-Zn were relatively longer than that in SOFOUR-TEPE-Zn (Figures S34 and S35, Supporting Information), indicating the weaker  $\text{C}_2\text{H}_2$  capture capability. In sharp contrast, the  $\text{CO}_2$  molecule could only form weak O–C $\cdots$ H van der Waals (vdW) interactions (2.71–2.93 Å) with the H atoms of the pyridine rings of SOFOUR-TEPE-Zn (Figure S36, Supporting Information). Note that no evidence for interactions between  $\text{CO}_2$  and  $\text{SO}_4^{2-}$  pillar in SOFOUR-TEPE-Zn, and no efficient  $\text{CO}_2$  packing was observed due to the electro-repulsive effect (Figure S36, Supporting Information). Whereas, strong interactions were observed between  $\text{CO}_2$  and  $\text{SO}_4^{2-}$  pillar via O–C $\cdots$ O–S bonds (2.80 and 2.86 Å) and SOFOUR-1-Zn framework via O–C $\cdots$ H bonds (2.45–3.64 Å, Figures S37 and S38, Supporting Information). The low-loading adsorption enthalpy of  $\text{C}_2\text{H}_2$  with SOFOUR-TEPE-Zn was calculated to be  $-54.7$ ,  $-71.2$ ,  $-63.0$ , and  $-45.7 \text{ kJ mol}^{-1}$  in Site-I, Site-II, Site-III, and Site-IV respectively. Furthermore, the distribution density of  $\text{C}_2\text{H}_2$  was illustrated by GCMC simulations. At 1 kPa, the adsorbed  $\text{C}_2\text{H}_2$  molecules were distributed near DFT-derived adsorption sites (Figure S39, Supporting Information). As the loading-pressure increased to 50 kPa, no new adsorption location emerged, and the  $\text{C}_2\text{H}_2$  distribution density enhanced (Figure S40, Supporting Information). Intriguing, the  $\text{C}_2\text{H}_2$  distribution density merely changed at 100 kPa (Figure S41, Supporting Information), suggesting the rapid  $\text{C}_2\text{H}_2$  adsorption and saturation before 50 kPa.

The charge transfer analysis on the gas-loaded structures was further performed, in which the blue and yellow surfaces indicate charge accumulation and depletion, respectively. At Sites I-III, strong potential-field induced electron bias was generated between H atoms of  $\text{C}_2\text{H}_2$  and O atoms of  $\text{SO}_4^{2-}$  pillars (Figure 4f and Figure S33b, Supporting Information). Notably, the originally positively-charged H atoms of  $\text{C}_2\text{H}_2$  were almost entirely surrounded by negative electrons, and a large proportion of positrons were clustered around the O atoms of  $\text{SO}_4^{2-}$  pillars. The apparent guest-host charge transfers demonstrated that the electron-potential derived mechanisms endowed strong  $\text{C}_2\text{H}_2$  adsorptions in SOFOUR-TEPE-Zn. Comparably, at Site-IV, relatively weak guest-host charge transfers between H atoms of  $\text{C}_2\text{H}_2$  and C=C bonds occurred (Figure S42, Supporting Information). On the contrary, the charge transfer between  $\text{CO}_2$  molecule and SOFOUR-TEPE-Zn framework



**Figure 4.** a) Dense packing of  $C_2H_2$  molecules in SOFOUR-TEPE-Zn viewed along the Z-axis. b–e)  $C_2H_2$  binding sites in SOFOUR-TEPE-Zn by theoretical studies. f) Charge density difference plots of  $C_2H_2$ -loaded structure.

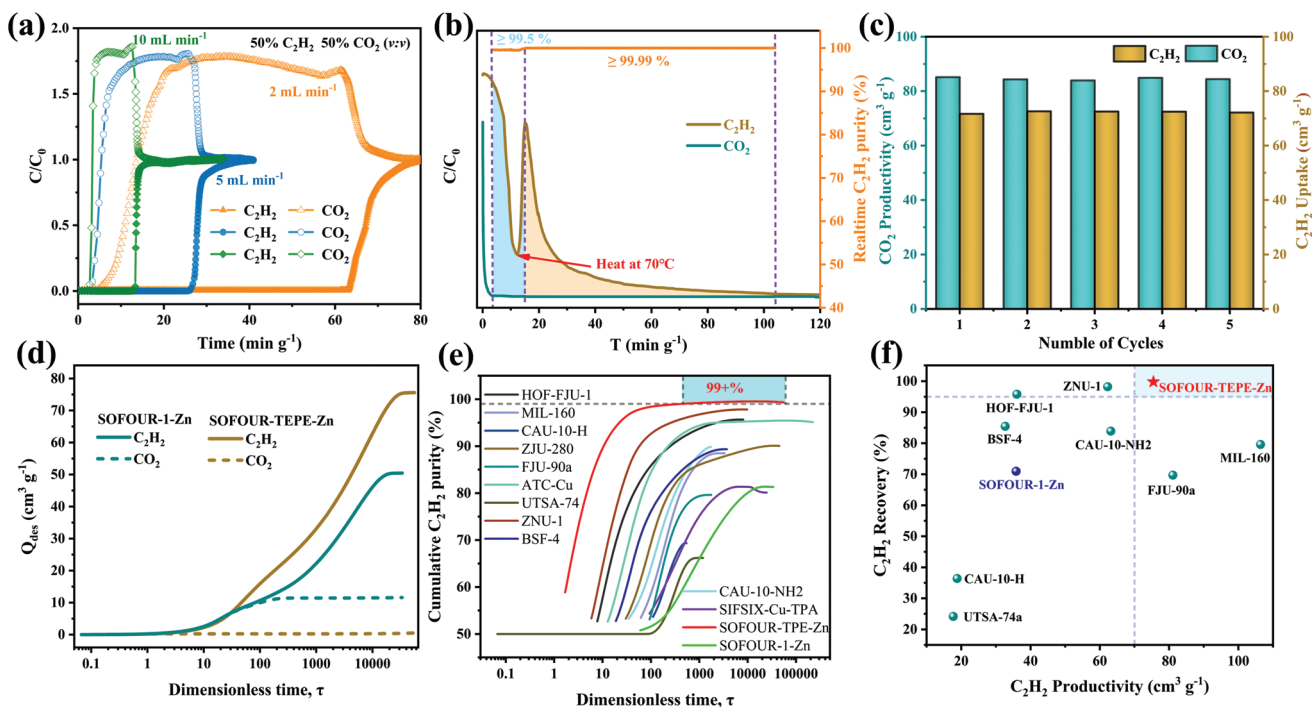
was negligible (Figure S43, Supporting Information). However, both  $C_2H_2$  and  $CO_2$  molecules generated strong potential-field-induced electron bias with SOFOUR-1-Zn (Figures S44 and S45, Supporting Information). Therefore, the dense negative electrostatic potential environments constructed by  $SO_4^{2-}$  pillars and TEPE ligand-induced the preferred  $C_2H_2$  binding over  $CO_2$  on SOFOUR-TEPE-Zn.

#### 2.4. Transient Breakthrough Experiments and PSA Simulations

To demonstrate the feasibility in industrial processes of using SOFOUR-TEPE-Zn under dynamic conditions, transient breakthrough experiments at three different flow rates were carried out for binary  $C_2H_2/CO_2$  (50/50, v/v) mixtures at room temperature (Figure 5a). Clean  $C_2H_2/CO_2$  separations were obtained at three flow rates, and the simulated breakthrough curves matched well with the experimental ones (Figures S48–S50, Supporting Information). With the binary gas-mixture injected into the adsorption bed at the flow rate of  $2.0 \text{ mL min}^{-1}$ , the  $CO_2$  passed through the bed quickly at  $\approx 4.2 \text{ min g}^{-1}$ , whereas the  $C_2H_2$  was retained for  $63.3 \text{ min g}^{-1}$ . When the flow rates increased to 5.0 and  $10.0 \text{ mL min}^{-1}$ , the breakthrough point for  $C_2H_2$  decreased to 25.4 and  $12.3 \text{ min g}^{-1}$ , and the clean separations were still retained. The corresponding dynamic  $C_2H_2$  adsorption amount was calculated to be 72.0, 70.8, and  $68.1 \text{ cm}^3 \text{ g}^{-1}$  at 2.0, 5.0, and  $10.0 \text{ mL min}^{-1}$ , respectively. More

importantly, high-purity  $C_2H_2$  product was generated during desorption processes, thus the desorption conditions and methods should be investigated but commonly less explored. In this work, we applied a two-step desorption process to collect as many high-purity  $C_2H_2$  products as possible. The saturated adsorption column was purged by helium (He) stream at  $10.0 \text{ mL min}^{-1}$  and 298 K to blow out weakly adsorbed  $C_2H_2$ , then heated to 343 K to extract firmly adsorbed  $C_2H_2$ . As illustrated by the desorption curves (Figure 5b), almost all adsorbed  $CO_2$  could be wiped out quickly at  $3.33 \text{ min g}^{-1}$ , followed by the  $C_2H_2$  stream with purity above 99.5%. When the desorption rate decreased at  $11.95 \text{ min g}^{-1}$ , the heating at 343 K rapidly facilitated the desorption rate of  $C_2H_2$ , while no additional  $CO_2$  was released. Benefiting from this strategy, the purity of recovered  $C_2H_2$  raised to above 99.99% after  $14.24 \text{ min g}^{-1}$ . Noticeably, the collected amounts of  $C_2H_2$  reached  $60.1 \text{ cm}^3 \text{ g}^{-1}$  with purity > 99.5% and  $33.2 \text{ cm}^3 \text{ g}^{-1}$  with purity > 99.99%. Moreover, the cycling and reusability of adsorbents are critical parameters for practical applications. Successive cycling breakthrough cycles at three flow rates were conducted, and no noticeable deterioration in breakthrough times was observed (Figures S51–S53, Supporting Information). Besides, about  $84.5 \text{ cm}^3 \text{ g}^{-1}$  of  $CO_2$  with a purity of 99.99% could be stably obtained in each breakthrough cycle while maintaining high  $C_2H_2$  dynamic uptakes (Figure 5c).

The simulations of PSA processes were further conducted to compare separation performances of SOFOUR-TEPE-Zn,



**Figure 5.** a) The breakthrough curves of SOFOUR-TEPE-Zn for C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> (50/50, v/v) at different flow rates at 298 K. b) The signals of desorbed gases from the breakthrough column. c) The CO<sub>2</sub> productivity and C<sub>2</sub>H<sub>2</sub> uptake during cycle breakthrough tests at 2.0 mL min<sup>-1</sup>. d) Cumulative moles of C<sub>2</sub>H<sub>2</sub> and CO<sub>2</sub> recovered, and e) Cumulative C<sub>2</sub>H<sub>2</sub> purity recovered from SOFOUR-TEPE-Zn and benchmark adsorbents during simulated counter-current blowdown operations. f) Comparison plot of recovered C<sub>2</sub>H<sub>2</sub> productivity and recovery for obtaining 99.5% C<sub>2</sub>H<sub>2</sub>.

SOFOUR-1-Zn, and other benchmark MOFs (Figure 5d-e and Figures S21–S31, Supporting Information). The counter-current vacuum blowdown operations were applied to collect C<sub>2</sub>H<sub>2</sub> products in a simplified two-bed PSA scheme (Figure S1, Supporting Information).<sup>[37,38]</sup> In practice, the counter-current blowdown operation will be initiated just before C<sub>2</sub>H<sub>2</sub> breaks through in the adsorption column, as indicated by the arrows in Figure S47, Supporting Information. The cumulative moles of recovered C<sub>2</sub>H<sub>2</sub> and CO<sub>2</sub> as a function of dimensionless time were plotted in Figure 5d. The recovered amount of C<sub>2</sub>H<sub>2</sub> reached 75.7 cm<sup>3</sup> g<sup>-1</sup> on SOFOUR-TEPE-Zn during the counter-current blowdown process with 100% C<sub>2</sub>H<sub>2</sub> recovery, higher than that of SOFOUR-1-Zn (50.4 cm<sup>3</sup> g<sup>-1</sup>), ZNU-1 (63.4 cm<sup>3</sup> g<sup>-1</sup>), CAU-10-NH<sub>2</sub> (75.3 cm<sup>3</sup> g<sup>-1</sup>), UTSA-74 (73.5 cm<sup>3</sup> g<sup>-1</sup>), and HOF-FJU-1 (37.6 cm<sup>3</sup> g<sup>-1</sup>, Figure S54 and Table S7, Supporting Information). Noticeably, the amount of recovered CO<sub>2</sub> constantly remained at 0.5 cm<sup>3</sup> g<sup>-1</sup> on SOFOUR-TEPE-Zn, significantly lower than 11.6 cm<sup>3</sup> g<sup>-1</sup> on SOFOUR-1-Zn, indicating a much higher C<sub>2</sub>H<sub>2</sub> purity during counter-current blowdown process.<sup>[38,44]</sup>

As shown in Figure 5e, a record-high C<sub>2</sub>H<sub>2</sub> purity of 99+% could be achieved at  $\tau = 412.1$  on SOFOUR-TEPE-Zn, and the final C<sub>2</sub>H<sub>2</sub> purity could reach 99.34% with 100% C<sub>2</sub>H<sub>2</sub> recovery, outperforming that of SOFOUR-1-Zn (81.31%), MIL-160 (88.47%), CAU-10-NH<sub>2</sub> (89.82%), ZJU-280 (90.06%), FJU-90a (79.62%), UTSA-74 (66.19%), and ZNU-1 (97.80%, Figure S54 and Table S7, Supporting Information). To produce polymer-degree C<sub>2</sub>H<sub>2</sub> (purity > 99.5%), certain amounts of gas products will be released before collection in the counter-current blowdown process, which will inevitably

lead to the reduction of gas recovery. Therefore, we further compared the gas recovery on the basis of obtaining 99.5% purity C<sub>2</sub>H<sub>2</sub> (Table S8, Supporting Information). As shown in Figure 5f, SOFOUR-TEPE-Zn still maintained a high gas recovery of 99.82% with a C<sub>2</sub>H<sub>2</sub> productivity of 75.5 cm<sup>3</sup> g<sup>-1</sup>, outperforming SOFOUR-1-Zn (70.97% and 35.8 cm<sup>3</sup> g<sup>-1</sup>), HOF-FJU-1 (95.81% and 36.1 cm<sup>3</sup> g<sup>-1</sup>), ZNU-1 (98.22% and 62.3 cm<sup>3</sup> g<sup>-1</sup>), BSF-4 (85.45% and 32.7 cm<sup>3</sup> g<sup>-1</sup>), UTSA-74 (24.18% and 177 cm<sup>3</sup> g<sup>-1</sup>), FJU-90a (69.73% and 81.1 cm<sup>3</sup> g<sup>-1</sup>), and MIL-160 (79.61% and 106.4 cm<sup>3</sup> g<sup>-1</sup>).

### 3. Conclusion

In summary, a dense electronegative pore environment was constructed in SOFOUR-TEPE-Zn, achieving highly selective recognition for C<sub>2</sub>H<sub>2</sub> and benchmark C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> separation performances. Noticeably, SOFOUR-TEPE-Zn exhibited a record-high C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> selectivity (16833) with leading C<sub>2</sub>H<sub>2</sub> adsorption capacity (89.1 cm<sup>3</sup> g<sup>-1</sup>) at 298 K and 1.0 bar. Dynamic breakthrough experiments confirmed clean separations of equimolar C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> gas-mixtures. Meanwhile, 60.1 cm<sup>3</sup> g<sup>-1</sup> C<sub>2</sub>H<sub>2</sub> of 99.5% purity or 33.2 cm<sup>3</sup> g<sup>-1</sup> C<sub>2</sub>H<sub>2</sub> of 99.99% purity can be recovered during desorption using stepped purging and mild heating. The simulated PSA processes demonstrated high C<sub>2</sub>H<sub>2</sub> productivity of 75.5 cm<sup>3</sup> g<sup>-1</sup> C<sub>2</sub>H<sub>2</sub> of 99.5% purity could be produced with 99.82% C<sub>2</sub>H<sub>2</sub> recovery. DFT-D and GCMC simulations identified the favorable C<sub>2</sub>H<sub>2</sub> adsorption sites in the electronegative pore environments created by SO<sub>4</sub><sup>2-</sup> anions and TEPE ligands.

## Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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## Conflict of Interest

The authors declare no conflict of interest.

## Data Availability Statement

The data that support the findings of this study are available in the supplementary material of this article.

## Keywords

adsorptive separation, electrostatic separation, metal-organic frameworks, pore environment modification

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# ADVANCED MATERIALS

## Supporting Information

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Engineering Pore Environments of Sulfate-Pillared  
Metal-Organic Framework for Efficient C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub>  
Separation with Record Selectivity

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*Supplementary Information*

**Engineering Pore Environments of Sulfate-pillared Metal-Organic Framework  
for Efficient C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> Separation with Record Selectivity**

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## Materials

All reagents were purchased from commercial companies and used without further purification. ZnSO<sub>4</sub>·7H<sub>2</sub>O (99.98%, Aladdin), 1,1,2,2-tetra(pyridin-4-yl) ethene (C<sub>22</sub>H<sub>16</sub>N<sub>4</sub>, 99+%, Extension), and methanol (CH<sub>4</sub>O, anhydrous, 99.9%, Aladdin). N<sub>2</sub> (99.999%), acetylene (C<sub>2</sub>H<sub>2</sub>, 99.99%), carbon dioxide (CO<sub>2</sub>, 99.99%), He (99.999%), and mixed gas-mixtures of C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> (50/50, v/v), were purchased from Shanghai Wei Chuang Gas Co., Ltd (China).

## Synthesis of SOFOUR-TEPE-Zn

Typically, ZnSO<sub>4</sub>·7H<sub>2</sub>O (0.3 mmol) was added to a solution of TEPE (0.3 mmol) in 20 mL MeOH and stirred at room temperature overnight. SOFOUR-TEPE-Zn·xMeOH was obtained as a white microcrystalline powder, which was isolated by filtration, washed with MeOH three times, and dried 6 h in a vacuum oven at 333 K. (yield: 1527 mg as synthesized, 1245 mg as activated).

## Details for Rietveld refinement

The initial structure for SOFOUR-TEPE-Zn was referred to the reported work (CCDC identifier: 2105435). We applied the EXPO2014 software to conduct the Rietveld refinement, the 2 $\theta$  range of 5~60° was used for the refinement. Chebyshev (Background Function) and Pseudo-Voigt (Peak Shape Functions) were applied to refine the structure until the R<sub>wp</sub> value converged and the overlay of the observed with refined profiles showed good agreement. Unit cell parameters and fitting reliability are listed in Table S2, and we have deposited the CIF in the CCDC database with an identifier number of 2240118.

## <sup>1</sup>H NMR and <sup>13</sup>C NMR spectroscopy analysis of digested MOF samples NMR measurement:

For <sup>1</sup>H NMR and <sup>13</sup>C NMR spectroscopy, the activated SOFOUR-TEPE-Zn was digested using the following protocol: 500  $\mu$ L of 20% DCl in D<sub>2</sub>O mixed with 1000  $\mu$ L of DMSO-d<sub>6</sub> to give a DCl/DMSO-d<sub>6</sub> stock solution. About 5 mg of SOFOUR-TEPE-Zn or TEPE ligands was digested in 450  $\mu$ L of this stock solution. Spectra were acquired immediately on a Bruker Spectrometer following dissolution.

## Ultimate element analysis

The contents of C, H, N, S, and O elements were determined by an Elementar Vario MICRO elemental analyzer with an O measurement mode. In detail, about 2 mg samples were weighed and

wrapped in a tin foil ark, then placed in the sample tray. Using high-purity helium as the carrier gas, the content of each element was detected by a TCD detector in CHNS and O mode, respectively.

### **Scanning electron microscope (SEM)**

The sample was directly glued to the conductive adhesive, and the gold spraying for 45s (10mA) was conducted on Oxford Quorum SC7620 sputtering coater. The SEM images were recorded on a ZEISS Sigma 300 scanning electron microscope with an accelerated voltage of 3kV.

