



# Scalable Synthesis of Robust MOF for Challenging Ethylene Purification and Propylene Recovery with Record Productivity

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**Abstract:** Ethylene (C<sub>2</sub>H<sub>4</sub>) purification and propylene (C<sub>3</sub>H<sub>6</sub>) recovery are highly relevant in polymer synthesis, yet developing physisorbents for these industrial separation faces the challenges of merging easy scalability, economic feasibility, high moisture stability with great separation efficiency. Herein, we reported a robust and scalable MOF (MAC-4) for simultaneous recovery of C<sub>3</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>4</sub>. Through creating nonpolar pores decorated by accessible N/O sites, MAC-4 displays top-tier uptakes and selectivities for C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>6</sub> over C<sub>2</sub>H<sub>4</sub> at ambient conditions. Molecular modelling combined with infrared spectroscopy revealed that C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>6</sub> molecules were trapped in the framework with stronger contacts relative to C<sub>2</sub>H<sub>4</sub>. Breakthrough experiments demonstrated exceptional separation performance for binary C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> as well as ternary C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> mixtures, simultaneously affording record productivities of 27.4 and 36.2 L kg<sup>-1</sup> for high-purity C<sub>2</sub>H<sub>4</sub> (≥ 99.9 %) and C<sub>3</sub>H<sub>6</sub> (≥ 99.5 %). MAC-4 was facilely prepared at deckgram-scale under reflux condition within 3 hours, making it as a smart MOF to address challenging gas separations.

## Introduction

Global demand for propylene (C<sub>3</sub>H<sub>6</sub>) and ethylene (C<sub>2</sub>H<sub>4</sub>) which are important chemical feedstocks in downstream manufacture industry is increasing,<sup>[1,2]</sup> with a total global production of beyond 300 million tons in 2023.<sup>[3,4]</sup> C<sub>3</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>4</sub> are traditionally produced from the crude oil cracking or dehydrogenation process. Considerable attention has been recently paid to producing C<sub>3</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>4</sub> from natural gas, coal, biomass, and methanol-to-olefins (MTO) reaction.<sup>[5]</sup> In these processes, C<sub>2</sub>H<sub>4</sub> products inevitably comprise small of ethane (C<sub>2</sub>H<sub>6</sub>) impurities at 6–10 %, while the products of MTO reaction mainly contain C<sub>3</sub>H<sub>6</sub> of 20.9 wt % and C<sub>2</sub>H<sub>4</sub> of 51.1 wt %.<sup>[6,7]</sup> Therefore, the follow-up separation by cryogenic distillation cycling operated under high pressure and low temperature conditions is essential to derive polymer-grade olefins since their highly close physicochemical properties.<sup>[8–10]</sup> Replacing distillation technology by adsorption separation using porous adsorbents would bring tremendous global benefits due to high efficiency, energy saving, and environmental friendliness.<sup>[11–13]</sup>

Metal–organic frameworks (MOFs) as an emerging type of customizable adsorbents with abundant functionality and structural modularity offer a promising platform for addressing the task-specific requirements of various applications,<sup>[14–18]</sup> especially in gas separation and purification.<sup>[19–24]</sup> For C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> separation, the utilization of C<sub>2</sub>H<sub>6</sub>-selective MOFs is more desirable owing to pure C<sub>2</sub>H<sub>4</sub> products can be directly obtained through one-step separation process, avoiding additional desorption step that is indispensably for C<sub>2</sub>H<sub>4</sub>-selective MOFs and greatly reducing energy consumption.<sup>[25–28]</sup> However, C<sub>2</sub>H<sub>6</sub>-selective MOFs were not well developed, in particularly they usually suffer from “trade-off” effect with either low selectivity because of the difficulty in discriminating C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> or low adsorption capacity owing to small available voids.<sup>[29,30]</sup> This trouble makes it be a constant challenge in designing C<sub>2</sub>H<sub>6</sub>-selective MOFs.

The latest research demonstrated that the creation of open metal sites (OMSs) in MOFs is effective for C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> separation, wherein the OMSs bind the C=C π units in C<sub>3</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>4</sub> by M⋯π interactions with different strengths.<sup>[7,31]</sup> However, this strategy is not judicious for designing C<sub>2</sub>H<sub>6</sub>-selective MOFs since C<sub>2</sub>H<sub>4</sub> are more easily adsorbed by OMSs. As high contents of C<sub>2</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> in MTO products, the collection of high-purity C<sub>2</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub> through separating C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> mixtures is important for the

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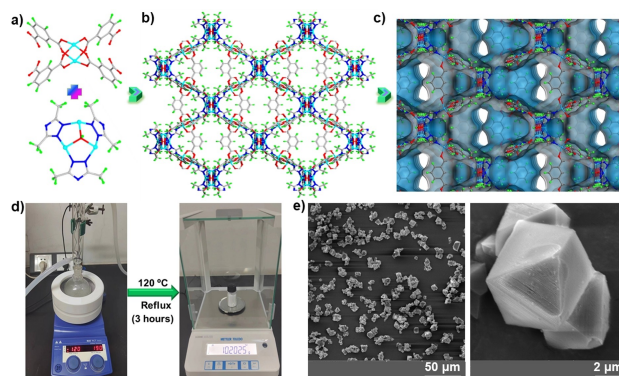
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downstream application of olefins. However, at present the simultaneous recovery of  $C_3H_6$  and  $C_2H_4$  by MOFs was only reported in one example.<sup>[32]</sup> So it is of great industrial and academic interest to develop the MOFs for separating both  $C_2H_6/C_2H_4$  and  $C_3H_6/C_2H_4$  mixtures to afford pure  $C_2H_4$  and  $C_3H_6$ , respectively. Besides, the real challenge remaining for  $C_2H_4$  purification technology through MOFs could lie in the scale-up synthesis and affordable cost of the materials upon maintaining the separation performance. Currently, most of the reported  $C_3H_6$ - or  $C_2H_6$ -selective MOFs suffer from high production cost, poor stability or synthesis scalability, severely hindering their practical utilization. To date, the efficient  $C_3H_6$ - and  $C_2H_6$ -selective MOFs that satisfied all the above requirements have not been reported. Thus, it is extremely essential to develop MOFs that merge the factor regarding to excellent separation performance, while remains a daunting challenge.

A handful of  $C_2H_6$ -selective MOFs containing nonpolar pore surfaces (e.g., aliphatic or aromatic moieties) have been recently evidenced to be certainly beneficial for preferentially adsorbing  $C_2H_6$  over  $C_2H_4$  based on the slightly higher polarizability of  $C_2H_6$  ( $44.7 \times 10^{25} \text{ cm}^{-3}$ ) over  $C_2H_4$  ( $42.52 \times 10^{25} \text{ cm}^{-3}$ ).<sup>[25,33]</sup> In addition, there were also some MOFs that mainly relied on well-designed available interacting sites (e.g. N/O atoms), leading to more hydrogen bonds with  $C_2H_6$  and  $C_3H_6$  than  $C_2H_4$ .<sup>[34,35]</sup> With the above considerations in mind, we supposed that design nonpolar pore environments with N/O active sites in MOFs could display the potential for both  $C_2H_6/C_2H_4$  and  $C_3H_6/C_2H_4$  separation. Herein, we developed a highly stable MOF, MAC-4 [ $Zn_2(\text{dmtrz})_3(\text{ipa})_3(\text{OH})$ ], fabricated by Zhou et al.<sup>[36]</sup> This material is composed of inexpensive and easily available ligands of isophthalic acid ( $H_2\text{ipa}$ ) and 3,5-dimethyl-1,2,4-triazole (Hdmtrz) ligands. In particular, it contains nonpolar pores with rich O/N sites and inorganic secondary building units (SBUs) without undesired OMSs, these two structure features would be very favourable for the target function of  $C_2H_6$ - and  $C_3H_6$  selectivity over  $C_2H_4$  in MOFs. MAC-4 displayed not only high uptakes and selectivities for  $C_2H_6$  and  $C_3H_6$  over  $C_2H_4$  but also efficient one-step purification of  $C_2H_4$  from  $C_2H_6/C_2H_4$  and  $C_3H_6/C_2H_4$  mixtures with high  $C_2H_4$  productivity of  $21.6 \text{ L kg}^{-1}$  and  $349.3 \text{ L kg}^{-1}$ , respectively. MAC-4 also provided a record high  $C_3H_6$  ( $\geq 99.5\%$ ) recovery capacity of  $70.1 \text{ L kg}^{-1}$  in single  $C_3H_6/C_2H_4$  separation process, as well as one-step acquisition of  $C_2H_4$  ( $\geq 99.9\%$ ) and  $C_3H_6$  ( $\geq 99.5\%$ ) from  $C_3H_6/C_2H_6/C_2H_4$  mixtures. GCMC calculations unveiled that multiple N/O active sites in nonpolar pores provided stronger interactions with both  $C_3H_6$  and  $C_2H_6$  over  $C_2H_4$ .

## Results and Discussion

MAC-4 with an orthorhombic  $Pnma$  space group was built on two types of cluster-based SBUs: paddle-wheel [ $Zn_2(\text{COO})_4$ ] and triangle [ $Zn_3(\text{OH})(\text{dmtrz})_3$ ]. The same SBUs are connected by  $\text{ipa}^{2-}$  linkers or Zn–N coordination bonds to produce one-dimensional chains along the  $b$  and  $a$  axes, respectively (Figure 1a and S1). The linkage between two



**Figure 1.** a) [ $Zn_2(\text{COO})_4$ ] and [ $Zn_3(\text{OH})(\text{dmtrz})_3$ ] SBUs, b) and c) 3D structure of MAC-4 (H, green; Zn, turquoise; C, gray; O, red; N, blue); d) photographs of the deckgram-scale synthesis of MAC-4; e) SEM images of MAC-4 microcrystalline with octahedral bulk.

types of SBUs through coordination interactions generates a 3D porous network. Remarkably, the framework with the void of  $\sim 45.5\%$  contains 1D zig-zag open channels (size  $\sim 5.9\text{--}8.0 \text{ \AA}$ ) that were decorated by the methyl groups of dmtrz, phenyl rings of  $\text{ipa}^{2-}$  ligands as well as rich N and O sites (Figure 1b and 1c).

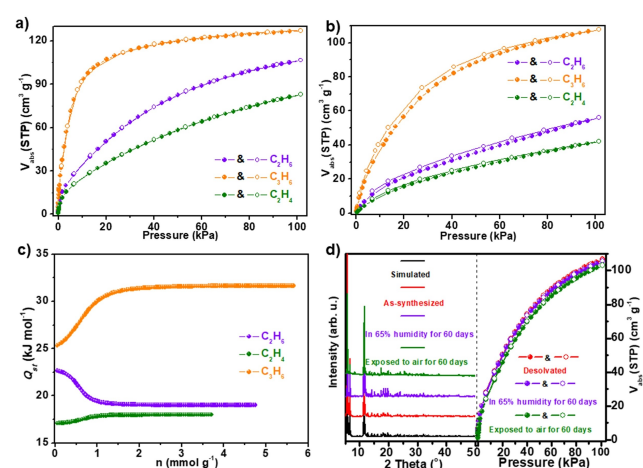
In the pursuit of convenient synthesis methods, it was important to find that MAC-4 could be rapidly and easily synthesized through refluxing the reactants in DMF within 3 hours with a high yield (78%). The phase purity and crystallinity of the MAC-4 microcrystalline were verified by scanning electron microscope (SEM) and powder X-ray diffraction (PXRD) tests (Figure 1d, 1e and S2). Thermogravimetric analysis (TGA) displayed a continuous weight loss; however, the  $\text{CH}_2\text{Cl}_2$ -exchanged samples showed a wide thermostable plateau up to  $350^\circ\text{C}$  following an initial weight loss before  $140^\circ\text{C}$  (Figure S3).