### **Transmission electron microscope (TEM) and energy dispersive X-ray spectroscopy (EDX) elemental mapping**

Transmission electron microscope images were obtained by a Thermo Fisher Talos F200S G2 microscope with selected area electron diffraction (SAED) patterns. EDX analyses were performed with a Ge detector and careful calibration using standards permitted quantitative analyses of major elements.

### **X-ray Photoelectron Spectroscopy (XPS)**

The XPS spectra of SOFOUR-TEPE-Zn were collected by Thermo Scientific K-Alpha XPS instrument. The sample chamber was vacuumed less than  $2.0 \times 10^{-7}$  mbar before each test. The spot size was 400  $\mu\text{m}$ , the working voltage was 12 kV, and the filament current was 6 mA. The full spectrum scanning energy was 150 eV with a step size of 1 eV. The narrow-spectrum scanning energy was 50 eV with a step size of 0.1 eV.

### **Fourier transform infrared spectroscopy (FT-IR)**

In a dry environment, an appropriate amount of SOFOUR-TEPE-Zn and dried potassium bromide (KBr) powder were added into a mortar, thoroughly ground and transferred to a tablet press. The background was first collected during the test, and then the infrared spectrum of the sample was collected. The resolution was  $4 \text{ cm}^{-1}$ , the number of scans was 32, and the test wave number was  $400\text{-}4000 \text{ cm}^{-1}$ .

### **Gas adsorption measurements**

Equilibrium and kinetic adsorptions of  $\text{C}_2\text{H}_2$ , and  $\text{CO}_2$  at 273, 298 K, and 323 K were measured on Micromeritics 3 Flex adsorption apparatus (Micromeritics Instruments, USA). To remove all the

guest solvents in the framework, the fresh powder samples were evacuated under a high vacuum at 333 K for 6 h. The Brunauer-Emmett-Teller (BET) surface area was calculated using the adsorption branch with the relative pressure  $P/P_0$  in the range of 0.05 to 0.3. The total pore volume ( $V_{tot}$ ) was calculated based on the adsorbed amount of  $CO_2$  at the  $P/P_0$  of 0.99. The helium gas was used to determine the free space of the system. The sample was degassed for 6 h between each measurement.

### Fitting of unary isotherm data

The unary isotherms for  $C_2H_2$  measured at three different temperatures 273 K, 298 K, and 323 K in SOFOUR-TEPE-Zn were fitted with excellent accuracy using either the dual-site Langmuir model, where we distinguish two distinct adsorption sites A and B:

$$q = \frac{q_{sat,A} b_A P}{1 + b_A P} + \frac{q_{sat,B} b_B P}{1 + b_B P} \quad (S1)$$

In eq (S1), the Langmuir parameters  $b_A, b_B$  are both temperature dependent

$$b_A = b_{A0} \exp\left(\frac{E_A}{RT}\right); \quad b_B = b_{B0} \exp\left(\frac{E_B}{RT}\right) \quad (S2)$$

In eq (S2),  $E_A, E_B$  are the energy parameters associated with sites A, and B, respectively.

The unary isotherms for  $CO_2$  measured at three different temperatures 273 K, 298 K, and 323 K in SOFOUR-TEPE-Zn were fitted with excellent accuracy using the single-site Langmuir model.

$$q = \frac{q_{sat,A} b_A P}{1 + b_A P} \quad (S3)$$

The unary isotherm fit parameters for  $C_2H_2$  and  $CO_2$  in SOFOUR-TEPE-Zn are provided in Table S1.

### Isosteric heat of adsorption

The isosteric heat of adsorption,  $Q_{st}$ , is defined as

$$Q_{st} = -RT^2 \left( \frac{\partial \ln P}{\partial T} \right)_q \quad (S4)$$

where the derivative in the right member of eq (S4) is determined at constant adsorbate loading,  $q$ .

### IAST calculations

For screening MOFs for separation of binary mixtures of components 1 and 2, the adsorption selectivity,  $S_{ads}$ , is defined by

$$S_{ads} = \frac{q_1/q_2}{y_{10}/y_{20}} \quad (S5)$$

In eq (S5),  $y_{10}, y_{20}$  are the mole fractions of the bulk gas phase mixture.

The  $C_2H_2(1)/CO_2(2)$  mixture separations are envisaged to be carried out in fixed bed adsorbers. In such devices, the separations are dictated by adsorption selectivity and uptake capacity. Using the shock wave model for fixed-bed adsorbers, Krishna<sup>[1, 2]</sup> has suggested that the appropriate metric is the separation potential,  $\Delta q_1$ . The appropriate expression describing the productivity of pure  $C_2H_2$  in the desorption phase of fixed-bed operations is

$$\Delta q_1 = q_1 - q_2 \frac{y_{10}}{y_{20}} \quad (S6)$$

In eq (S6)  $y_{10}, y_{20}$  are the mole fractions of the feed mixture during the adsorption cycle. In the derivation of eq (S6), it is assumed that the concentration “fronts” traversed the column in the form of shock waves during the desorption cycle. The molar loadings  $q_1, q_2$  of the two components are determined using the Ideal Adsorbed Solution Theory (IAST) of Myers and Prausnitz using the unary isotherm fits as data inputs.<sup>[3]</sup> The physical significance of  $\Delta q_1$  is the maximum productivity of pure  $C_2H_2(1)$  that is achievable in PSA operations.

### Calculation of kinetic adsorption

The kinetic adsorption curves of  $C_2H_2$  and  $CO_2$  for SOFOUR-TEPE-Zn were measured on Intelligent Gravimetric Analyzer (IGA-100, HIDEN).

The diffusional time constants ( $D'$ ,  $D/r^2$ ) were calculated by the short-time solution of the diffusion equation assuming a step change in the gas-phase concentration<sup>[4]</sup>, clean beds initially, and micropore diffusion control:

$$\frac{M_t}{M_e} = \frac{6}{\sqrt{\pi}} \cdot \sqrt{\frac{D}{r^2} \cdot t} \quad (S7)$$

Where  $M_t$  is the gas uptake at time  $t$ (s),  $M_e$  is the gas uptake at equilibrium ( $cm^3 g^{-1}$ ),  $D$  ( $m^2 s^{-1}$ ) is the diffusivity and  $r$  (m) is the radius of the equivalent spherical particle. The slopes of  $M_t/M_e$  versus  $t^{1/2}$  are derived from the fitting of the plots at 500 mbar and 298 K.

## Transient breakthrough experiments and simulations

The breakthrough experiments were performed on a self-assembly device. Typically, the activated SOFOUR-TEPE-Zn (0.5145 g) was packed into a stainless-steel column (4 mm inner diameter  $\times$  30mm). The column was first purged with a He flow (10 mL min<sup>-1</sup>) at room temperature for 6 h before breakthrough measurements. The binary C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> (50/50, v/v) gas-mixture was introduced at fixed flow rates of 2 mL min<sup>-1</sup>, 5 mL min<sup>-1</sup>, and 10 mL min<sup>-1</sup>, respectively. The outlet gas from the column was monitored using mass spectrometry (Hidden, UK), and an attached mass flow controller (Seven Star, MC-2SCCM-D) was used to control the gas flow. After each breakthrough measurement, the columns packed with samples were regenerated by purging dry He gas (10 mL min<sup>-1</sup>) at room temperature.

Transient breakthrough simulations were carried out for the same operating conditions as in the three experimental data sets, using the methodology described in earlier publications.<sup>[1, 2, 5-7]</sup> In these simulations, intra-crystalline diffusion influences are ignored.

## Adsorption/desorption cycles

The desired ethyne product is available in the blowdown phase of the simplified scheme shown in Figure S1. To compare the separation performance of SOFOUR-TEPE-Zn with other materials with excellent properties, we conducted simulations of both adsorption and counter-current vacuum blow-down operations. For these simulations we choose: length of packed bed,  $L = 0.3$  m; cross-sectional area,  $A = 1$  m<sup>2</sup>; superficial gas velocity at the entrance to the bed,  $u_0 = 0.04$  m s<sup>-1</sup>; voidage of the packed bed,  $\varepsilon = 0.4$ . The interstitial gas velocity  $v = \frac{u}{\varepsilon}$ . The total volume of the bed is

$V_{bed} = LA$ . The volume of zeolite or MOF used in the simulations is  $V_{ads} = LA(1 - \varepsilon)$ .

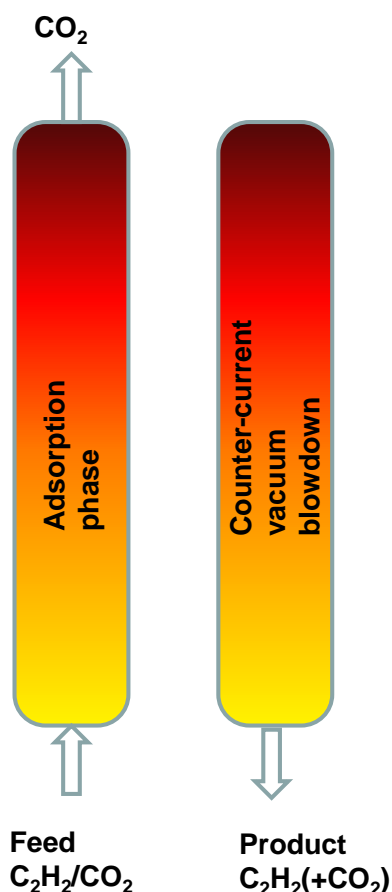
It is important to note that the volume of adsorbent,  $V_{ads}$ , includes the pore volume of the adsorbent material. If  $\rho$  is the framework density, the mass of the adsorbent in the bed is:

$$m_{ads} = (1 - \varepsilon) \times (L \times A) \times (\rho) \text{ kg.} \quad (\text{S8})$$

The dimensionless concentrations in the exit,  $c_i/c_{i0}$  are plotted as a function of the parameter:

$$\frac{(Q_0 = \text{flow rate mL min}^{-1}) \times (\text{time in min})}{(\text{g MOF packed in tube})} = \frac{Q_0 t}{m_{ads}} = \text{mL g}^{-1}. \quad (\text{S9})$$

In our simulations, a deep vacuum (= 2 Pa) was applied. Since the vacuum pump characteristics are unknown, it is arbitrarily assumed that the interstitial velocity in the fixed bed is maintained at  $v = \frac{u}{\varepsilon} = 0.1 \text{ m s}^{-1}$ . Desorption is a much slower process, and the time required for the total recovery of adsorbed components is significant.



**Figure S1.** Sequential steps in the operation of a fixed-bed adsorber in a simplified two-bed scheme for C<sub>2</sub>H<sub>2</sub>(1)/CO<sub>2</sub>(2) separation.<sup>[8]</sup>

### Density functional theory calculations

First-principles density functional theory (DFT) calculations were performed using Materials Studio's CASTEP code. All calculations were conducted under the generalized gradient approximation (GGA) with Perdew-Burke-Ernzerhof (PBE). The optimized structures are in great consistency with the experimentally determined crystal structures. The energy, force, and displacement convergence criteria were set as  $1 \times 10^{-5}$  eV,  $3 \times 10^{-2}$  eV, and  $1 \times 10^{-3}$  Å, respectively. Single point energy calculations with the same parameters using Dmol<sup>3</sup> were performed on optimized SOFOUR-TEPE-Zn. The electron density data obtained from these calculations were used



to construct the  $0.015 \text{ e}^- \text{ \AA}^{-3}$  electron density isosurfaces of the  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  molecules, while the electron density data of both frameworks were used to construct the  $0.15 \text{ e}^- \text{ \AA}^{-3}$  electron density isosurfaces, with a grid interval of  $0.1 \text{ \AA}$ . The calculated electrostatic potential for SOFOUR-TEPE-Zn and  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  molecules were then mapped onto their electron density isosurfaces. A semiempirical addition of dispersive forces to conventional DFT was included in the calculation to account for van der Waals interactions. Cutoff energy of 600 eV and a  $2 \times 2 \times 3$  k-point mesh were enough for the total energy coverage within  $0.01 \text{ meV atom}^{-1}$ . The structures of the synthesized materials were first optimized from the reported crystal structures. To obtain the binding energy, the pristine structure and an isolated gas molecule placed in a supercell (with the same cell dimensions as the pristine crystal structure) were optimized and relaxed as references.  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  gas molecules were then introduced to different locations of the channel pore, followed by a full structural relaxation. The static binding energy was calculated by the equation  $E_B = E(\text{gas}) + E(\text{adsorbent}) - E(\text{adsorbent} + \text{gas})$ .

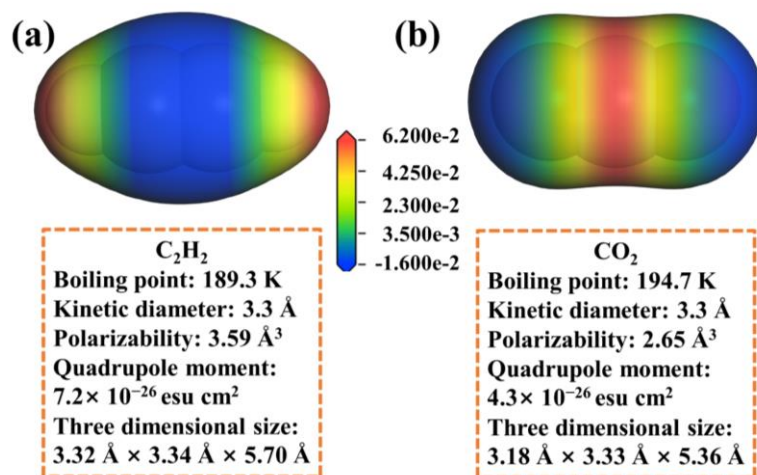
### **Grand Canonical Monte Carlo (GCMC) calculations**

All the GCMC simulations were performed in MS 2020 package. The crystal structure of the SOFOUR-TEPE-Zn was chosen after the DFT geometry optimization. The framework and the individual  $\text{C}_2\text{H}_2$  and  $\text{CO}_2$  were considered rigid during the simulation. The charges for atoms of the SOFOUR-TEPE-Zn and gas components were derived from the Mulliken method. The simulations adopted the fixed pressure task, Metropolis method in the sorption module, the force field parameters of metal atoms are from the UFF force field, while those of non-metallic atoms are from Dreiding force field. The interaction energy between the adsorbed molecules and the framework was computed through the Coulomb and Lennard-Jones 6-12 (LJ) potentials. The cutoff radius was chosen  $15.5 \text{ \AA}$  for LJ potential, and the electrostatic interactions were handled using the Ewald summation method. The loading steps and the equilibration steps were  $5 \times 10^7$ , the production steps were  $5 \times 10^7$ .

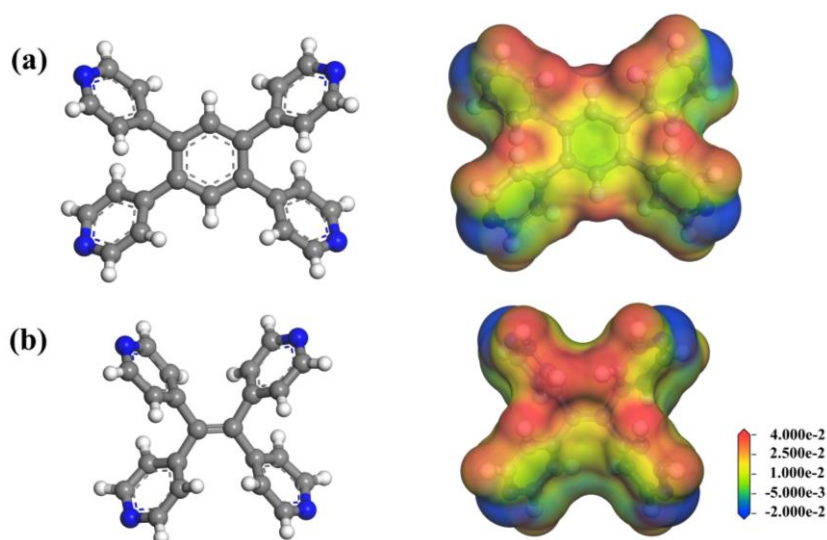
### **Structural stability tests**

Powder X-ray diffraction (PXRD) was collected on a PANalytical Empyrean Series 2 diffractometer with Cu  $K\alpha$  radiation ( $\lambda = 1.540598 \text{ \AA}$ ), which operated at 40 kV, 40 mA and a scan speed of  $0.0167^\circ$ ,

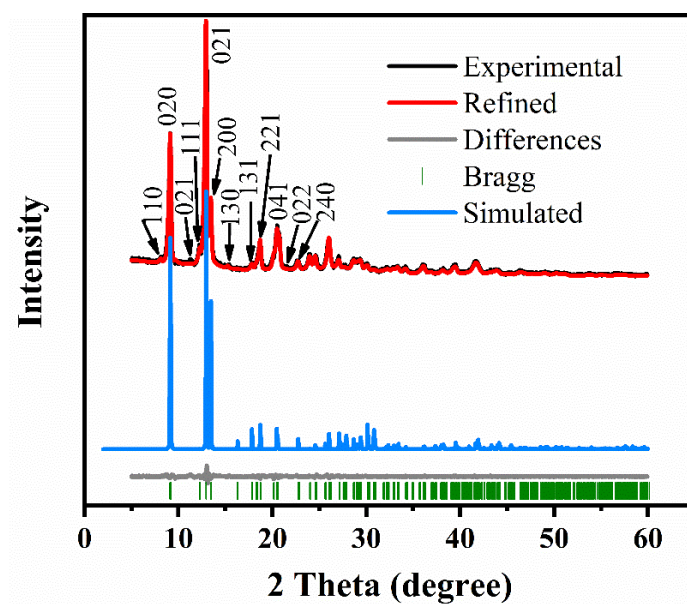
a scan time of 15 s per step, and  $2\theta$  ranging from 5 to  $60^\circ$  at room temperature. The thermogravimetric analysis (TGA) data were performed on a NETZSCH Thermogravimetric Analyzer (STA2500) from 25 to  $800^\circ\text{C}$  with a heating rate of  $10^\circ\text{C}/\text{min}$  under an  $\text{N}_2$  atmosphere. Solvent stability tests were performed by placing 100 mg samples in 20 mL vials containing 15 mL of organic solvent for one week at ambient temperature. Then, the solid was separated by filtration and subsequently activated at 343 K for 6 h, and PXRD tests characterized the structure of materials.



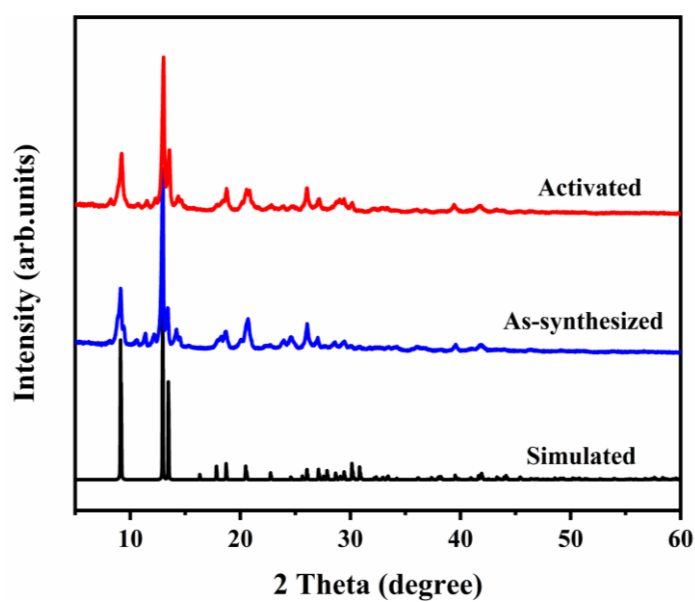
**Figure S2.** Isosurface maps of the molecular electrostatic potential (MESP), molecular sizes, and physical properties for (a)  $\text{C}_2\text{H}_2$  and (b)  $\text{CO}_2$ . Red and blue colors represent the positive and negative part of MESP, respectively.