Nitrogen ( $\text{N}_2$ ) adsorption isotherms at 77 K showed type-I curves for the scaled-up and single-crystal MAC-4 samples with the saturated loadings of  $338$  and  $343 \text{ cm}^3 \text{ g}^{-1}$ , respectively, indicating the close Brunauer–Emmett–Teller (BET) surface areas of  $1180$  and  $1218 \text{ m}^2 \text{ g}^{-1}$  (Figure S4). The pore size distribution of  $6.4\text{--}10.8 \text{ \AA}$  agrees with the calculated results from crystal structure. The accessible porous wall of MAC-4 is mainly modified by phenyl rings and methyl groups in ligands, giving rise to a hydrophobic environment, as confirmed by the water vapour adsorption showing a type-V isotherm at 298 K (Figure S5). The structure of MAC-4 after both activation and water adsorption was intact, as demonstrated by PXRD (Figure S2).

The suitable pore size and nonpolar pore environment of MAC-4 inspired us to examine its  $C_2H_4$  purification performance. First, the sorption isotherms of different shape of MAC-4 samples prepared from solvothermal (crystals) and reflux (microcrystalline) reactions were measured at 273 and 298 K (Figure S6–S8). Both samples displayed very close sorption isotherms for  $C_2H_6$ ,  $C_2H_4$ , and  $C_3H_6$ , demonstrated no difference in adsorption performance between the samples. MAC-4 showed typical type-I sorption iso-

therms for  $C_2H_6$ ,  $C_2H_4$ , and  $C_3H_6$  with the uptakes of 107/124, 83/108, and 127/140  $cm^3 g^{-1}$  at 100 kPa and 298/273 K, respectively (Figure 2a and S9). The  $C_2H_6$  uptake in MAC-4 is remarkably higher than most top-performing  $C_2H_6$ -selective materials, such as MUF-15,<sup>[37]</sup> Azole-Th-1,<sup>[38]</sup> NKCOF-21,<sup>[39]</sup> TJT-100,<sup>[30]</sup>  $Fe_2(O_2)dobdc$ ,<sup>[40]</sup> MAF-49<sup>[41]</sup> and so on, and is slightly lower than benchmark MOFs CPM-233<sup>[42]</sup> and ZJU-120a<sup>[43]</sup> (Figure S10). MAC-4 also shows exceptional loadings of 56, 42, and 108  $cm^3 g^{-1}$  for  $C_2H_6$ ,  $C_2H_4$ , and  $C_3H_6$  at a high temperature of 353 K (Figure 2b). Meanwhile, the adsorption curves of MAC-4 exhibit higher uptakes and steeper slopes for  $C_3H_6$  and  $C_2H_6$  than  $C_2H_4$ , indicating selective adsorption of  $C_3H_6$  and  $C_2H_6$  over  $C_2H_4$ . These findings are in accord with the calculated values of adsorption enthalpy ( $Q_{st}$ ) at zero coverage with the order of  $C_3H_6$  (25.3  $kJ mol^{-1}$ ) >  $C_2H_6$  (22.7  $kJ mol^{-1}$ ) >  $C_2H_4$  (17.1  $kJ mol^{-1}$ ) (Figure 2c). It was noted that the  $Q_{st}$  data showed inflection points for three gases, in particular for  $C_3H_6$  and  $C_2H_6$ , from zero-coverage to 1.5, 1.0, and 1.0  $mmol g^{-1}$  loadings for  $C_3H_6$ ,  $C_2H_6$ , and  $C_2H_4$  gases, respectively, which corresponded to the amounts of gas molecules in one pore were about 1.7, 1, and 1 molecules. The inflection points for  $Q_{st}$  data could be because of the reorientation of gas molecules in pores under increased pressure. Meanwhile, due to relatively high loadings, the interactions between the  $C_3H_6$  molecules in pores could also be responsible for the obviously increased  $Q_{st}$  of  $C_3H_6$ .<sup>[37]</sup> Notably, the  $Q_{st}$  values of three gases are below 32  $kJ mol^{-1}$  owing to the nonpolar pores of MAC-4, implying a facile regeneration treatment with low energy consumption. In fact, the fully reproducible  $C_3H_6$ ,  $C_2H_6$ , and  $C_2H_4$  adsorption curves can be recycled with the simple activation treatment (353 K for 10 minutes) prior to each cycle (Figure S11–13).

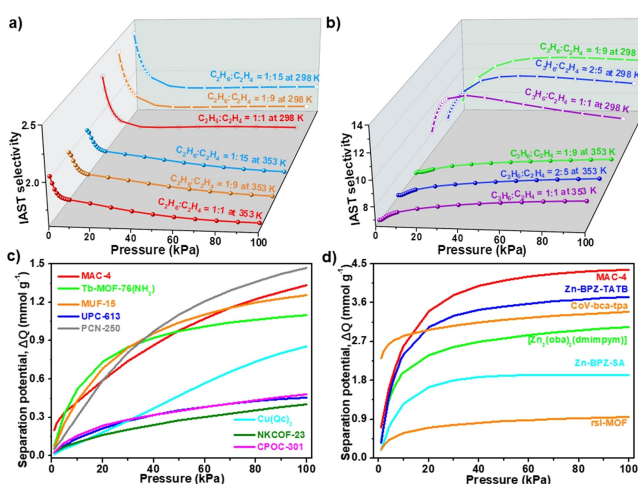
Given that the real-industrial application environment, the material must possess long-term and high humidity stability. The stability of MAC-4 toward air environments and humidity was evaluated and monitored by gas adsorptions and PXRD measurements. As divulged in Figure 2d



**Figure 2.** a) Sorption isotherms of MAC-4 at 298 K; b) sorption isotherms of MAC-4 at 353 K; c)  $Q_{st}$  curves; d) PXRD patterns (left) and  $C_2H_6$  adsorption isotherms (right) of MAC-4 samples.