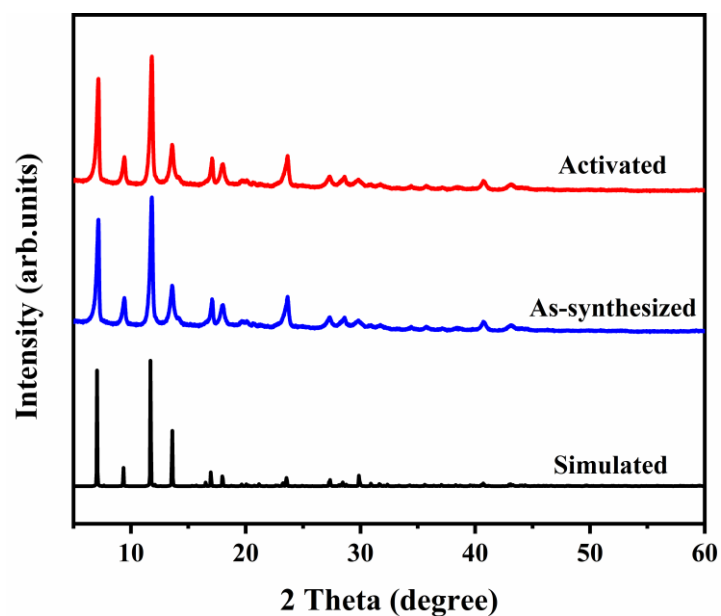
**Figure S3.** The molecule structure and MESP mapping for (a) TEPB and (b) TEPE organic ligand.



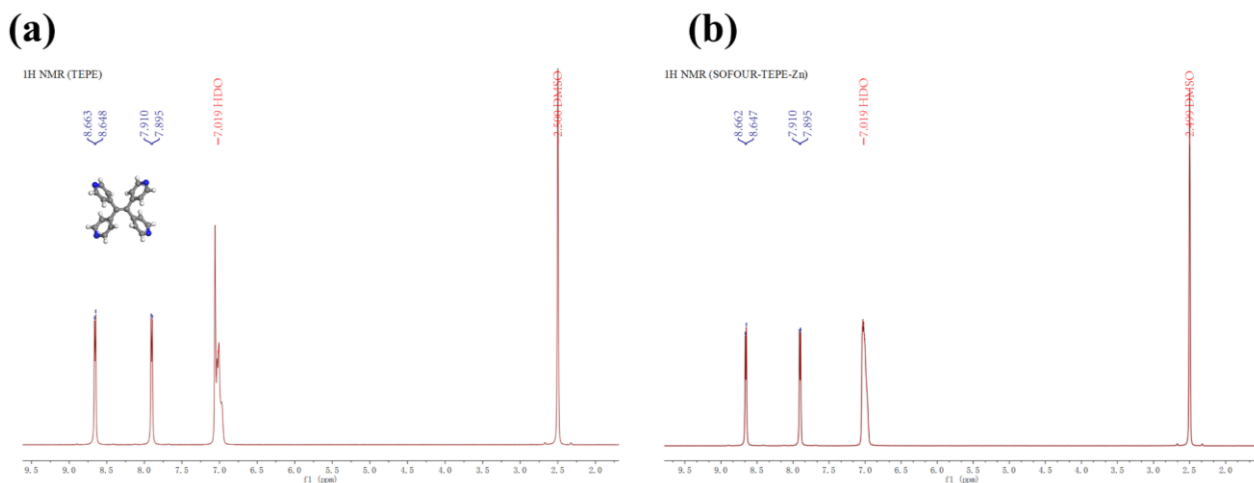
**Figure S4.** Rietveld refinement plot and PXRD patterns of as-synthesized SOFOUR-TEPE-Zn.



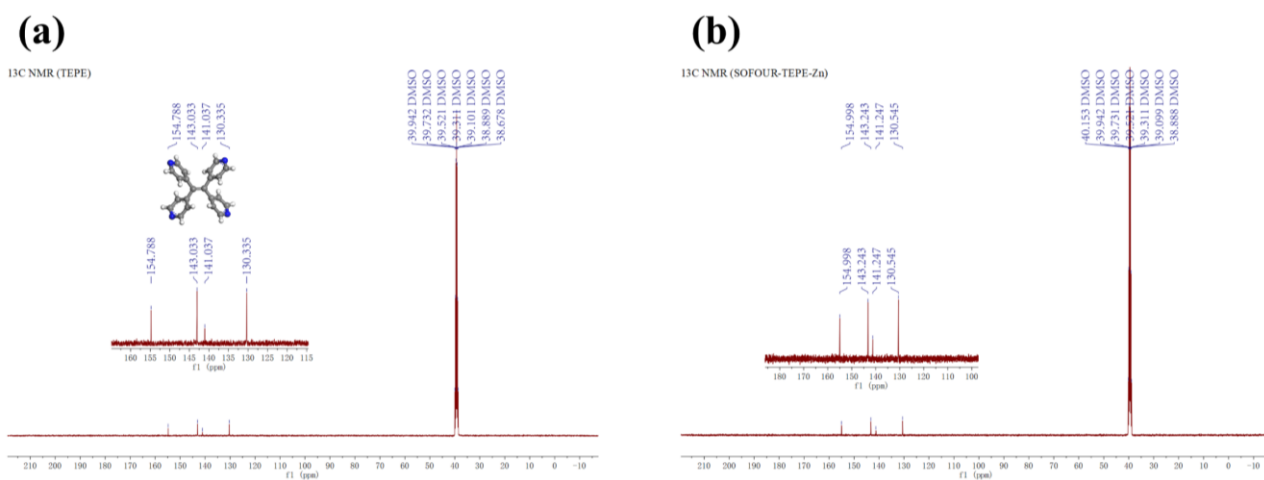
**Figure S5.** PXRD patterns of SOFOUR-TEPE-Zn under different conditions.



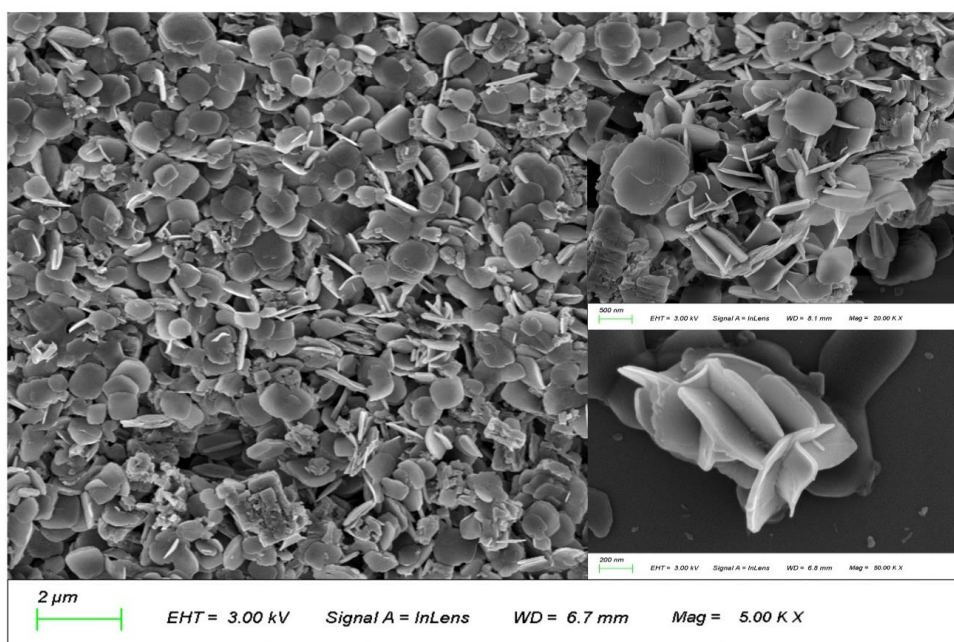
**Figure S6.** PXRD patterns of SOFOUR-1-Zn under different conditions.



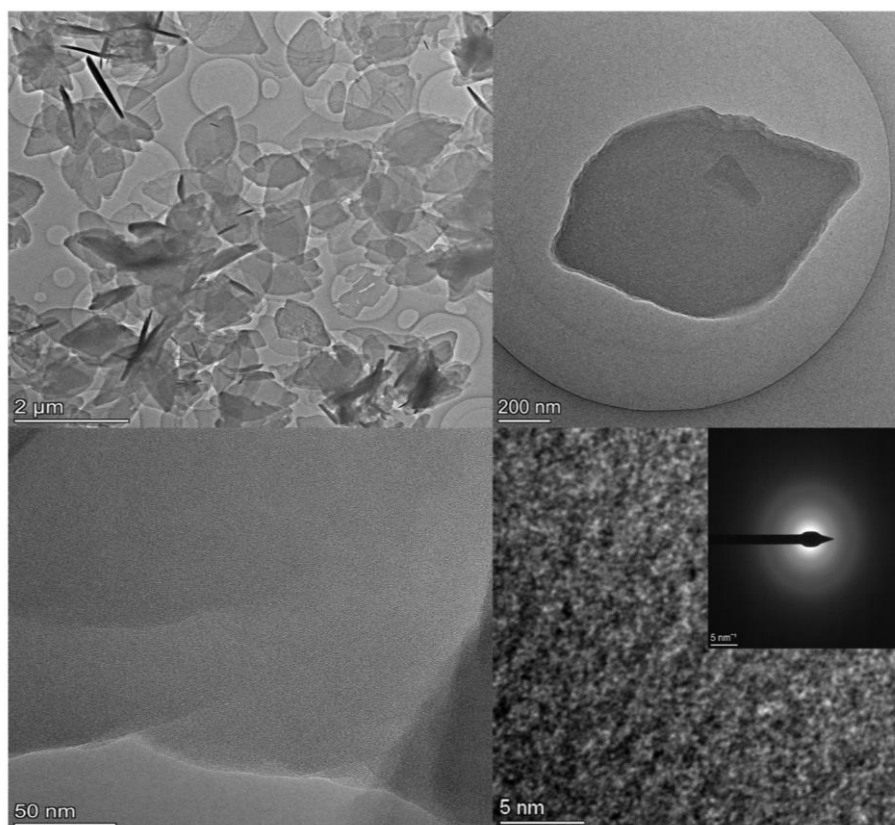
**Figure S7.**  $^1\text{H}$  NMR spectrums of digested (a) TEPE ligands and (b) SOFOUR-TEPE-Zn.



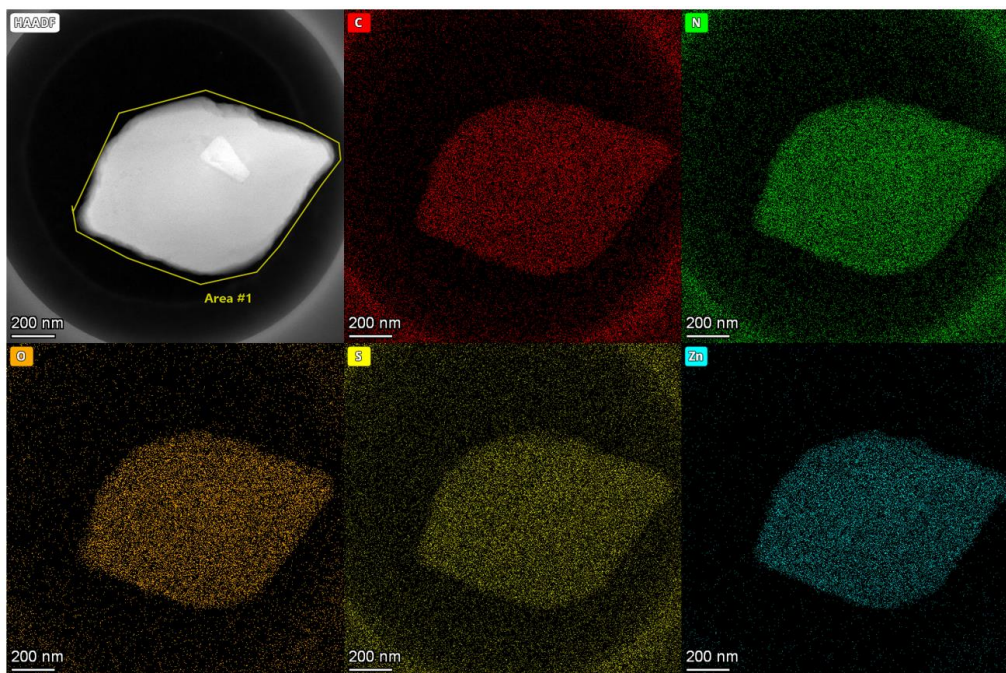
**Figure S8.**  $^{13}\text{C}$  NMR spectrums of digested (a) TEPE ligands and (b) SOFOUR-TEPE-Zn.



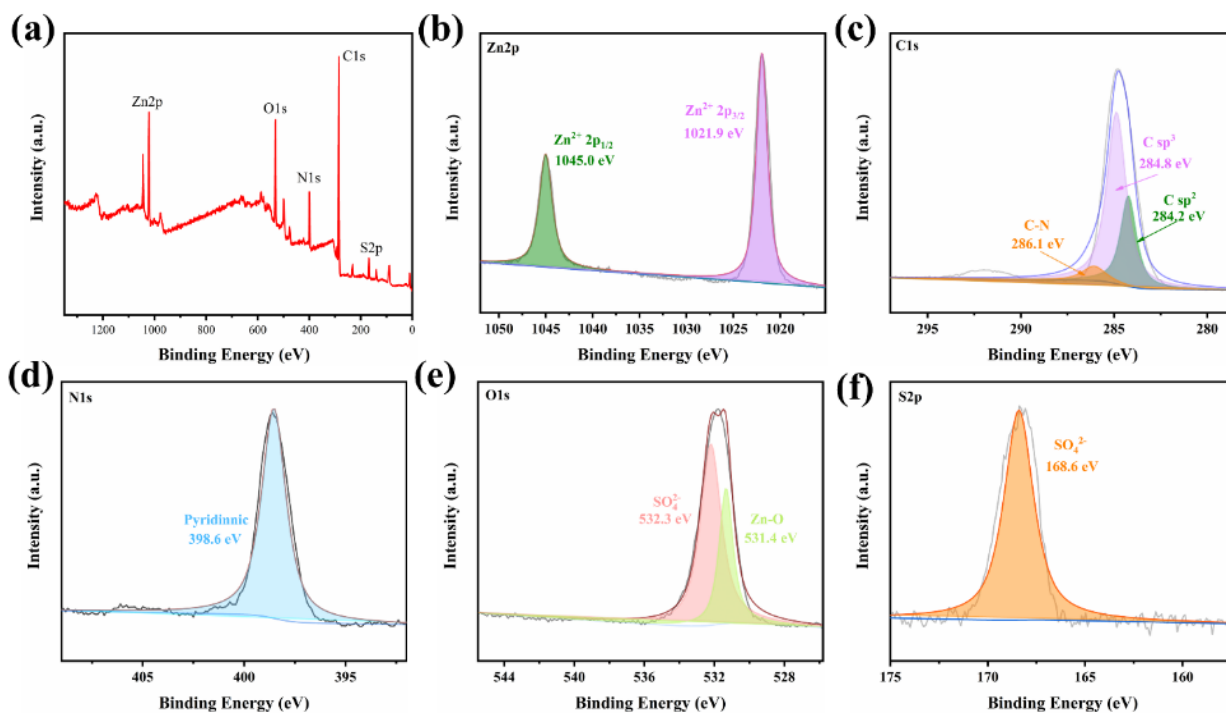
**Figure S9.** SEM image of SOFOUR-TEPE-Zn with the corresponding enlarged images.



**Figure S10.** TEM images of SOFOUR-TEPE-Zn with the corresponding enlarged images. Note: No obvious SAED pattern was observed due to the intolerance to the electron bombardment.



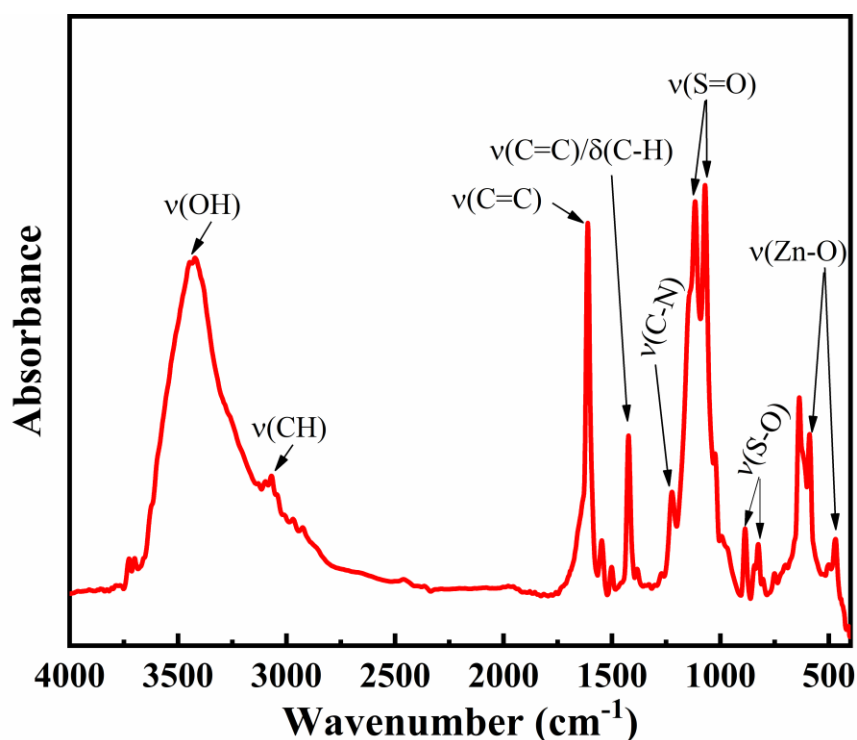
**Figure S11.** TEM-EDX elemental mapping of SOFOUR-TEPE-Zn.



**Figure S12.** Wide and high-resolution XPS spectra of SOFOUR-TEPE-Zn.

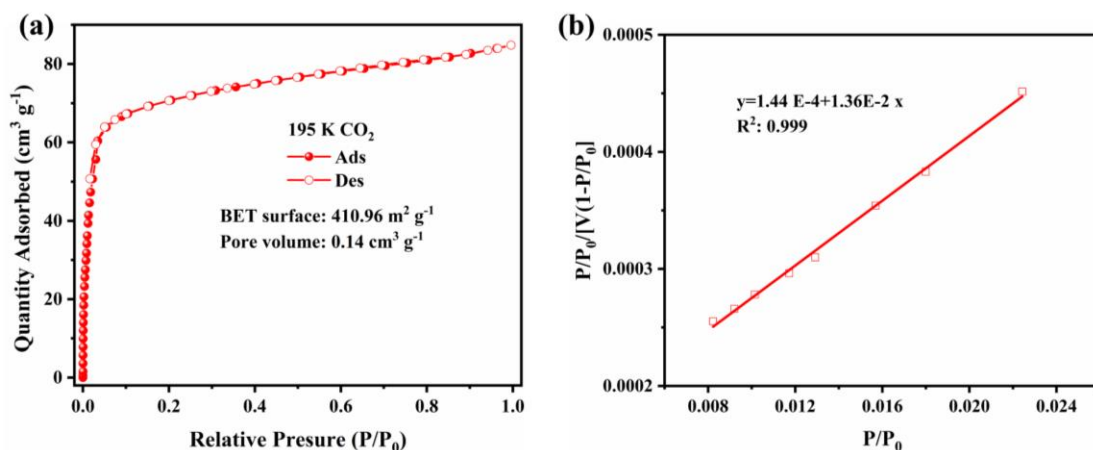
The wide XPS survey illustrated that SOFOUR-TEPE-Zn contained C, N, O, S, and Zn elements (Figure S12a). All the measured spectra are calibrated in energy at the binding energy (BE) of C 1s (284.8 eV) to adjust the surface charging effects. The high-resolution Zn 2p spectra displayed two

peaks at around 1045.0 and 1021.9 eV, corresponding to the Zn 2p<sub>1/2</sub> and Zn 2p<sub>3/2</sub> states, respectively (Figure S12b).<sup>[9]</sup> The high-resolution C 1s spectrum could be divided into three peaks, including the peaks of 284.2 and 286.1 eV for the sp<sup>2</sup> C and sp<sup>3</sup> C, and the peak at 286.1 eV for the C-N bond (Figure S12c).<sup>[10]</sup> The high-resolution N 1s spectrum displayed the characteristic peak of pyridinic-N at 398.6 eV (Figure S12d).<sup>[11]</sup> The high-resolution O 1s spectrum could be divided into two peaks at 523.3 and 531.4 eV, attributing to the sulfate-O and Zn-O bonds (Figure S12e).<sup>[12-14]</sup> The peak at 168.6 eV in the high-resolution S 2p spectrum belonged to the sulfate-S (Figure S12f).<sup>[15]</sup>

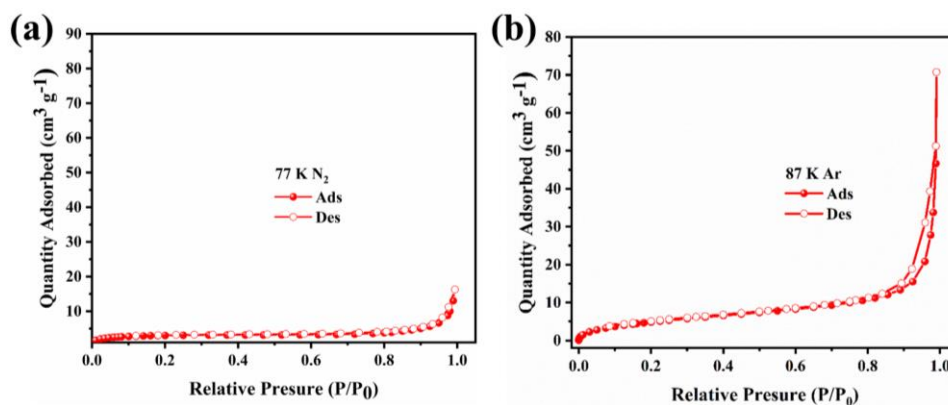


**Figure S13.** The FT-IR spectrum of the SOFOUR-TEPE-Zn.

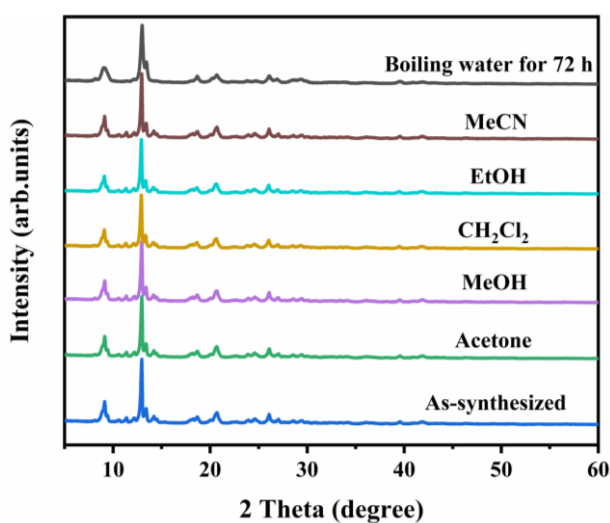
The broad peak at 3422.1 cm<sup>-1</sup> was attributed to the stretching vibration of -OH group due to the water molecules in the framework. The peak at 1611.4 cm<sup>-1</sup> corresponded to the stretching vibration of C=C bond. The small peaks at 1547.0 and 1501.5 cm<sup>-1</sup> were attributed to the N-H bending vibration of amide II, and the small peak at 1223.3 cm<sup>-1</sup> was the N-H bending vibration of amide III. The peak at 1423.6 cm<sup>-1</sup> belonged to the stretching vibration of C=C or the bending vibration of C-H in the pyridine ring. The strong peaks at 1116.6 and 1071.0 cm<sup>-1</sup> can be attributed to the antisymmetric stretching vibrations of S=O in SO<sub>4</sub><sup>2-</sup> groups.<sup>[16]</sup> The small peaks at 886.3 and 825.8 cm<sup>-1</sup> belonged to the stretching vibration of S-O. The peaks at 589.3 and 469.3 cm<sup>-1</sup> corresponded to the Zn-O stretching vibrations.<sup>[16-18]</sup>



**Figure S14.** (a) CO<sub>2</sub> adsorption isotherm of SOFOUR-TEPE-Zn at 195 K; (b) BET calculation plot for SOFOUR-TEPE-Zn based on its corresponding CO<sub>2</sub> adsorption isotherm at 195 K.

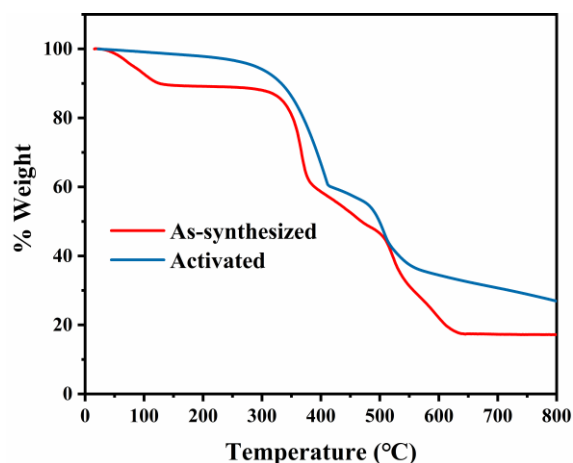


**Figure S15.** (a) N<sub>2</sub> adsorption isotherm at 77 K and (b) Ar adsorption isotherm at 87 K of SOFOUR-TEPE-Zn.

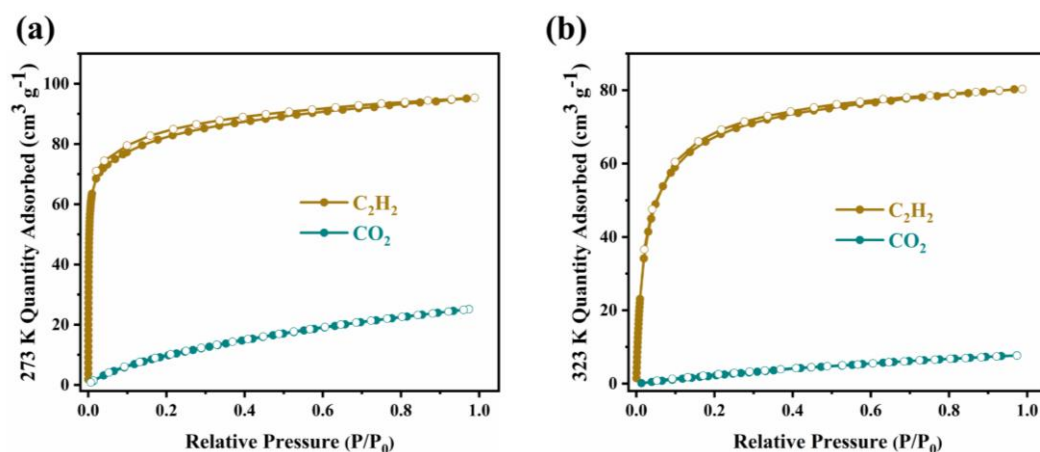


**Figure S16.** PXRD patterns of SOFOUR-TEPE-Zn after immersing in different solvents for 10 days and boiling water for 72 h.

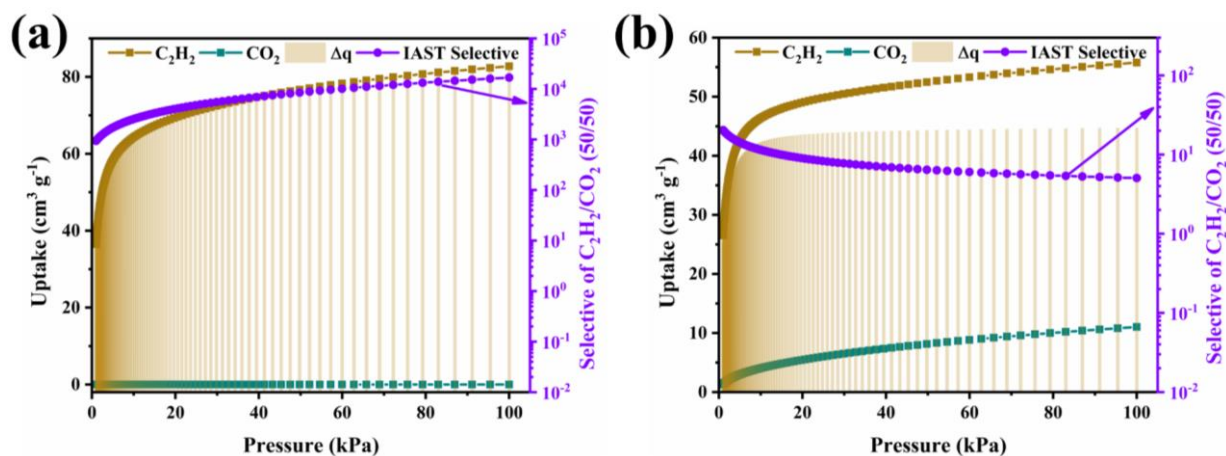




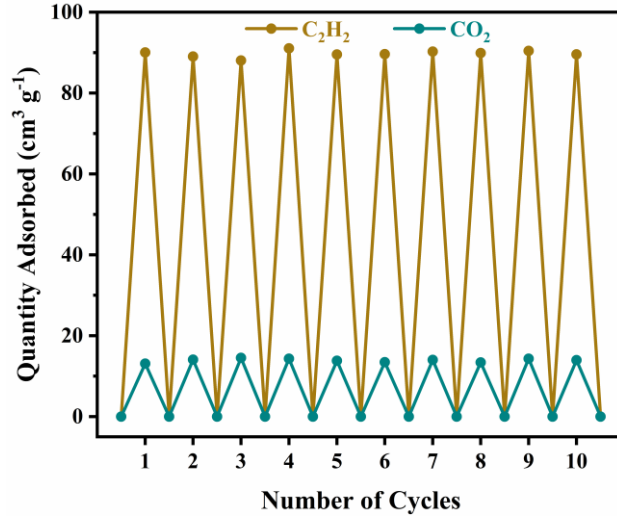
**Figure S17.** TGA curves of as-synthesized and activated SOFOUR-TEPE-Zn.



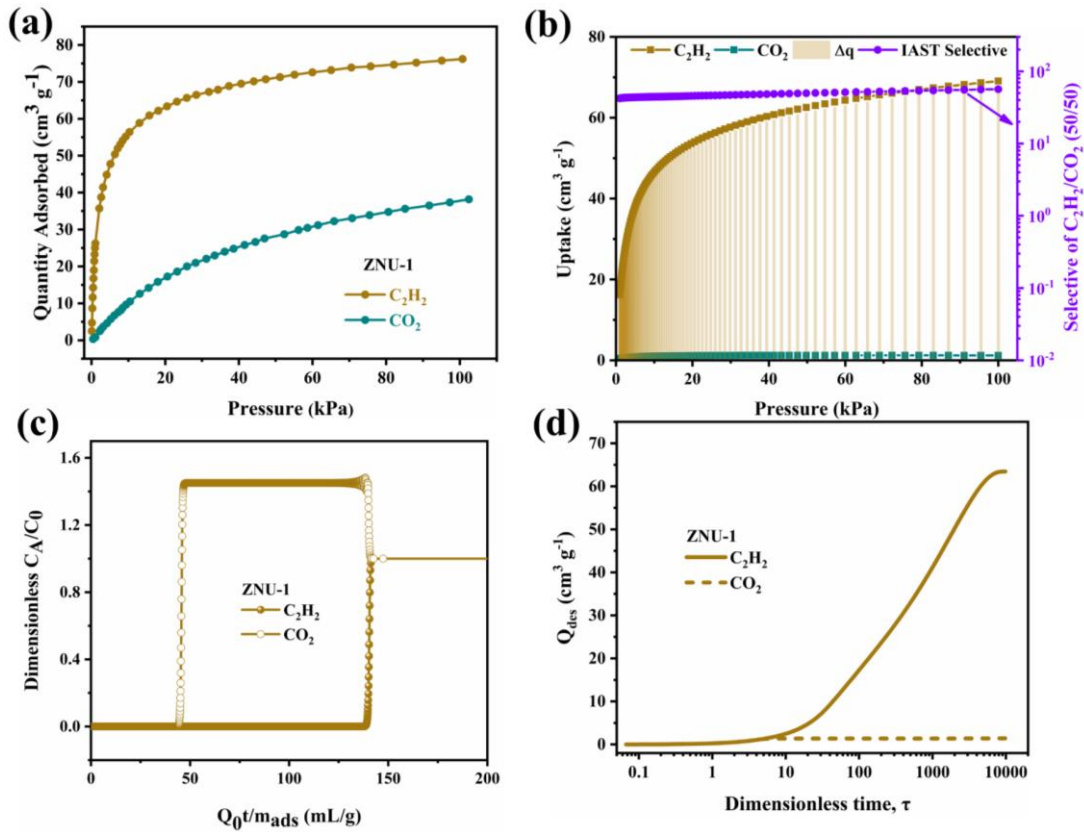
**Figure S18.** Adsorption isotherms of  $C_2H_2$  and  $CO_2$  on SOFOUR-TEPE-Zn at (a) 273 K and (b) 323 K.



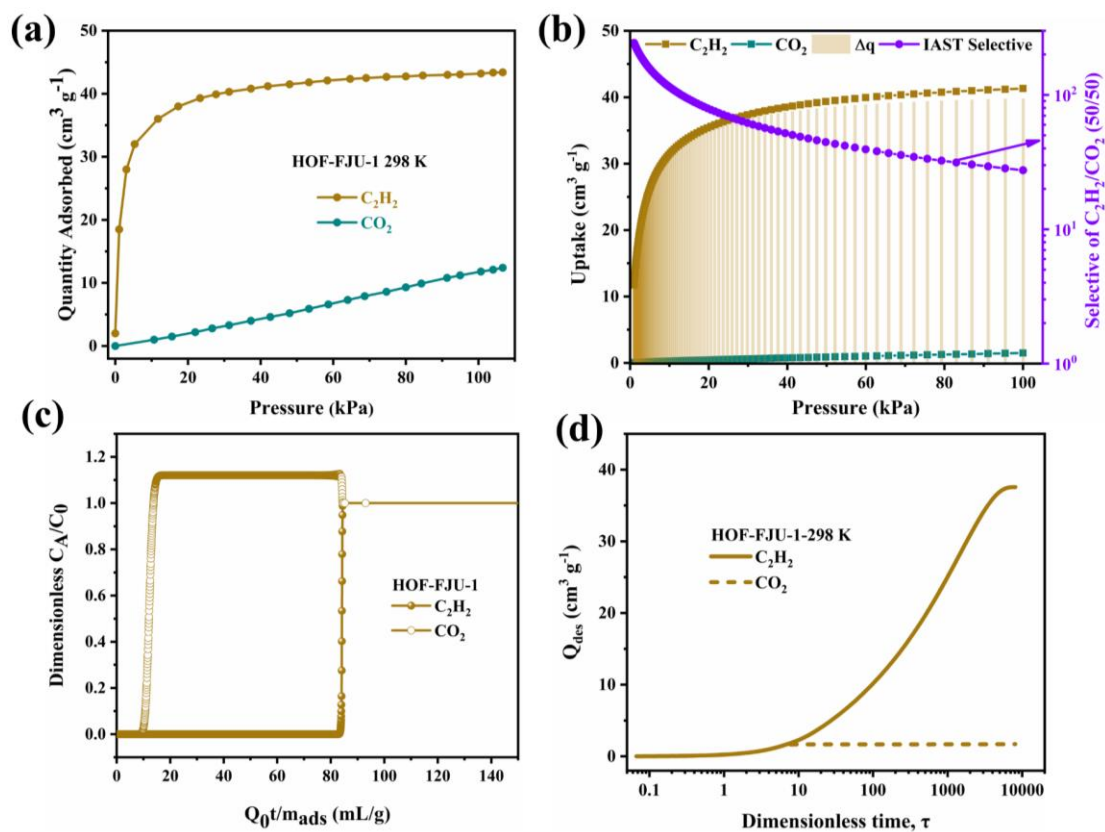
**Figure S19.** Predicted mixture adsorption isotherms and selectivity of (a) SOFOUR-TEPE-Zn and (b) SOFOUR-1-Zn based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K.



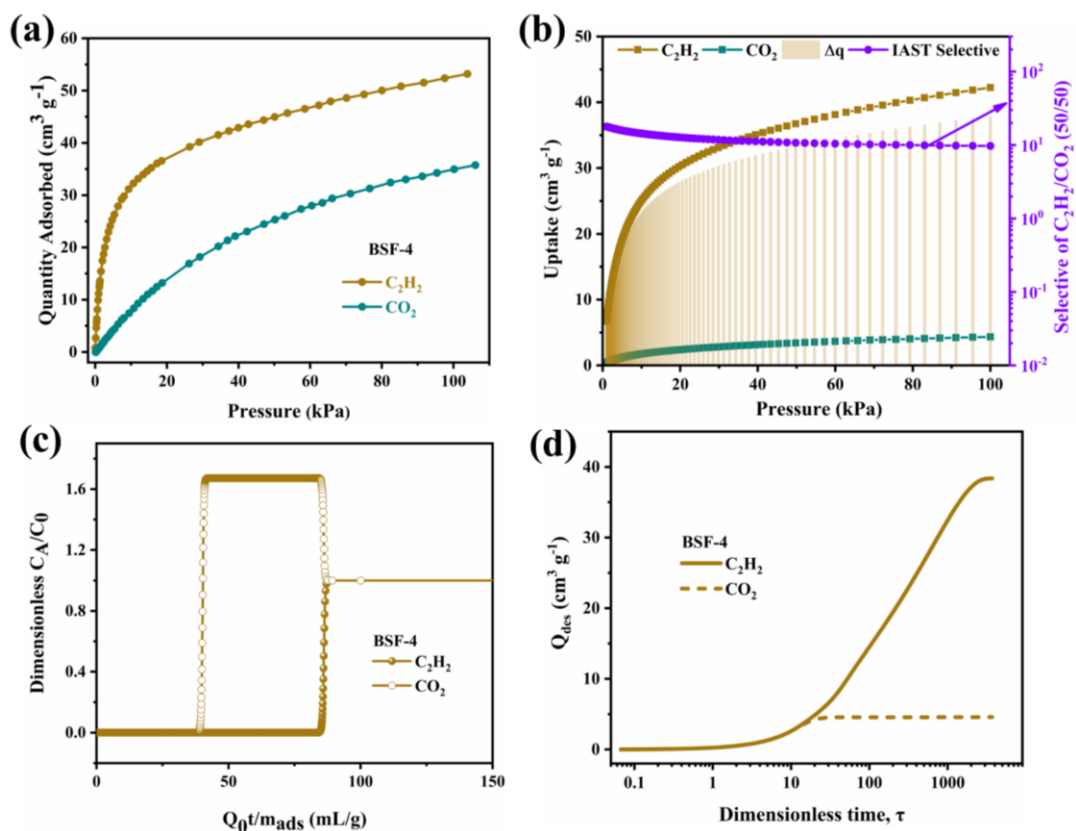
**Figure S20.** The 10 adsorption cycles of  $C_2H_2$  and  $CO_2$  at 298 K.