(left), after exposing to 65 % humidity and air environment for 60 days, MAC-4 remains intact without crystallinity loss and phase transformation, as verified by PXRD. Moreover, the adsorption isotherms for  $C_2H_6$  at 298 K for above samples are very close to that of the initial samples, confirming and guaranteeing the great stability of MAC-4 for practical utilization (Figure 2d right).

As for higher uptakes and larger adsorption enthalpies toward  $C_3H_6$  and  $C_2H_6$  than  $C_2H_4$ , the separation selectivities of MAC-4 for  $C_2H_6/C_2H_4$  and  $C_3H_6/C_2H_4$  mixtures were evaluated by employing ideal adsorbed solution theory (Figure S14–S16). For  $C_2H_6/C_2H_4$  mixtures, MAC-4 displays high initial selectivities of 2.0/2.3/3.8, 2.0/2.4/4.1, and 2.0/2.4/4.2 for 1/1, 1/9, and 1/15 mixtures at 353/298/273 K, respectively, and which are still high of 1.7/1.9/2.2 at 100 kPa (Figure 3a, S17, and S19). These selectivities are higher than or comparable to many well-developed  $C_2H_6$ -selective adsorbents, e.g. SNUU-40,<sup>[44]</sup> CPOC-301,<sup>[45]</sup> NKCOF-22,<sup>[39]</sup> and TJT-100.<sup>[30]</sup> For  $C_3H_6/C_2H_4$  mixtures, the selectivity values were calculated to be 8.6/9.5/16.2, 8.4/10.6/19.2, and 8.1/10.9/20.6 for 1/1, 2/5, and 1/9  $C_3H_6/C_2H_4$  mixtures at 353/298/273 K, respectively (Figure 3b, S18, and S19), which are only lower than  $Zn_2(ob)_2(dmipym)$ ,<sup>[34]</sup> but significantly larger than most of materials, such as Mn-dpzip,<sup>[31]</sup> NEM-7-Cu,<sup>[46]</sup> and Zn-BPZ-SA<sup>[35]</sup> (Figure S20). At the same time, the separation potential ( $\Delta Q$ ) that was reported by Krishna and integrated the advantages of selectivity and capacity was utilized to evaluate the separation performance, which reflects the maximum  $C_2H_4$  productivity.<sup>[47,48]</sup> For equimolar  $C_2H_6/C_2H_4$  mixtures,  $\Delta Q$  were calculated to be 0.5, 1.3, and 1.9  $mmol g^{-1}$  at 353, 298, and 273 K, respectively (Figure S21), outdoing the most advanced  $C_2H_6$ -selective adsorbents, such as MUF-15,<sup>[37]</sup> NKCOF-23,<sup>[39]</sup> CPOC-301,<sup>[45]</sup> and Tb-MOF-76( $NH_2$ ),<sup>[49]</sup> under the same conditions (Figure 3c). The corresponding  $\Delta Q$  values for equimolar  $C_3H_6/C_2H_4$  mixtures are 3.2, 4.4, and 5.3  $mmol g^{-1}$  at 353, 298, and 273 K, respectively (Figure S22), superior to some well-



**Figure 3.** a) and b) IAST selectivities of MAC-4 for  $C_2H_6/C_2H_4$  and  $C_3H_6/C_2H_4$  mixtures; comparisons of separation potential for  $C_2H_6/C_2H_4$  (c) and  $C_3H_6/C_2H_4$  (d) mixtures in MAC-4 and other adsorbents at 298 K.

developed MOFs, e.g.  $[\text{Zn}_2(\text{oba})_2(\text{dmimpym})]$ ,<sup>[34]</sup> Zn-BPZ-SA,<sup>[35]</sup> CoV-bca-tca,<sup>[50]</sup> and Zn-BPZ-TATB<sup>[32]</sup> (Figure 3d).

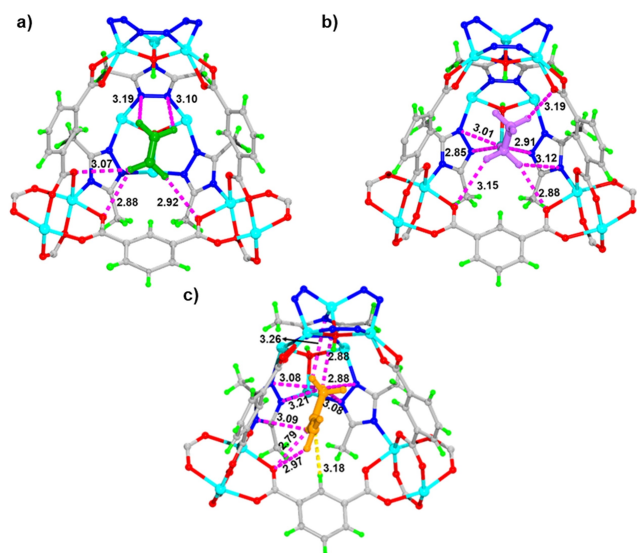
To gain precise insight into the preferential adsorption sites of  $\text{C}_3\text{H}_6$ ,  $\text{C}_2\text{H}_4$ , and  $\text{C}_2\text{H}_6$  in MAC-4, molecular modelling was performed based on Grand Canonical Monte Carlo (GCMC) simulations. All three gas molecules were preferentially located at the cavities formed around two  $[\text{Zn}_2(\text{COO})_4]$  SBUs and two triazolate-trinuclear  $[\text{Zn}_3(\text{OH})(\text{dmtrz})_3]$  SBUs. One  $\text{C}_2\text{H}_4$  interacts with three carboxylate O atoms and two triazolate N atoms through quintuple  $\text{C}\cdots\text{H}\cdots\text{O}/\text{N}$  hydrogen bonds ( $\text{H}\cdots\text{O}/\text{N}=2.88\text{--}3.19\text{ \AA}$ ) (Figure 4a). In comparison, the interactions between the framework and  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_6$  molecules are more and stronger, in which  $\text{C}_2\text{H}_6$  is bound to four N atoms from  $[\text{Zn}_3(\text{OH})(\text{dmtrz})_3]$  SBUs and three O atoms through seven  $\text{C}\cdots\text{H}\cdots\text{O}/\text{N}$  hydrogen bonds ( $\text{H}\cdots\text{O}=2.85\text{--}3.19\text{ \AA}$ ) (Figure 4b). For  $\text{C}_3\text{H}_6$ , it not only is involved in nine  $\text{C}\cdots\text{H}\cdots\text{O}/\text{N}$  hydrogen bonds ( $\text{H}\cdots\text{O}=2.79\text{--}3.26\text{ \AA}$ ), but also forms one  $\text{C}\cdots\text{H}\cdots\pi$  interaction via the alkenyl  $\pi$  clouds of  $\text{C}_3\text{H}_6$  (Figure 4c). Therefore, the MOF possesses a greater affinity for  $\text{C}_2\text{H}_6$  and  $\text{C}_3\text{H}_6$  relative to  $\text{C}_2\text{H}_4$ . Meanwhile, the calculated binding energies also showed larger values for  $\text{C}_3\text{H}_6$  ( $37.3\text{ kJ mol}^{-1}$ ) and  $\text{C}_2\text{H}_6$  ( $35.7\text{ kJ mol}^{-1}$ ) compared to  $\text{C}_2\text{H}_4$  ( $31.5\text{ kJ mol}^{-1}$ ).