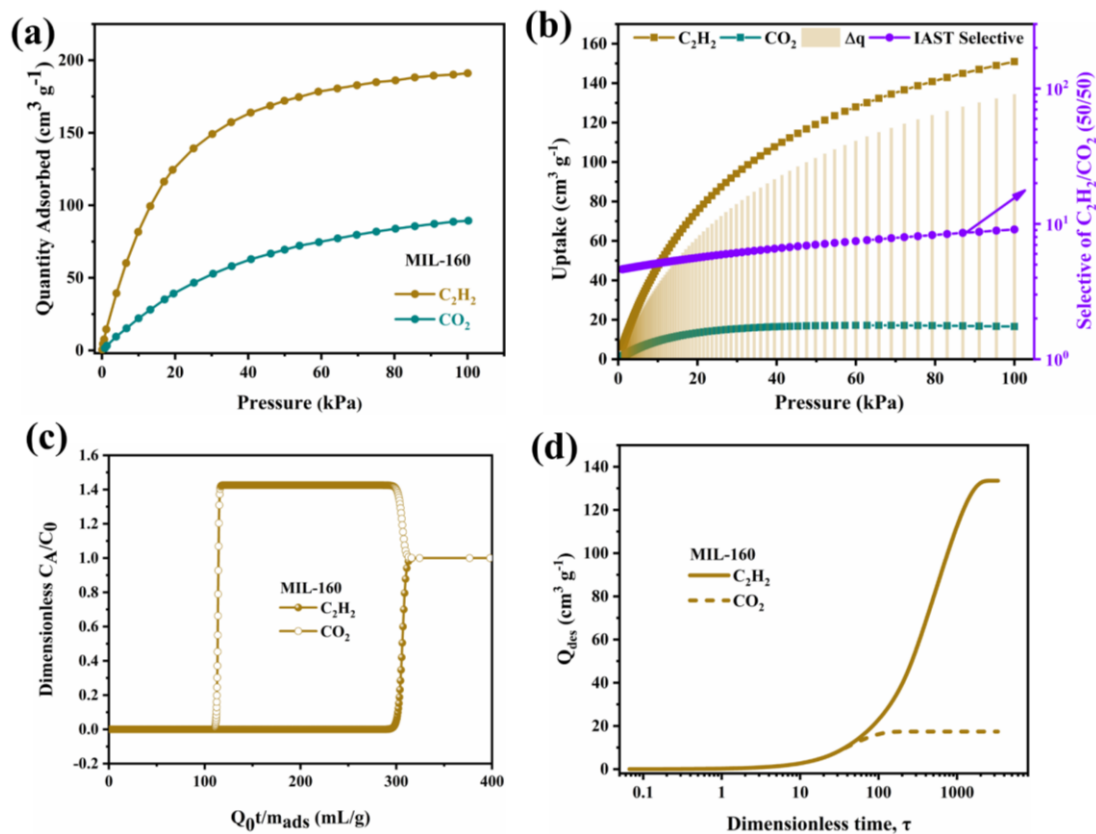
**Figure S21.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for ZNU-1 at 298 K.<sup>[19]</sup> (b) Predicted mixture adsorption isotherms and selectivity of ZNU-1 based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with ZNU-1 operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for ZNU-1.



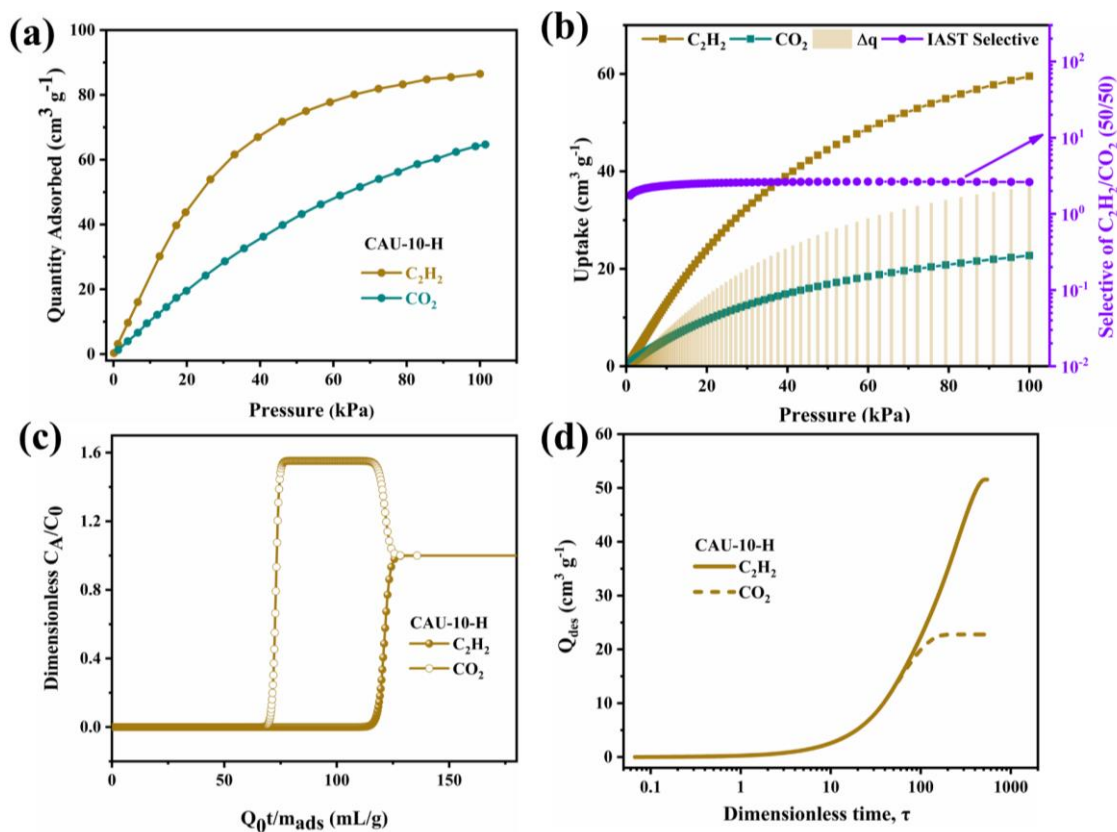
**Figure S22.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for HOF-FJU-1 at 298 K.<sup>[4]</sup> (b) Predicted mixture adsorption isotherms and selectivity of HOF-FJU-1 based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with HOF-FJU-1 operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for HOF-FJU-1.



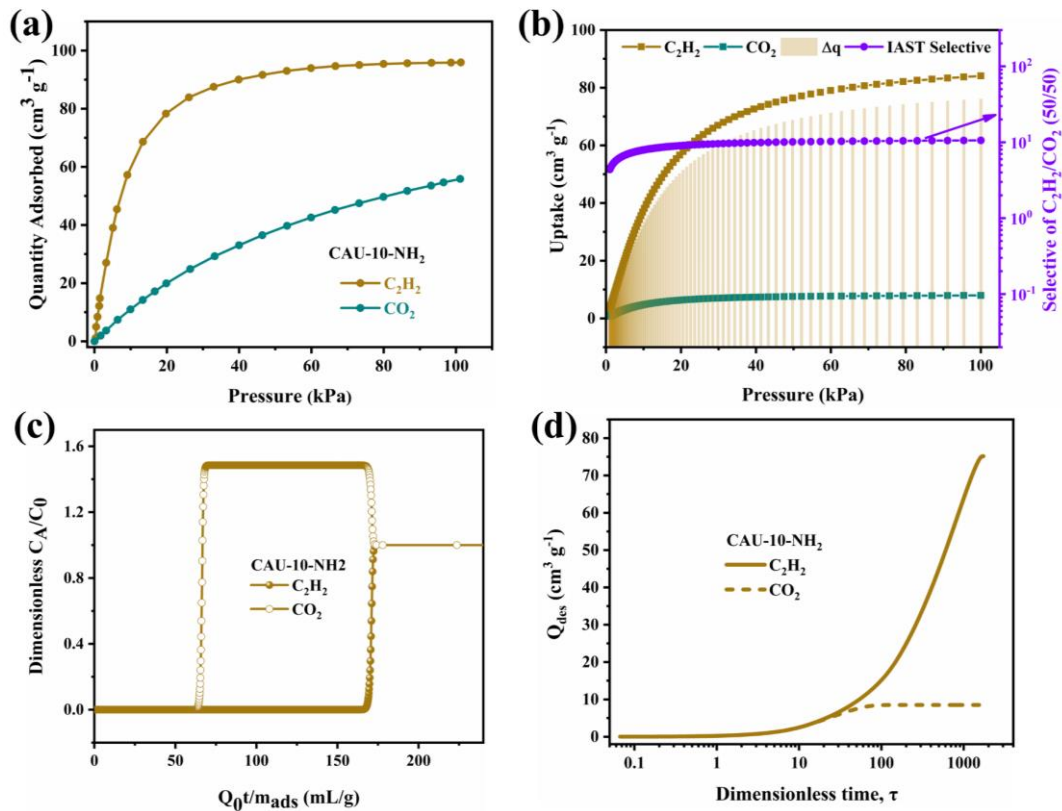
**Figure S23.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for BSF-4 at 298 K.<sup>[19]</sup> (b) Predicted mixture adsorption isotherms and selectivity of BSF-4 based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with BSF-4 operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for BSF-4.



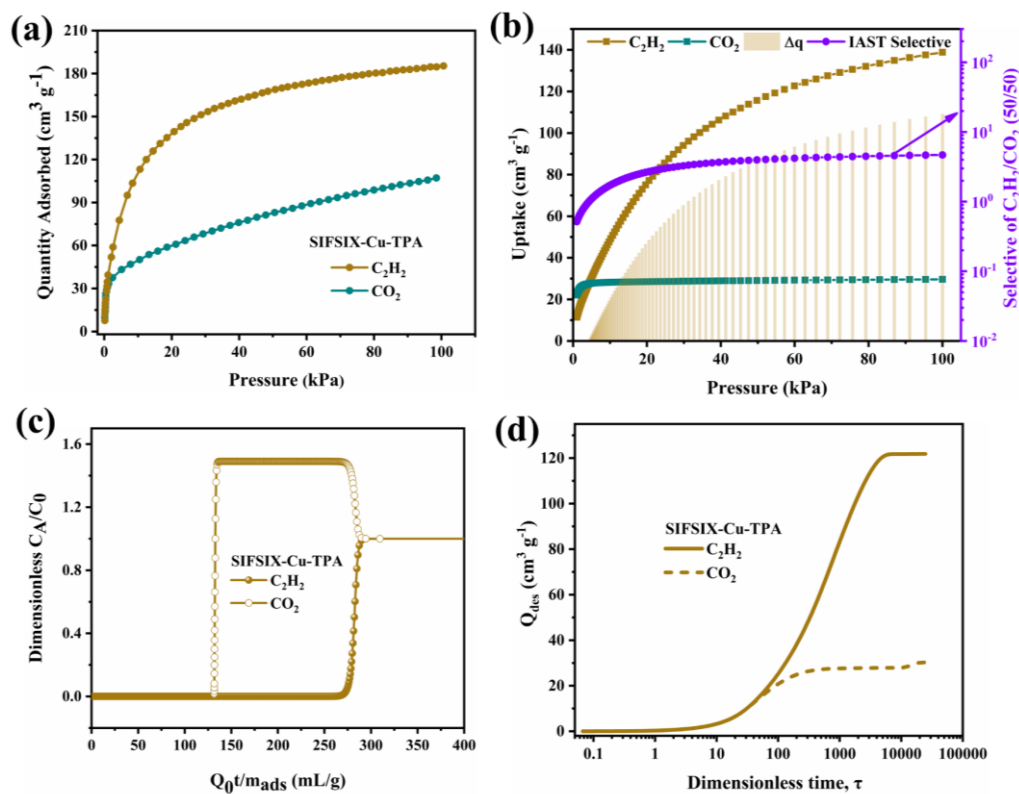
**Figure S24.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for MIL-160 at 298 K.<sup>[20]</sup> (b) Predicted mixture adsorption isotherms and selectivity of MIL-160 based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with MIL-160 operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for MIL-160.



**Figure S25.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for CAU-10-H at 298 K.<sup>[21]</sup> (b) Predicted mixture adsorption isotherms and selectivity of CAU-10-H based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with CAU-10-H operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for CAU-10-H.

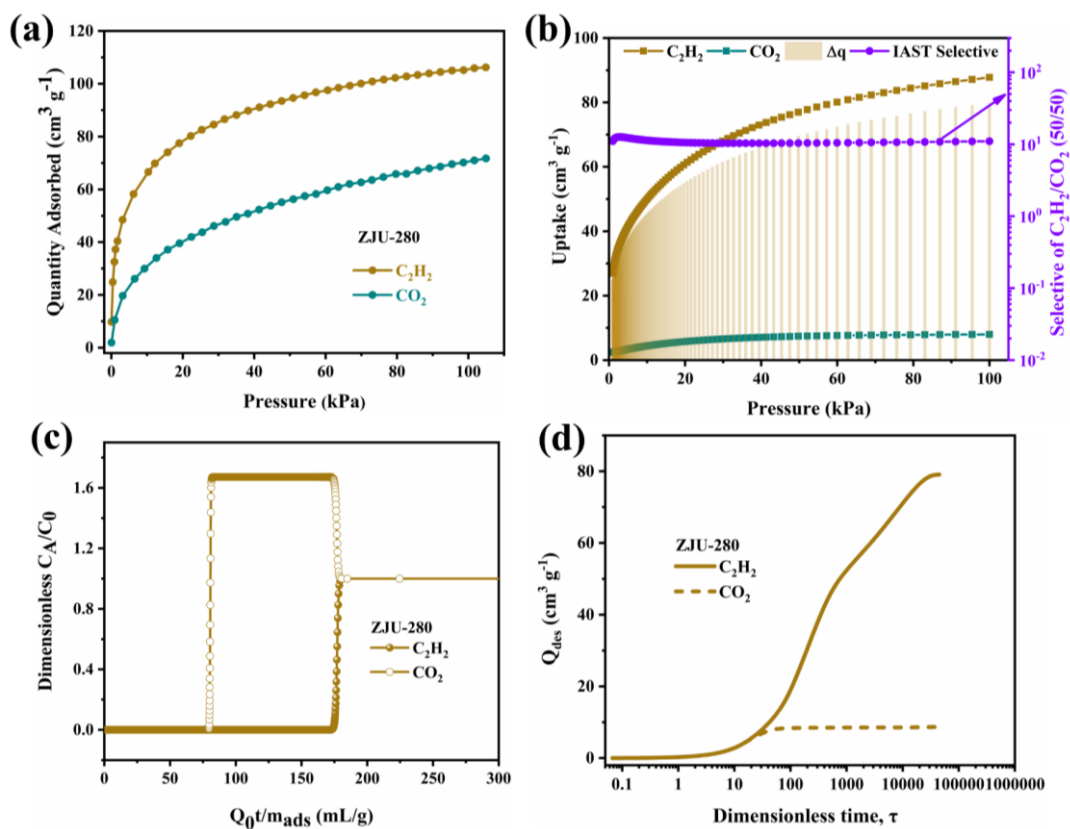


**Figure S26.** (a) C<sub>2</sub>H<sub>2</sub> and CO<sub>2</sub> adsorption isotherms for CAU-10-NH<sub>2</sub> at 298 K.<sup>[22]</sup> (b) Predicted mixture adsorption isotherms and selectivity of CAU-10-NH<sub>2</sub> based on IAST method for a 50:50 C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> mixture at 298 K. (c) Simulated breakthrough curve for 50/50 C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> mixtures in fixed bed packed with CAU-10-NH<sub>2</sub> operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for CAU-10-NH<sub>2</sub>.

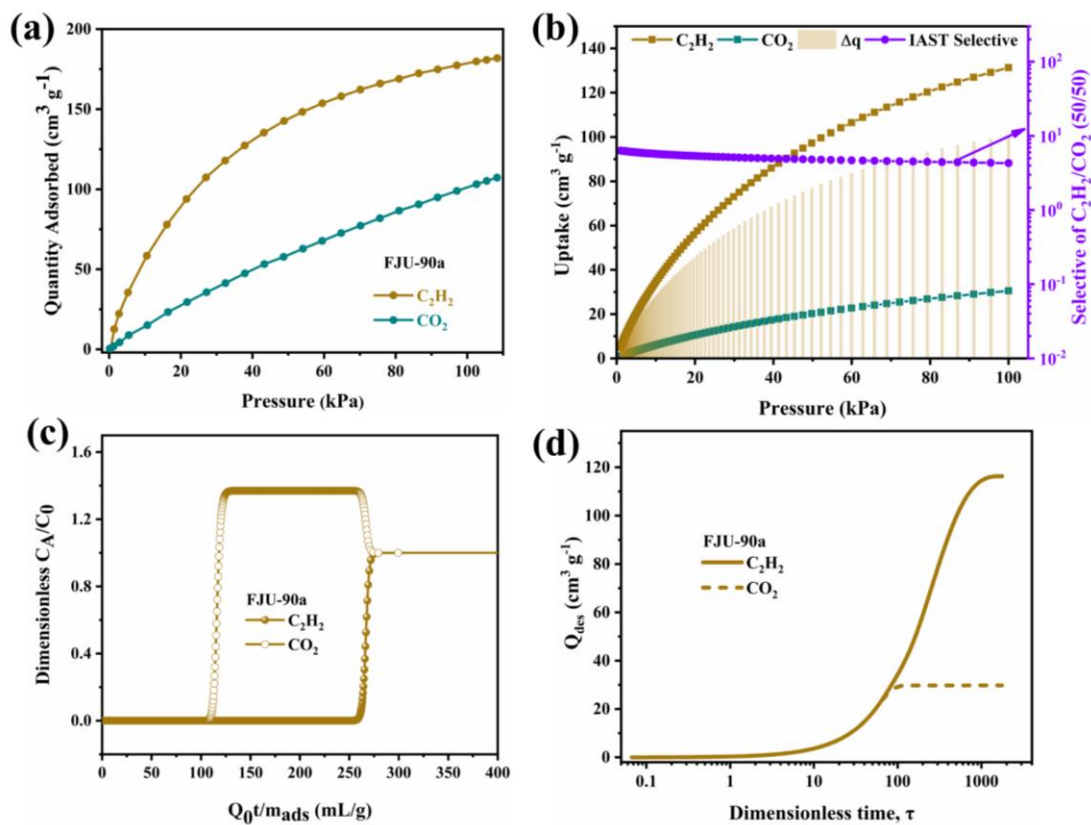


**Figure S27.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for SIFSIX-Cu-TPA at 298 K.<sup>[23]</sup> (b) Predicted mixture adsorption isotherms and selectivity of SIFSIX-Cu-TPA based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with SIFSIX-Cu-TPA operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for SIFSIX-Cu-TPA.