The interactions of  $\text{C}_2\text{H}_4$ ,  $\text{C}_3\text{H}_6$ , and  $\text{C}_2\text{H}_6$  with MAC-4 were deliberated at 100 kPa and 298 K by further simulations. As divulged in Figure S23–S26, two  $\text{C}_2\text{H}_4$ , three  $\text{C}_2\text{H}_6$ , and four  $\text{C}_3\text{H}_6$  molecules mainly interacted with the pore walls. Two  $\text{C}_2\text{H}_4$  via the  $-\text{CH}$  units form multiple  $\text{C}\cdots\text{H}\cdots\text{O}/\text{N}$  contacts with triazolate N atoms and carboxylate O atoms (Figure S23). Three  $\text{C}_2\text{H}_6$  molecules are located in different coordination fragments interacting with N/O atoms through  $\text{C}\cdots\text{H}\cdots\text{O}/\text{N}$  hydrogen bonds ( $\text{H}\cdots\text{O}/\text{N}=2.65\text{--}3.29\text{ \AA}$ ) (Figure S24).  $\text{C}_3\text{H}_6$  molecules are involved in more contacts not only with the accessible N/O atoms but also with the  $\pi$  centers and methyl groups from linkers. Specifically,  $\text{C}_3\text{H}_6$ -I

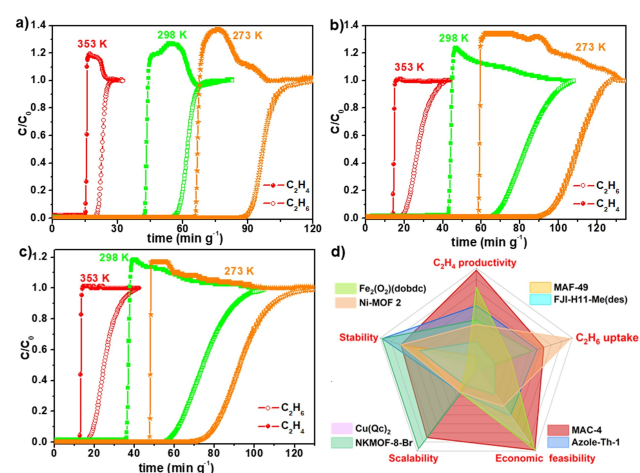
and  $\text{C}_3\text{H}_6$ -II exist in similar locations around two  $[\text{Zn}_2(\text{COO})_4]$  SBUs through  $\text{C}\cdots\text{H}\cdots\text{O}/\pi$  contacts ( $\text{H}\cdots\text{O}=2.69\text{--}3.17\text{ \AA}$ ,  $\text{H}\cdots\pi=2.86\text{--}3.32\text{ \AA}$ ) with carboxylate O atoms and phenyl  $\pi$  centers as well as  $\text{C}\cdots\text{H}\cdots\pi$  interactions between two  $\text{C}_3\text{H}_6$  molecules (Figure S25).  $\text{C}_3\text{H}_6$ -III and  $\text{C}_3\text{H}_6$ -IV are resided in the region of  $[\text{Zn}_3(\text{OH})(\text{dmtrz})_3]$  fragments through forming multiple  $\text{C}\cdots\text{H}\cdots\text{C}/\text{O}/\text{N}$  hydrogen bonds and  $\text{C}\cdots\text{H}\cdots\pi$  interactions with the ligands (Figure S26). Meanwhile, these multiple contacts for  $\text{C}_3\text{H}_6$  and  $\text{C}_2\text{H}_6$  molecules can also be confirmed by the higher values of interaction energy ( $E$ ) distributions for  $\text{C}_3\text{H}_6$  ( $\bar{E}=56.9\text{ kJ mol}^{-1}$ ) and  $\text{C}_2\text{H}_6$  ( $\bar{E}=41.8\text{ kJ mol}^{-1}$ ) compared to  $\text{C}_2\text{H}_4$  ( $\bar{E}=34.7\text{ kJ mol}^{-1}$ ) (Figure S27). The simulation results are in accordance with the experimental findings and well explain the high selectivities for both  $\text{C}_3\text{H}_6$  and  $\text{C}_2\text{H}_6$  over  $\text{C}_2\text{H}_4$ .