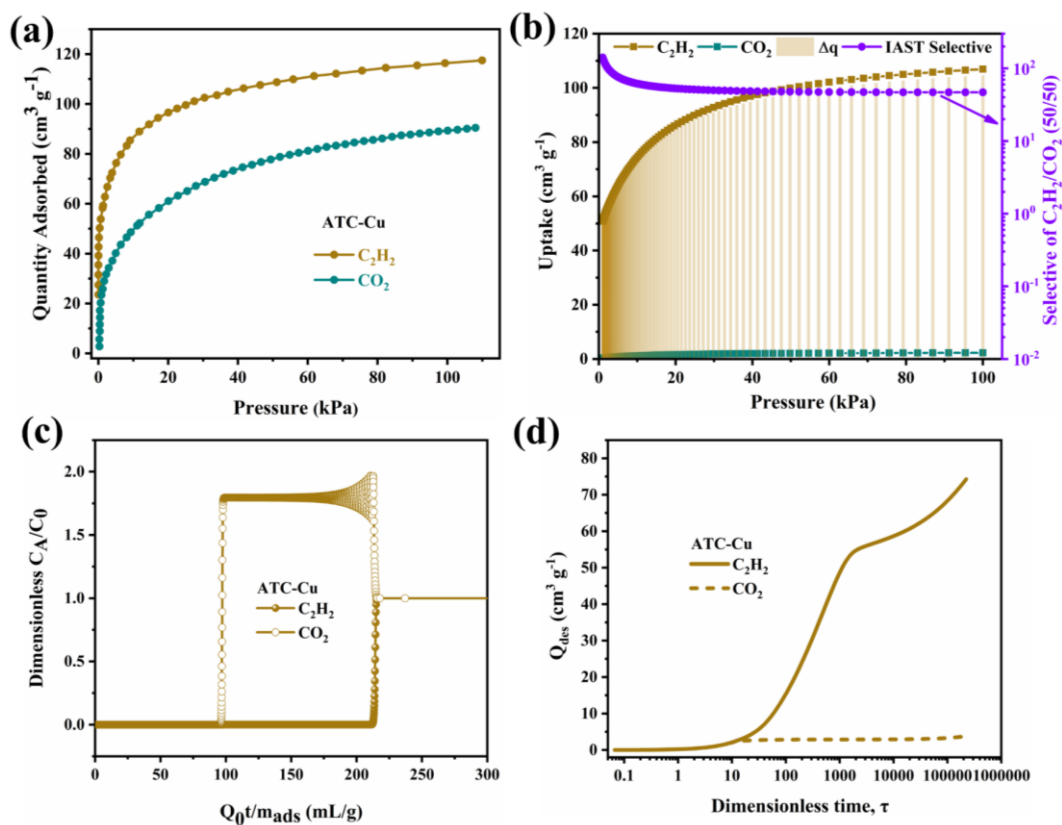




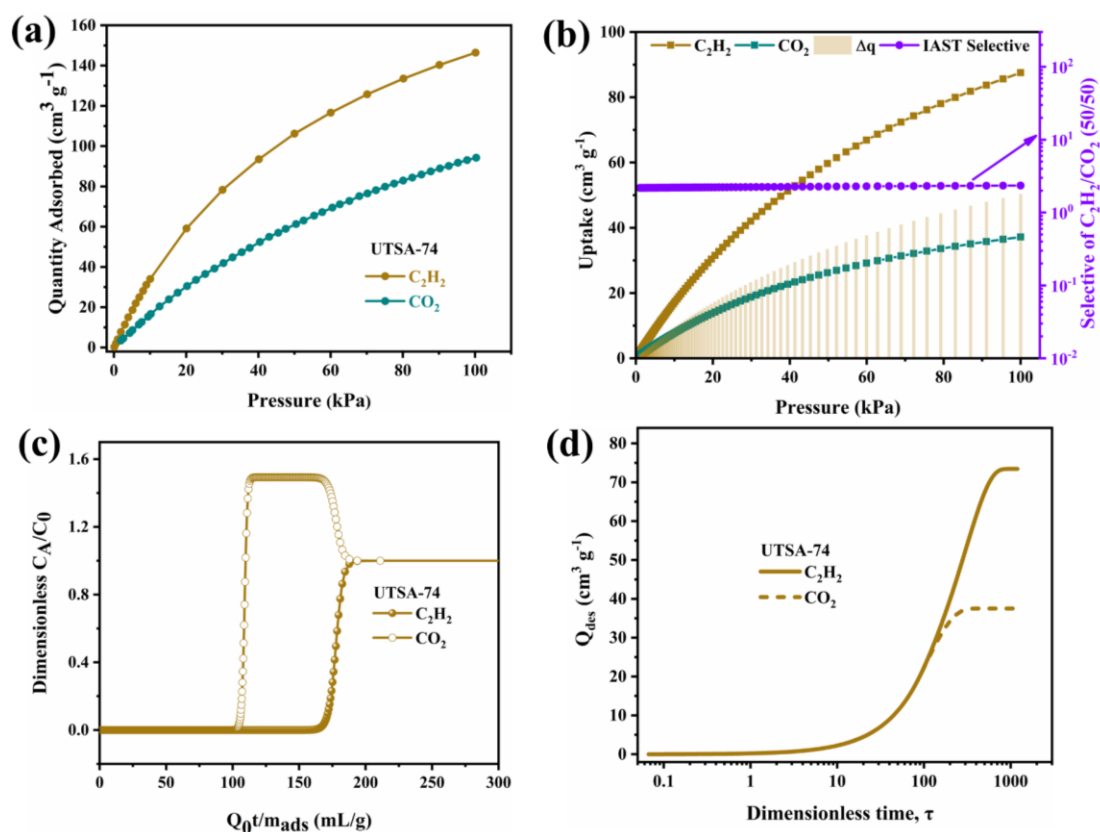
**Figure S28.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for ZJU-280 at 298 K.<sup>[24]</sup> (b) Predicted mixture adsorption isotherms and selectivity of ZJU-280 based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with ZJU-280 operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for ZJU-280.



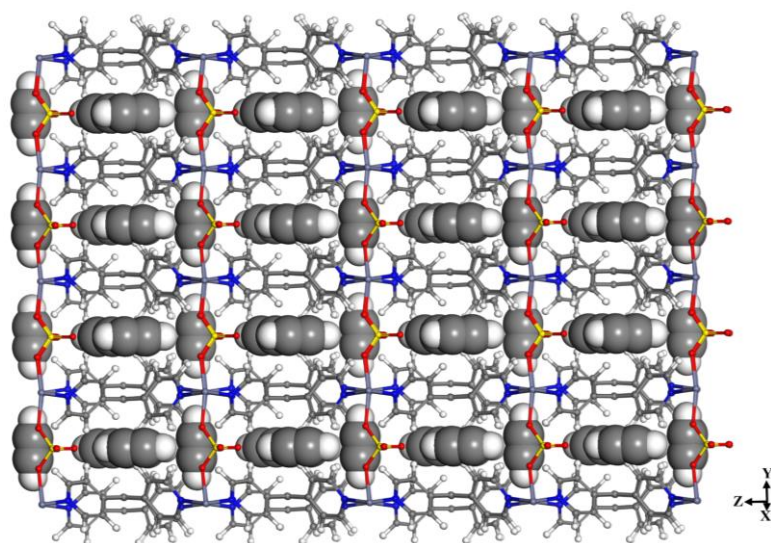
**Figure S29.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for FJU-90a at 298 K.<sup>[25]</sup> (b) Predicted mixture adsorption isotherms and selectivity of FJU-90a based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with FJU-90a operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for FJU-90a.



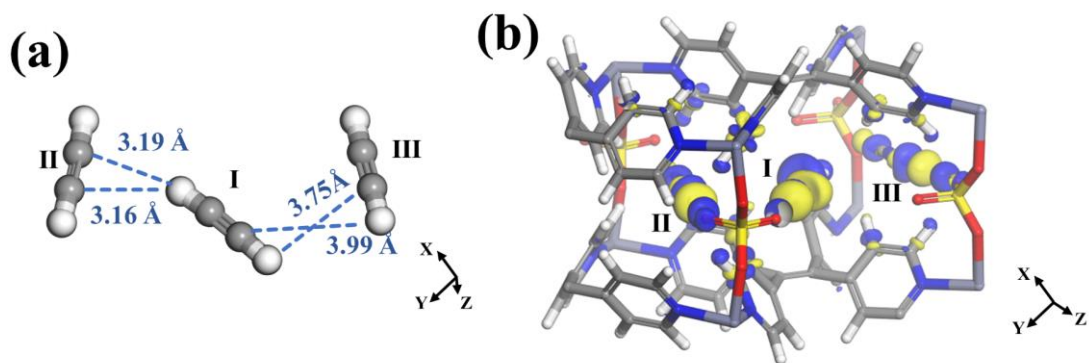
**Figure S30.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for ATC-Cu at 298 K.<sup>[26]</sup> (b) Predicted mixture adsorption isotherms and selectivity of ATC-Cu based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with ATC-Cu operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for ATC-Cu.



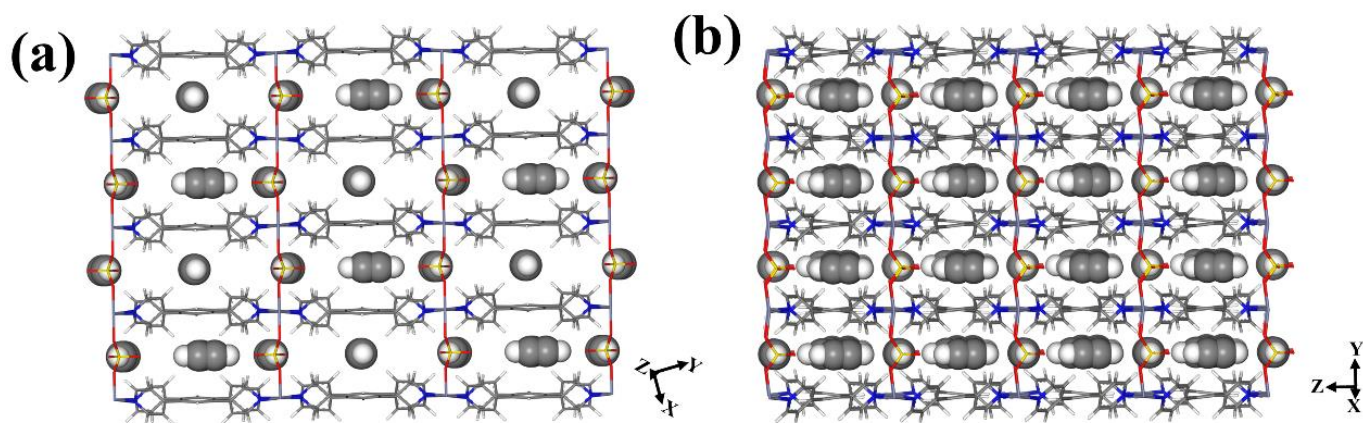
**Figure S31.** (a)  $C_2H_2$  and  $CO_2$  adsorption isotherms for UTSA-74 at 298 K.<sup>[27]</sup> (b) Predicted mixture adsorption isotherms and selectivity of UTSA-74 based on IAST method for a 50:50  $C_2H_2/CO_2$  mixture at 298 K. (c) Simulated breakthrough curve for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with UTSA-74 operating at 298 K and 100 kPa. (d) Simulations of counter-current blowdown operations for UTSA-74.



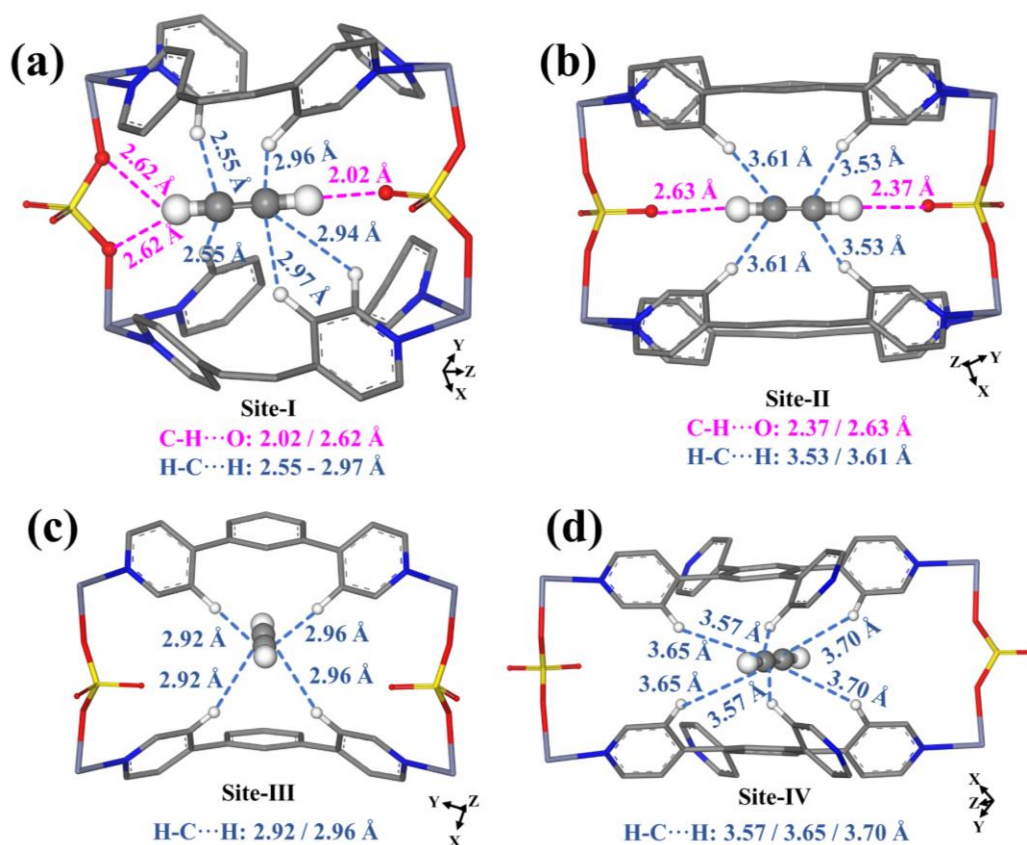
**Figure S32.** Dense packing of  $C_2H_2$  molecules in SOFOUR-TEPE-Zn.



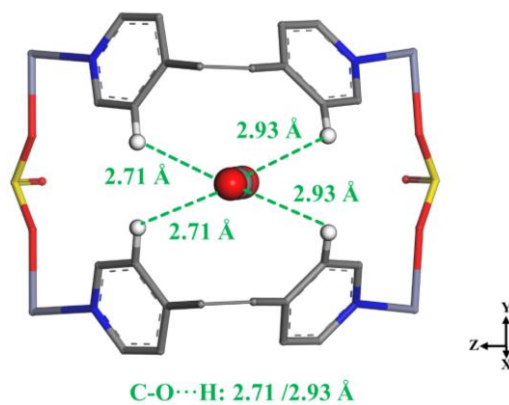
**Figure S33.** (a) Guest-guest interactions between  $C_2H_2$  molecules; (b) Charge density difference plots showing the interactions between framework and  $C_2H_2$  (Sites I-III).



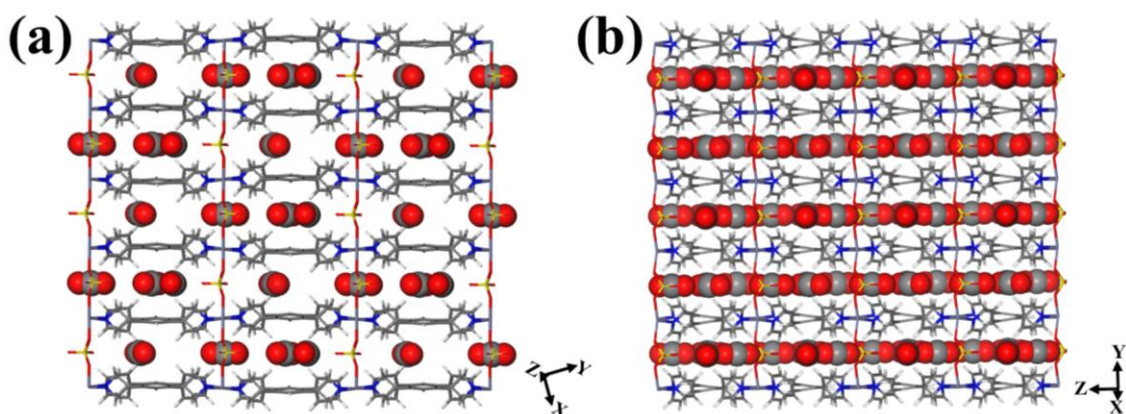
**Figure S34.** The packing pattern of  $C_2H_2$  molecules in SOFOUR-1-Zn: (a) viewed along the  $Z$ -axis and (b) viewed along the  $X$ -axis.



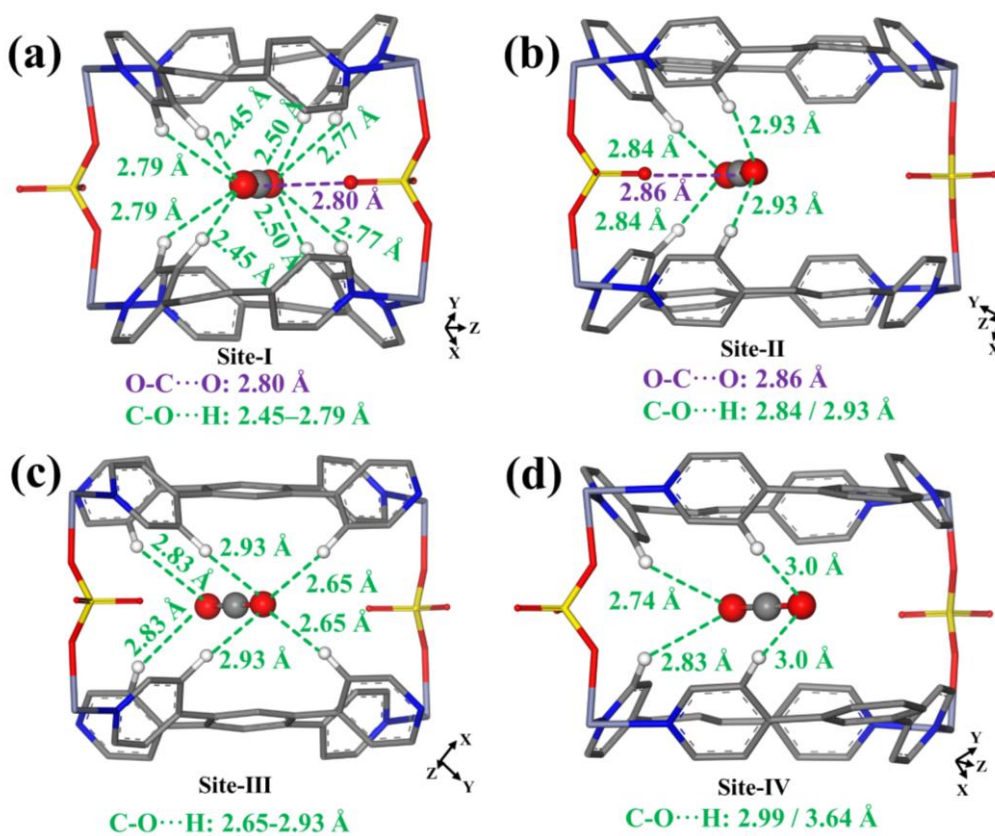
**Figure S35.**  $\text{C}_2\text{H}_2$  binding sites in SOFOUR-1-Zn by DFT calculations.



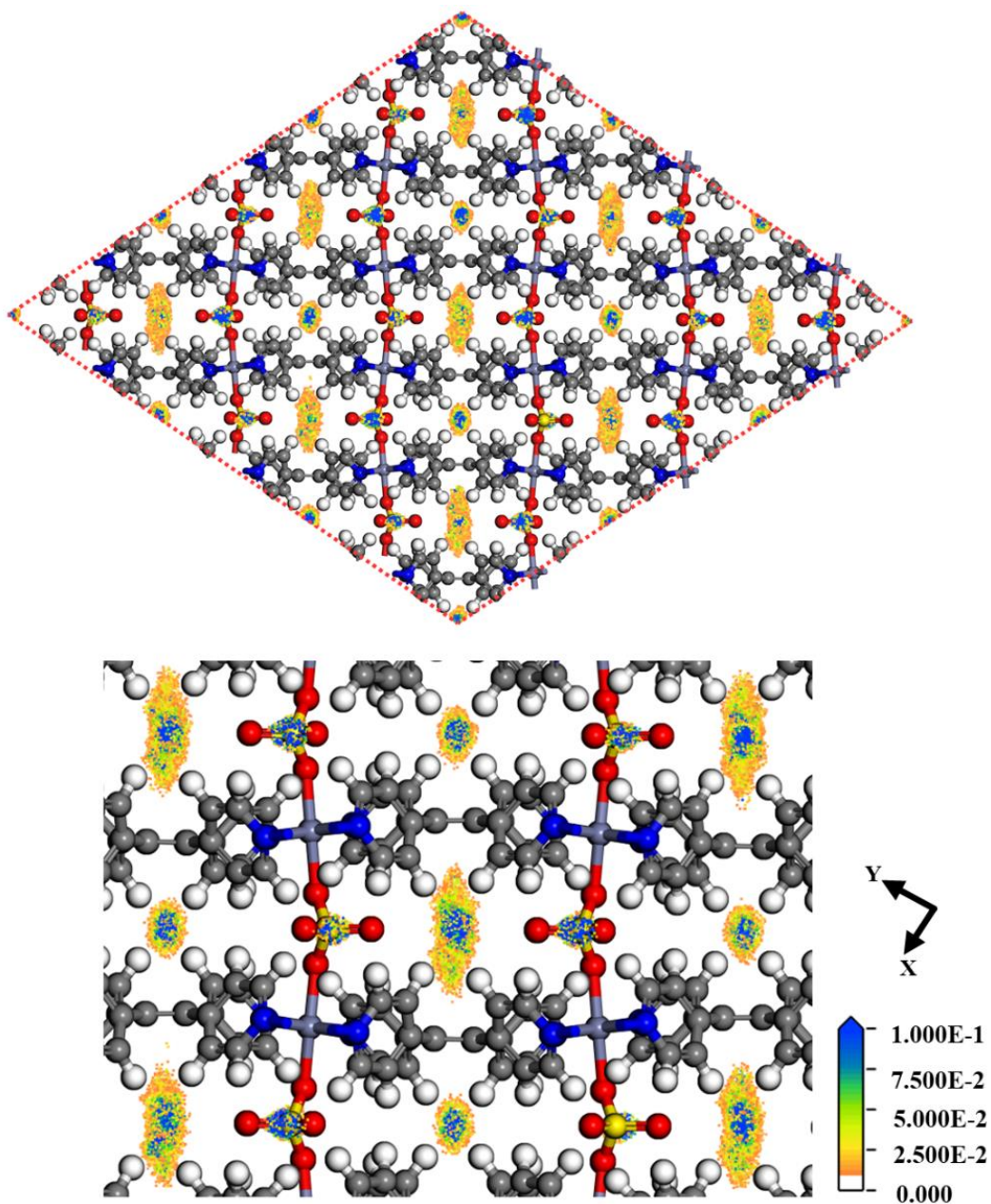
**Figure S36.** DFT-derived  $\text{CO}_2$  binding site in SOFOUR-TEPE-Zn ( $\Delta E = -33.38 \text{ kJ mol}^{-1}$ )



**Figure S37.** The packing pattern of CO<sub>2</sub> molecules in SOFOUR-1-Zn: (a) viewed along the Z-axis and (b) viewed along the X-axis.

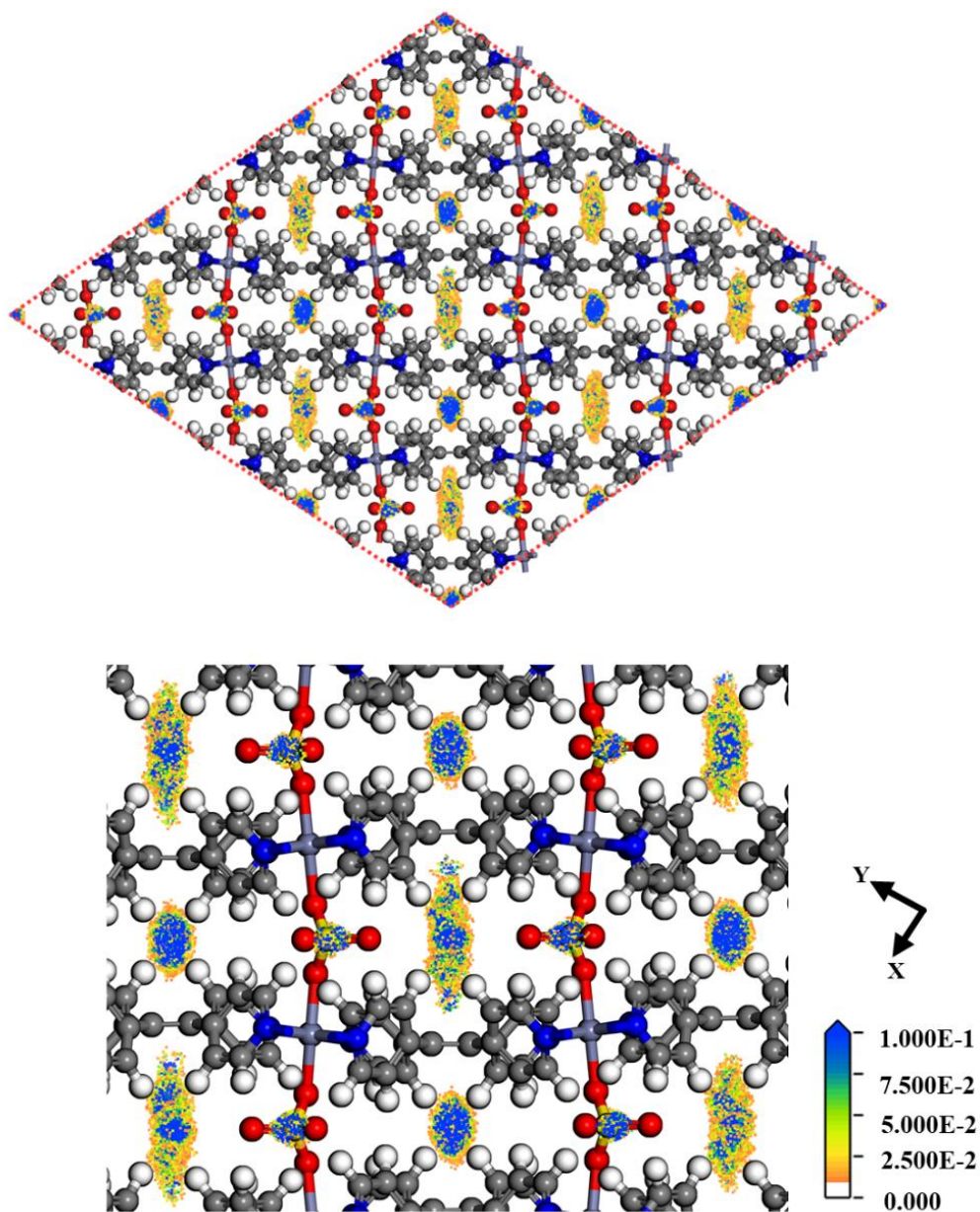


**Figure S38.** CO<sub>2</sub> binding sites in SOFOUR-1-Zn by DFT calculations.

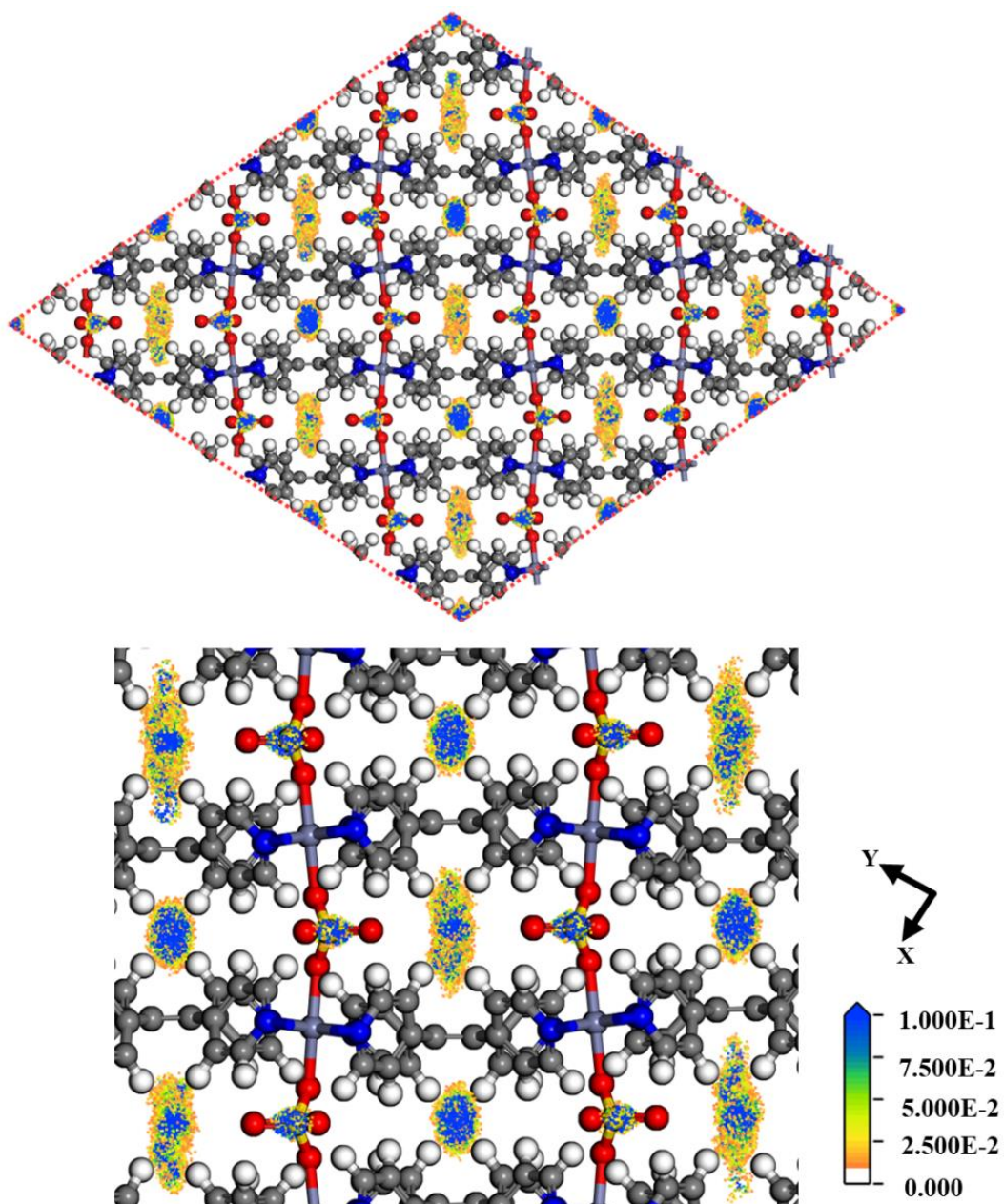


**Figure S39.** GCMC simulations for the distribution density of C<sub>2</sub>H<sub>2</sub> in SOFOUR-TEPE-Zn at 1 kPa.

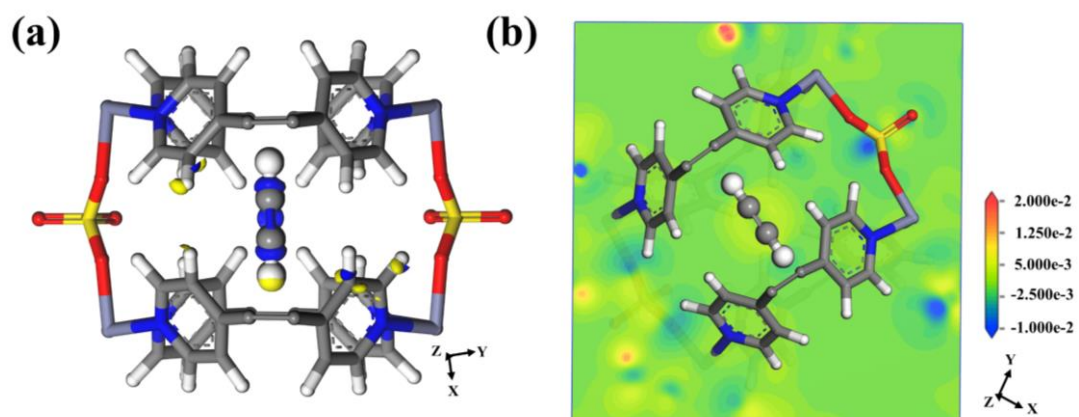




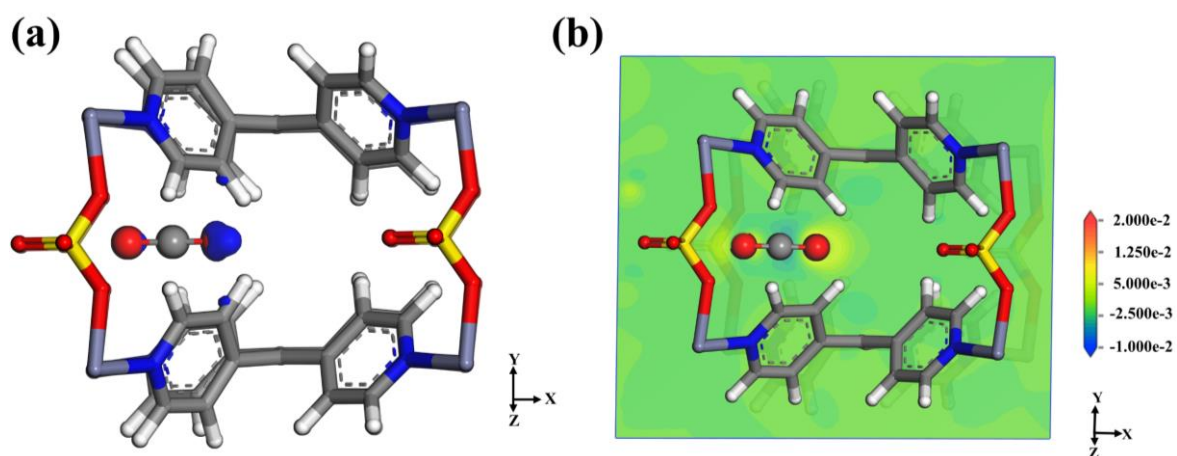
**Figure S40.** GCMC simulations for the distribution density of  $C_2H_2$  in SOFOUR-TEPE-Zn at 50 kPa.



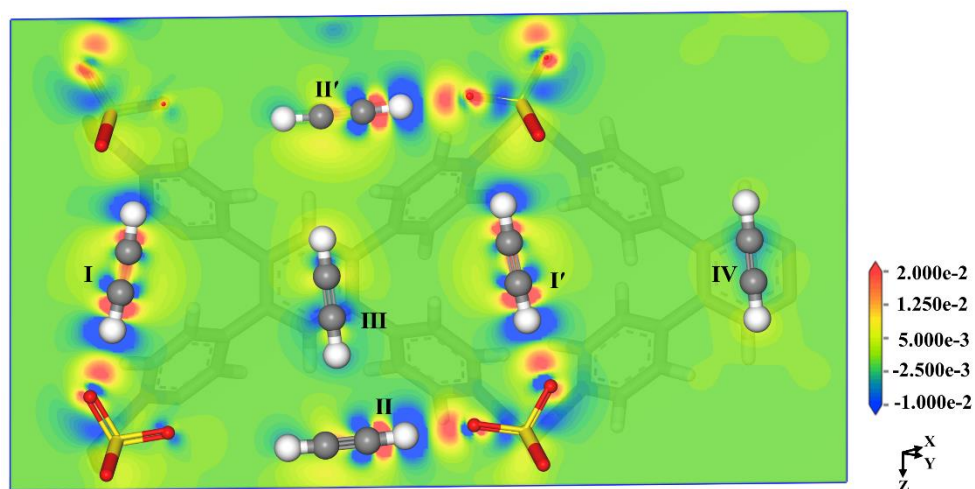
**Figure S41.** GCMC simulations for the distribution density of  $C_2H_2$  in SOFOUR-TEPE-Zn at 100 kPa.



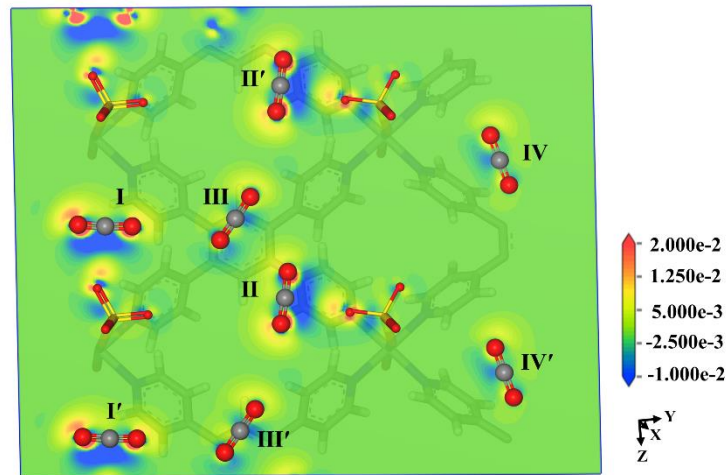
**Figure S42.** Charge density difference plots showing the interaction between framework and  $C_2H_2$  (Site IV).



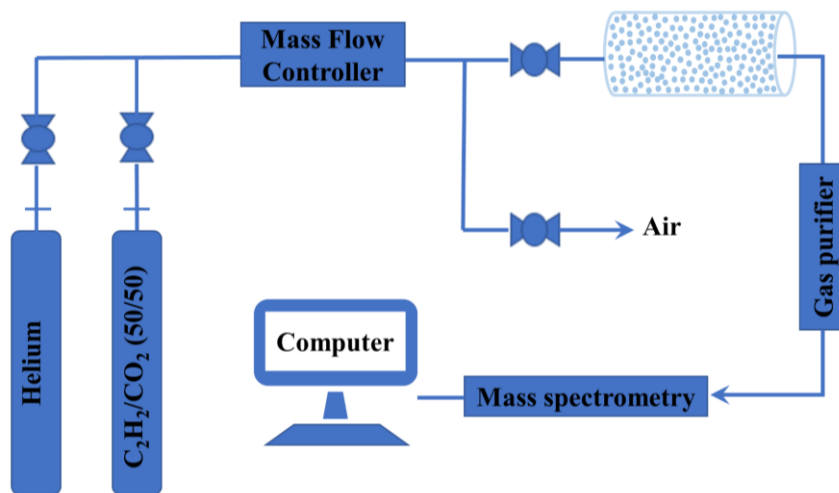
**Figure S43.** Charge density difference plots showing the interaction between framework and  $CO_2$ .



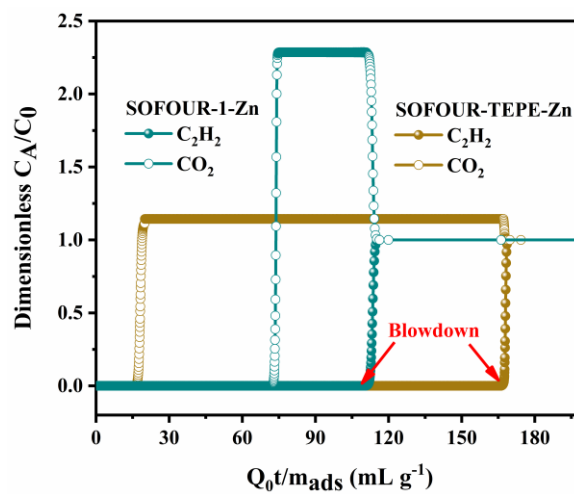
**Figure S44.** Charge density difference plots of  $C_2H_2$ -loaded in SOFOUR-1-Zn.



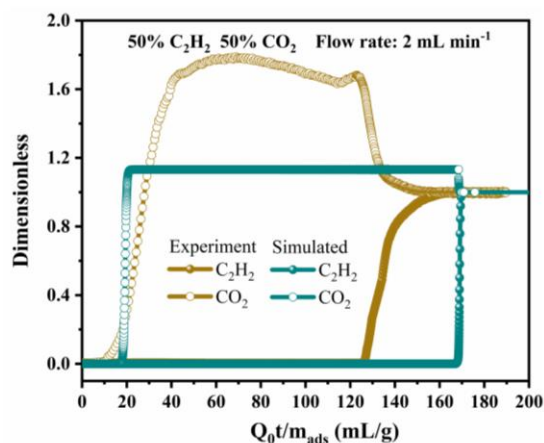
**Figure S45.** Charge density difference plots of CO<sub>2</sub>-loaded in SOFOUR-1-Zn.