Breakthrough experiments were performed at 273, 298, and 353 K for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (v/v, 5/5, 1/9, and 1/15) mixtures under Ar as the carrier gas (vol %, 90 %, 90 % and 84 %, a total flow of  $7\text{ mL min}^{-1}$ ), in which the mixtures were passed through the packed column. As shown in Figure 5a–5c, three mixtures can be completely separated by MAC-4, in which  $\text{C}_2\text{H}_4$  was first outflowed from the column to directly get pure  $\text{C}_2\text{H}_4$  ( $\geq 99.9\%$ ), while  $\text{C}_2\text{H}_6$  was adsorbed in the bed for a certain period of times. During this process, 1 kg MAC-4 can retrieve high-purity  $\text{C}_2\text{H}_4$  ( $\geq 99.9\%$ ) about 5.4, 14.9, and 21.6 L from 5/5, 1/9, and 1/15  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  mixtures at 298 K, respectively. The breakthrough experiments for the higher concentrations of  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  mixtures (10/10, 20/20, 30/30, v/v) were also tested at 273 and 298 K (Figure S28–S30), and it also displayed the complete separation of the mixtures. Moreover, the cycling experiments showed no loss of separation ability in MAC-4, illustrating outstanding reusability (Figure S31).

The difficult scalability and high cost of MOF adsorbents has long been a troubled issue for their application. In general, the cost of MOFs primarily depends on ligands. Although some MOFs display benchmark performance for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  separation, they suffer from long-time (48–72 h)



**Figure 4.** Preferential adsorption sites for a)  $\text{C}_2\text{H}_4$ , b)  $\text{C}_2\text{H}_6$ , and c)  $\text{C}_3\text{H}_6$  (H, green; Zn, turquoise; C, gray; O, red; N, blue).



**Figure 5.** a–c) Breakthrough curves for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  mixtures at 273, 298, and 353 K: a) 1/1, b) 1/9, c) 1/15; d) comprehensive comparisons for MAC-4 and other porous materials.

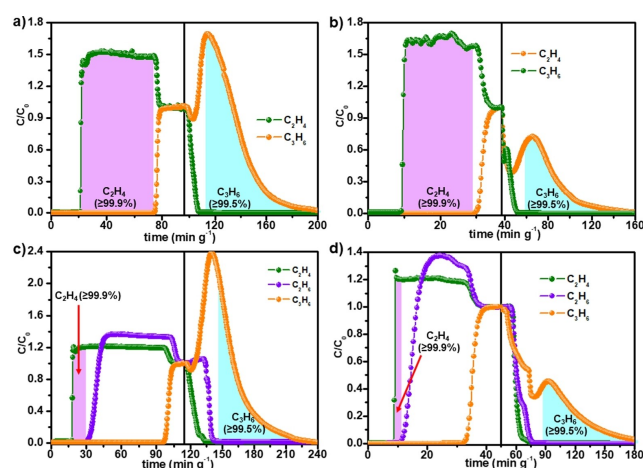
heating synthesis conditions and the use of expensive ligands, such as 2-bromoimidazole-4,5-dicarbonitrile of NKMOF-8-Br ( $142 \text{ \$ g}^{-1}$ ), 2,3,5,6-tetramethylterephthalic acid of Ni(TMBDC)(DABCO) $_{0.5}$  ( $309 \text{ \$ g}^{-1}$ ), 4-(1H-tetrazol-5-yl) benzoic acid of Azole-Th-1 ( $62 \text{ \$ g}^{-1}$ ), and 4,4',4'',4'''-(ethene-1,1,2,2-tetra-yl) tetrabenzoic acid of NUM-7a ( $309 \text{ \$ g}^{-1}$ ).<sup>[28]</sup> In contrast, MAC-4 could be facilely deck-gram-scalably prepared through stirring within 3 hours from commercially available cheap reagents with a cost of about  $1 \text{ \$ g}^{-1}$  (Table S2). Taken together, MAC-4 not only displays promising  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  separation performance, but also satisfies several crucial criteria for an industrial adsorbent including high stability, scalability, and economic feasibility, rendering it to be one of benchmark material to address challenges on  $\text{C}_2\text{H}_4$  purification in industrial application (Figure 5d).

The breakthrough experiments for various ratios of  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  (v/v: 20/20, 10/25, and 4/36) mixtures with Ar as carrier gas (vol %: 60%, 65%, and 60%) were also conducted to appraise the separation for MTO products. As presented in Figure 6a, 6b, S32, S33 and S34, highly efficient separation for the mixtures can be achieved by MAC-4, whereby  $\text{C}_2\text{H}_4$  eluted through the column to directly yield an outflow of pure  $\text{C}_2\text{H}_4$  ( $\geq 99.9\%$ ), but  $\text{C}_3\text{H}_6$  was adsorbed for a long time. About 125.1, 210.6, and 349.3 L of pure  $\text{C}_2\text{H}_4$  ( $\geq 99.9\%$ ) could be trapped from 20/20, 10/25, and 4/36  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  mixtures, respectively, for 1 kg MAC-4 at 298 K in one cycle, surpassing all-known  $\text{C}_3\text{H}_6$ -selective adsorbents, such as iso-MOF-4,<sup>[7]</sup>  $[\text{Zn}_2(\text{oba})_2(\text{dmimpym})]$ ,<sup>[34]</sup>  $\text{Fe}_2\text{Mn-L}$ ,<sup>[51]</sup> and  $\text{Zn-BPZ-SA}$ .<sup>[35]</sup> As  $\text{C}_3\text{H}_6$  is another target gas that needs to be purified from MTO products, the desorption experiments were then performed to determine  $\text{C}_3\text{H}_6$  purity and productivity. Upon reaching equilibrium concentration, the adsorption-saturated MAC-4 was purged by Ar gas ( $7 \text{ mL min}^{-1}$ ) at 323 K. As shown in Figure 6a and 6b, the