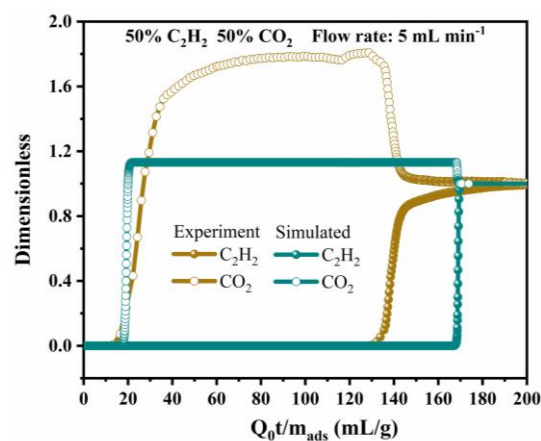
**Figure S46.** Breakthrough experiments apparatus.



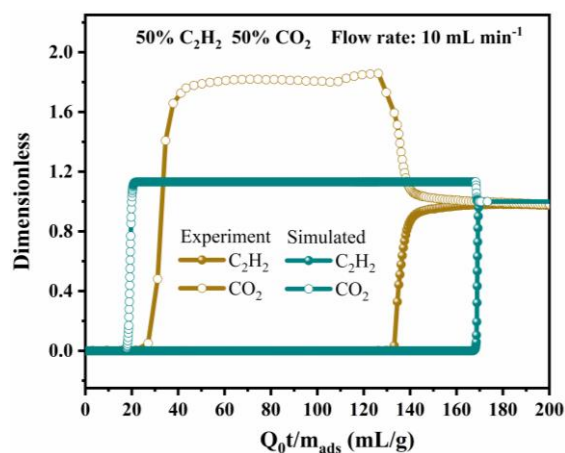
**Figure S47.** Simulated breakthrough curves for 50/50 C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> mixtures in fixed bed packed with SOFOUR-TEPE-Zn and SOFOUR-1-Zn operating at 298 K and 100 kPa.



**Figure S48.** Comparison of experimental and simulated breakthrough curves for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with SOFOUR-TEPE-Zn operating at 298 K and 100 kPa. The flow rate at the inlet is  $2.0 \text{ mL min}^{-1}$ .

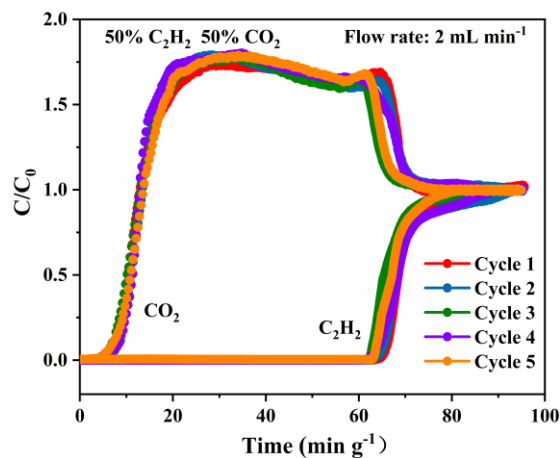


**Figure S49.** Comparison of experimental and simulated breakthrough curves for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with SOFOUR-TEPE-Zn operating at 298 K and 100 kPa. The flow rate at the inlet is  $5.0 \text{ mL min}^{-1}$ .

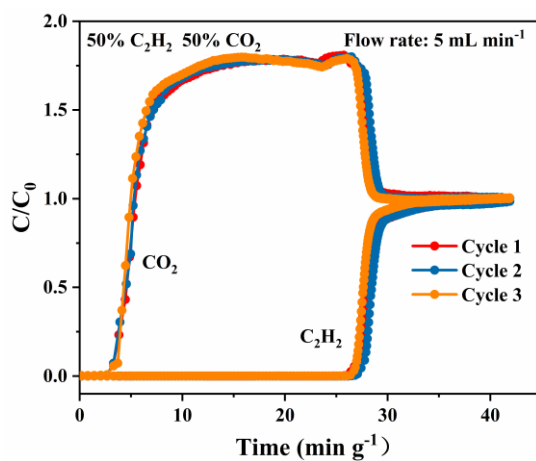


**Figure S50.** Comparison of experimental and simulated breakthrough curves for 50/50  $C_2H_2/CO_2$  mixtures in fixed bed packed with SOFOUR-TEPE-Zn operating at 298 K and 100 kPa. The flow rate at the inlet is  $10 \text{ mL min}^{-1}$ .

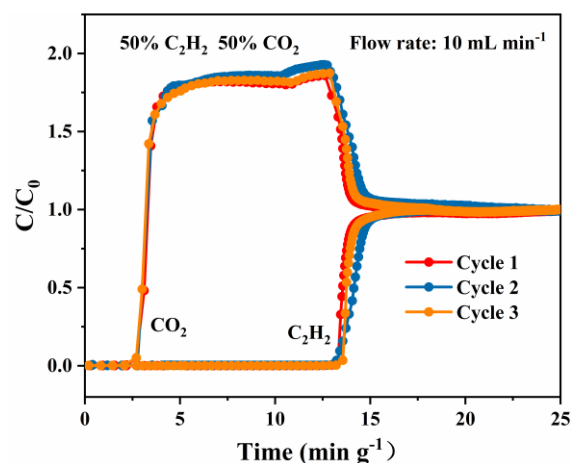
rate at the inlet is  $10.0 \text{ mL min}^{-1}$ .



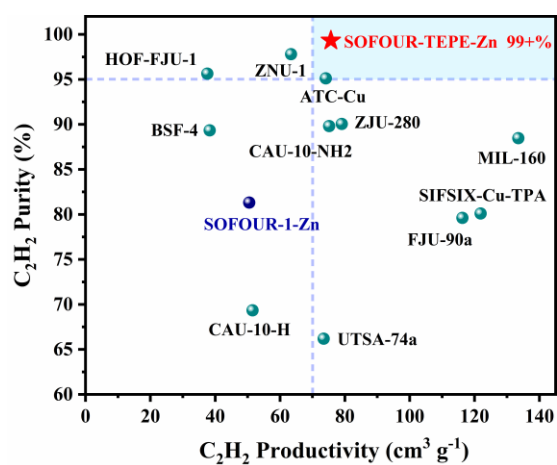
**Figure S51.** Cycling breakthrough tests for  $\text{C}_2\text{H}_2/\text{CO}_2$  (50/50,  $v/v$ ) on SOFOUR-TEPE-Zn at room temperature (flow rate:  $2.0 \text{ mL min}^{-1}$ ).



**Figure S52.** Cycling breakthrough tests for  $\text{C}_2\text{H}_2/\text{CO}_2$  (50/50,  $v/v$ ) on SOFOUR-TEPE-Zn at room temperature (flow rate:  $5.0 \text{ mL min}^{-1}$ ).



**Figure S53.** Cycling breakthrough tests for  $C_2H_2/CO_2$  (50/50, v/v) on SOFOUR-TEPE-Zn at room temperature (flow rate:  $10.0 \text{ mL min}^{-1}$ ).



**Figure S54.** Comparison of the  $C_2H_2$  productivity and purity with 100%  $C_2H_2$  recovery during counter-current blowdown process.

**Table S1.** Lattice parameters of the modeled structure of SOFOUR-TEPE-Zn and SOFOUR-1-Zn<sup>[28]</sup>.

Unit cell parameters	SOFOUR-TEPE-Zn	SOFOUR-1-Zn
Formula	C <sub>22</sub> H <sub>16</sub> N <sub>4</sub> O <sub>4</sub> SZn	C <sub>26</sub> H <sub>18</sub> N <sub>4</sub> O <sub>4</sub> SZn
Formula weight	497.858	547.87
Crystal system	Orthorhombic	Orthorhombic
Space group	<i>Cmm2</i>	<i>Cmm2</i>
a (Å)	13.15101	13.0325
b (Å)	19.41220	25.0760
c (Å)	9.63340	9.4686
$\alpha$ (°)	90.000	90.000
$\beta$ (°)	90.000	90.000
$\gamma$ (°)	90.000	90.000
V (Å <sup>3</sup> )	2459.31	3094.37
Z	4.000	4
D <sub>calcd</sub> (g cm <sup>-3</sup> )	1.34556	1.176
R <sub>p</sub> <sup>a</sup>	0.04272	/
R <sub>wp</sub> <sup>b</sup>	0.05574	/

**Table S2.** Unit cell parameters and reliability of fitting for SOFOUR-TEPE-Zn.

Parameters	Initial	Final
a	12.9776	13.15101
b	20.02782	19.41220
c	9.1038	9.6334
$\alpha$	90.000	90.000
$\beta$	90.00	90.00
$\gamma$	90.000	90.000

R<sub>p</sub> = 4.272%, R<sub>wp</sub> = 5.574%, GOF = 2.194, R<sub>f</sub> = 2.157%, R<sub>b</sub> = 1.453%



**Table S3.** List of atomic coordinates for the modeled structure of SOFOUR-TEPE-Zn.

Atom	x/a	y/b	z/c	B	Site
O1	0.39084	0.75390	0.94538	2.606	1
N2	0.25181	0.67873	0.76486	2.229	1
N3	0.26028	0.67552	0.06341	1.960	1
C4	0.18575	0.68269	0.65581	2.413	1
C5	0.18214	0.63221	0.55204	2.658	1
C6	0.25502	0.57969	0.54696	2.498	1
C7	0.33126	0.58196	0.64998	2.552	1
C8	0.32421	0.62839	0.76275	2.560	1
C9	0.26438	0.57788	0.28414	2.089	1
C10	0.18253	0.58161	0.19003	3.098	1
C11	0.18511	0.62720	0.07594	2.673	1
C12	0.33580	0.67657	0.16240	2.703	1
C13	0.34122	0.62701	0.26813	2.861	1
C14	0.26113	0.53581	0.41670	0.000	1
H15	0.13691	0.72634	0.64515	2.896	1
H16	0.12591	0.63698	0.47052	3.190	1
H17	0.40019	0.55303	0.63904	3.062	1
H18	0.38180	0.62757	0.84311	3.072	1
H19	0.11339	0.55367	0.20884	3.718	1
H20	0.12279	0.62656	0.00231	3.207	1
H21	0.39187	0.71715	0.16551	3.244	1
H22	0.40206	0.63010	0.34362	3.433	1
Zn23	0.25000	0.75000	0.91588	1.778	1
S24	0.50000	0.76379	0.84670	2.039	1
O25	0.50000	0.83698	0.78414	2.744	1
O26	0.50000	0.71317	0.72304	2.785	1

**Table S4.** Ultimate element analysis of SOFOUR-TEPE-Zn.

Elemental		N	C	H	S	O	N/S
%	Actual	10.22	48.16	3.90	6.05	15.74	1.69
(mass)	Theoretical	11.30	53.05	3.24	6.44	12.84	1.75

**Table S5.** Dual-site Langmuir parameter fits for C<sub>2</sub>H<sub>2</sub>, and the Single-site Langmuir parameter fits for CO<sub>2</sub> in SOFOUR-TEPE-Zn and SOFOUR-1-Zn.

		Site A			Site B		
		$\frac{q_{A,sat}}{\text{mol/kg}}$	$\frac{b_{A0}}{\text{Pa}^{-1}}$	$\frac{E_A}{\text{kJ mol}^{-1}}$	$\frac{q_{B,sat}}{\text{mol/kg}}$	$\frac{b_{B0}}{\text{Pa}^{-1}}$	$\frac{E_B}{\text{kJ mol}^{-1}}$
SOFOUR-TEPE-Zn	C <sub>2</sub> H <sub>2</sub>	2.95	2.454E-11	45.6	1.45	8.309E-10	25.3
	CO <sub>2</sub>	1.8	1.433E-10	26.25			
SOFOUR-1-Zn	C <sub>2</sub> H <sub>2</sub>	2.3	2.170E-03	/	1.65	8.287E-06	/
	CO <sub>2</sub>	4.4	4.580E-05				

**Table S6.** Comparison of the adsorption capacity and C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> (50/50, v/v) selectivity and heat of adsorption data of SOFOUR-TEPE-Zn with other best-performing materials at 298 K and 1.0 bar.

Sample	S <sub>BET</sub> (m <sup>2</sup> g <sup>-1</sup> )	C <sub>2</sub> H <sub>2</sub>	C <sub>2</sub> H <sub>2</sub>	CO <sub>2</sub>	S <sub>C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub></sub>	Q <sub>st</sub>	Ref.
		(cm <sup>3</sup> g <sup>-1</sup> ) 0.1 bar/0.5 bar	(cm <sup>3</sup> g <sup>-1</sup> ) 1.0 bar	(cm <sup>3</sup> g <sup>-1</sup> ) 1.0 bar	(50/50) 1.0 bar	(kJ mol <sup>-1</sup> ) C <sub>2</sub> H <sub>2</sub>	
SOFOUR-TEPE-Zn	459	72/82.69	89.04	14.06	16833	45.5	This work
ZNU-1	532	56.44/70	76.3	38.1	56.6	54.0	[19]
BSF-4	437	32.07/45.31	53.36	35.95	9.8	35.0	[19]
HOF-FJU-1	382.4	36/40.2	43.39	3.88	6675 (323 K)	46.73	[4]
MIL-160	1138	81.68/172.07	191.86	90	10.0	31.8	[20]
CAU-10-H	627	26.99/76.5	89.8	60	4.0	27.0	[21]
CAU-10-NH <sub>2</sub>	403	57.79/76.34	80.06	46.55	10.8	31.3	[22]
SIFSIX-Cu-TPA	1272	111.9/	185.51	107.22	5.3	39.1	[23]
ZJU-280	257	66.63/94.9	105.28	71.01	18.1	50.6	[24]
FJU-90a	1572	58/154.5	180	103	4.3	25.1	[25]
ATC-Cu	600	86/107.52	112.22	90.04	53.6	79.1	[26]
UTSA-74a	830	34/88.9	107.97	67.9	9.0	31.0	[27]
Zn-MOF-74	996	14.8/124	150	146	2.8	24.7	[27]
SOFOUR-1-Zn	612	52/61	69	81	6.6	57.0	[28]
SIFSIX-22-Zn	641	83.27/111.61	127	95	6.5	36.5	[28]

NCU-100	358	24.64/97.44	102.37	11	1787.0	60.5	[29]
NUS-71	582	9.63/26.45	44.11	10.29	16.0	32.7	[30]
CPL-1-NH <sub>2</sub>	103	35.39/40	41.2	4.7	119.0	50.0	[31]
Cu <sup>I</sup> @UiO-66 -(COOH) <sub>2</sub>	302	30.02/43.4	51.74	19.0	185.0	74.5	[32]
SNNU-45	1006	61.3/114.1	133.95	97	4.5	39.9	[33]
TIFSIX-2-Cu-i	685	66.97/83	91.84	96.3	10.7	46.3	[34]
FeNi-M'MOF	383	91.1/101.5	133	84	22.0	60.3	[35]
ZJU-74a	694	49/85.8	85.7	70.1	36.5	45.0	[36]
NKMOF-1-Ni	382	47.96/55.5	61	51.1	22.0	60.3	[37]
HOF-3a	165	24.04/4742.5	46.82	21	21.5	19.5	[38]
DICRO-4-Ni-i	398	23.72/36.3	43	23	13.9	37.7	[39]
JCM-1	550	39.79/63.5	76	38.1	13.7	36.9	[40]
ZJU-50a	1570	86.79/166.98	192	100	12.0	40.0	[41]
FJU-6-TAPB	1306	24.28/73	109.86	58	3.1	29.0	[42]
UTSA-300	311	-/52.6	68.99	4.1	860	57.6	[43]
MUF-17	211	62.9/82.1	112	56.2	6.0	49.5	[44]

**Table S7.** Comparison table of C<sub>2</sub>H<sub>2</sub> productivity and purity of SOFOUR-TEPE-Zn with other best-performing materials at 298 K and 1.0 bar at 100% C<sub>2</sub>H<sub>2</sub> recovery.

<b>Sample</b>	<b>C<sub>2</sub>H<sub>2</sub> Productivity (cm<sup>3</sup> g<sup>-1</sup>)</b>	<b>C<sub>2</sub>H<sub>2</sub> Purity (%)</b>	<b>C<sub>2</sub>H<sub>2</sub> Recovery (%)</b>
<b>SOFOUR-TEPE-Zn</b>	<b>75.71</b>	<b>99.33</b>	<b>100</b>
<b>SOFOUR-1-Zn</b>	<b>50.40</b>	<b>81.31</b>	<b>100</b>
<b>HOF-FJU-1</b>	<b>37.63</b>	<b>95.63</b>	<b>100</b>
<b>MIL-160</b>	<b>133.50</b>	<b>88.47</b>	<b>100</b>
<b>CAU-10-H</b>	<b>51.52</b>	<b>69.34</b>	<b>100</b>
<b>CAU-10-NH<sub>2</sub></b>	<b>75.26</b>	<b>89.82</b>	<b>100</b>
<b>SIFSIX-Cu-TPA</b>	<b>121.86</b>	<b>80.11</b>	<b>100</b>
<b>ZJU-280</b>	<b>79.07</b>	<b>90.06</b>	<b>100</b>
<b>FJU-90a</b>	<b>116.26</b>	<b>79.62</b>	<b>100</b>
<b>ATC-Cu</b>	<b>74.37</b>	<b>95.12</b>	<b>100</b>
<b>UTSA-74</b>	<b>73.47</b>	<b>66.19</b>	<b>100</b>
<b>ZNU-1</b>	<b>63.39</b>	<b>97.80</b>	<b>100</b>
<b>BSF-4</b>	<b>38.30</b>	<b>89.34</b>	<b>100</b>

**Table S8.** Comparison table of the C<sub>2</sub>H<sub>2</sub> productivity and recovery of SOFOUR-TEPE-Zn with other best-performing materials at 298 K and 1.0 bar for obtaining 99+% and 99.5+% C<sub>2</sub>H<sub>2</sub> purity. (Blue represents the highest purity that can be achieved and the corresponding productivity and recovery)

Sample	C <sub>2</sub> H <sub>2</sub> Purity of 99+%				C <sub>2</sub> H <sub>2</sub> Purity of 99.5+%			
	Start tau of collection	C <sub>2</sub> H <sub>2</sub> Purity (%)	C <sub>2</sub> H <sub>2</sub> Productivity (cm <sup>3</sup> g <sup>-1</sup> )	C <sub>2</sub> H <sub>2</sub> Recovery (%)	Start tau of collection	C <sub>2</sub> H <sub>2</sub> Purity (%)	C <sub>2</sub> H <sub>2</sub> Productivity (cm <sup>3</sup> g <sup>-1</sup> )	C <sub>2</sub> H <sub>2</sub> Recovery (%)
SOFOUR-TE PE-Zn	~0	99.34	75.71	99.99	0.65	99.51	75.49	99.82
SOFOUR-1- Zn	227.19	99.22	36.96	73.02	291.67	99.50	35.84	70.97
HOF-FJU-1	5.52	99.02	36.29	96.39	6.44	99.52	36.06	95.81
MIL-160	103.44	99.03	109.98	82.34	123.85	99.51	106.40	79.61
CAU-10-H	167.44	99.00	20.16	39.30	180.78	99.50	18.82	36.39
CAU-10-NH <sub>2</sub>	59.75	99.05	64.51	85.72	71.35	99.51	63.17	83.91
SIFSIX-Cu-T PA	431.47	95.21	64.51	52.88		/		
ZJU-280	54.26	99.05	66.98	84.78	133.09	99.43	55.55	70.28
FJU-90a	96.21	99.06	83.10	71.38	103.46	99.53	81.09	69.73
ATC-Cu	43.07	98.45	66.75	89.81		/		
UTSA-74	311.73	99.07	19.71	26.96	332.44	99.52	17.70	24.18
ZNU-1	2.98	99.00	62.72	98.75	4.23	99.51	62.27	98.22
BSF-4	20.34	99.02	33.38	87.20	24.08	99.51	32.70	85.45

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