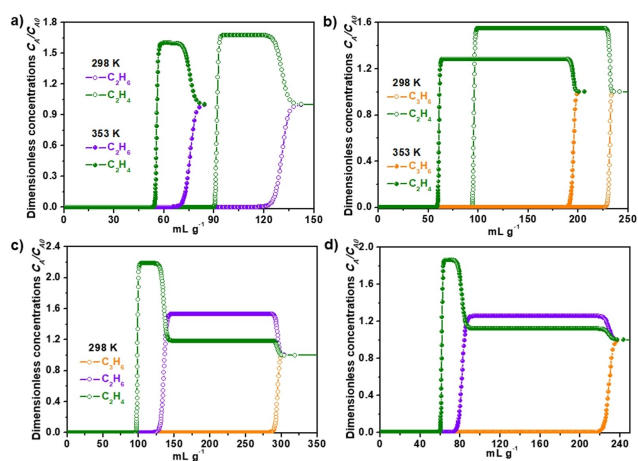
samples can be easily regenerated, in which the adsorbed  $\text{C}_2\text{H}_4$  was desorbed more quickly than  $\text{C}_3\text{H}_6$  owing to weaker binding affinity of MAC-4 for  $\text{C}_2\text{H}_4$ . It was estimated that 36.8 and  $70.1 \text{ L kg}^{-1}$  of  $\text{C}_3\text{H}_6$  ( $\geq 99.5\%$ ) could be produced from  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  (v/v, 20/20) mixtures at 353 and 298 K, respectively. To our best knowledge, these productivities of  $\text{C}_2\text{H}_4$  and  $\text{C}_3\text{H}_6$  obtained through MAC-4 separation are highest in reported materials.

Although MAC-4 achieved efficient  $\text{C}_2\text{H}_4$  purification and  $\text{C}_3\text{H}_6$  recovery from binary  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  mixtures, there are tremendous current impediments and challenges in the recovery of high-valuable  $\text{C}_3\text{H}_6$  from MTO products due to that typically contains few other light hydrocarbons. Thus, the separation experiments for ternary  $\text{C}_2\text{H}_6/\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  (v/v/v, 2/10/25 and 5/5/5) mixtures at 353 and 298 K were tested. For the 2/10/25  $\text{C}_2\text{H}_6/\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  mixtures at 298 K, it showed that at the column outlet highly pure  $\text{C}_2\text{H}_4$  ( $\geq 99.9\%$ ) flowed out firstly, with a  $27.4 \text{ L kg}^{-1}$  productivity, following by  $\text{C}_2\text{H}_6$  after  $29.5 \text{ min g}^{-1}$ , while  $\text{C}_3\text{H}_6$  was retained in the column as long as  $95.8 \text{ min g}^{-1}$ . After adsorption saturation, the desorption steps were carried out by purging with Ar gas ( $7 \text{ mL min}^{-1}$ ) at 323 K to evaluate the feasibility of  $\text{C}_3\text{H}_6$  recovery. As depicted in Figure 6c,  $\text{C}_2\text{H}_4$  and  $\text{C}_2\text{H}_6$  were rapidly desorbed from MAC-4 within  $30 \text{ min g}^{-1}$ , then the high-purity  $\text{C}_3\text{H}_6$  ( $\geq 99.5\%$ ) with a  $36.2 \text{ L kg}^{-1}$  productivity was recovered. Therefore, the pure  $\text{C}_3\text{H}_6$  and  $\text{C}_2\text{H}_4$  with record-high productivities can be respectively obtained from  $\text{C}_2\text{H}_6/\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  mixtures in one single adsorption/desorption operation. Furthermore, when the ratios of mixtures were adjusted to 5/5/5 or the temperature was rose to 353 K, MAC-4 still exhibited prominent separation ability (Figure 6d, S35, and S36). These results evidently demonstrated that MAC-4 might deliver pure both  $\text{C}_2\text{H}_4$  and  $\text{C}_3\text{H}_6$  from imitative MTO products. Furthermore, multiple breakthrough tests demonstrated no decrease of separation performance at least five continuous cycles (Figure S37), confirming good regeneration of MAC-4. Overall, MAC-4 combines the advances of benchmark  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  and  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  separation performance, ultrahigh moisture stability as well as scale-up synthesis, making it an outstanding adsorbent for  $\text{C}_2\text{H}_4$  purification and  $\text{C}_3\text{H}_6$  recovery application.

Next, transient breakthrough simulations were carried out for the exact same set of operating conditions as in the above mentioned experiments, using the methodology described in earlier publications.<sup>[52–55]</sup> In these simulations, intra-crystalline diffusion influences are ignored. There is good match between the experiments and simulations in every case (Figure S38–S45). Having established the accuracy of the transient breakthrough simulations, transient breakthrough simulations for the  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (50/50, v/v),  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  (50/50, v/v), and  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (33.33/33.33/33.33, v/v/v) mixtures without inert gas were performed at 298 and 353 K and 100 kPa to evaluate the practical applications for  $\text{C}_2\text{H}_4$  purification of MAC-4. The results in Figure 7 clearly demonstrate that MAC-4 is capable of separating three mixtures, whereby  $\text{C}_2\text{H}_4$  elutes first in all cases and subsequently reached a plateau to produce polymer-grade  $\text{C}_2\text{H}_4$  before  $\text{C}_2\text{H}_6$  and  $\text{C}_3\text{H}_6$  breakthrough



**Figure 6.** a) Breakthrough curves for  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  (v/v, 20/20) mixtures at 298 K; b) breakthrough curves for  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  (v/v, 20/20) mixtures at 353 K; c) breakthrough curves for the  $\text{C}_2\text{H}_6/\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  mixture (v/v/v, 2/10/25) mixtures at 298 K; d) breakthrough curves for the  $\text{C}_2\text{H}_6/\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  mixture (v/v/v, 2/10/25) mixtures at 353 K, after adsorption-saturated, the desorption curves obtained under Ar ( $7 \text{ mL min}^{-1}$ ) sweeping at 323 K.



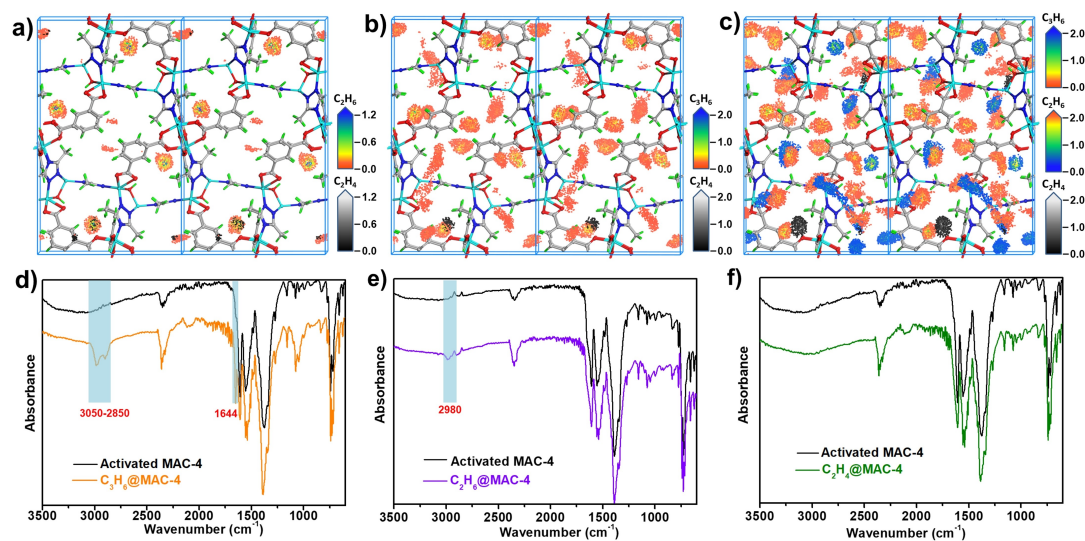
**Figure 7.** a) Simulated breakthrough curves of MAC-4 for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (50/50) at 298 and 353 K; b)  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  (50/50) at 298 and 353 K; c)  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (33.33/33.33/33.33) at 298 K; d)  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (33.33/33.33/33.33) at 353 K, the x-axis is not  $\text{min g}^{-1}$  but  $\text{mL g}^{-1}$ .

occurred. Based on the simulated breakthrough curves, MAC-4 can directly produce 8.2, 64.5, and 5.9  $\text{L kg}^{-1}$   $\text{C}_2\text{H}_4$  (purity > 99.9%) from  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$ ,  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$ , and  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  at 353 K, respectively. The corresponding  $\text{C}_2\text{H}_4$  productivity values at 298 K are 23.6, 94.3, and 18.9  $\text{L kg}^{-1}$ , respectively. The  $\text{C}_2\text{H}_4$  productivity for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (50/50, v/v) are obviously higher than most  $\text{C}_2\text{H}_6$ -selective adsorbents, such as  $\text{Fe}_2(\text{O}_2)\text{dobdc}^{[40]}$  and JNU-2,<sup>[56]</sup> Ni-MOF 2,<sup>[25]</sup> HOF-76a,<sup>[57]</sup> MAF-49,<sup>[41]</sup> NKMOF-14-PD,<sup>[58]</sup> and HOF-NBDA-(DMA)<sup>[59]</sup> (Figure S46).

In addition, the separation performance of MAC-4 was explored at a crucial low pressure by the simulated density distributions of equimolar binary  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  and  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  mixtures as well as ternary  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  mixtures. As predicted in Figure 8a and 8b, for the inlet of binary  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  or  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_4$  mixtures under 20 kPa, the density

distributions of mixture gases are concentrated at the corners of  $\text{ipa}^{2-}$  ligands and methyl group near the coordinated units in the framework. Although single-component adsorption site simulation results show that the coordinated units interact with  $\text{C}_2\text{H}_4$ , but for the mixtures the adsorption sites are more occupied by  $\text{C}_3\text{H}_6$  or  $\text{C}_2\text{H}_6$  molecules compared to  $\text{C}_2\text{H}_4$ . These findings coincided with the preferentially competitive adsorption for  $\text{C}_3\text{H}_6$  and  $\text{C}_2\text{H}_6$  molecules in the framework. Meanwhile, for  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  mixtures at 15 kPa, the density distributions of three gas molecules also deferred to the order of  $\text{C}_3\text{H}_6 > \text{C}_2\text{H}_6 \gg \text{C}_2\text{H}_4$  (Figure 8c), revealing the preferential adsorption and significant selectivity for  $\text{C}_3\text{H}_6$  and  $\text{C}_2\text{H}_6$  over  $\text{C}_2\text{H}_4$ , which further verified the excellent separation performance of MAC-4.

To further probe the gas binding sites, infrared (IR) spectroscopies of MAC-4 with the loading of  $\text{C}_3\text{H}_6$ ,  $\text{C}_2\text{H}_6$ , and  $\text{C}_2\text{H}_4$  were measured. Figure 8d shows an apparent and new stretching bands at 3050–2850 and 1646  $\text{cm}^{-1}$  that belong to  $\text{C}_3\text{H}_6$  in  $\text{C}_3\text{H}_6$ -loaded MAC-4.<sup>[60]</sup> Besides, tiny changes at 1558 and 1537  $\text{cm}^{-1}$  were observed, suggesting that  $\text{C}_3\text{H}_6$  molecule formed the interactions with triazole rings (Figure S47).<sup>[61]</sup> Similarly, when  $\text{C}_2\text{H}_6$  was loaded into MAC-4, characteristic peaks (2980  $\text{cm}^{-1}$ ) assigned to fundamental  $\nu(\text{CH}_3)$  stretches of  $\text{C}_2\text{H}_6$  molecule appeared (Figure 8e).<sup>[26,58]</sup> Meanwhile, the tiny changes at 1553 and 1538  $\text{cm}^{-1}$  were also observed, indicating that  $\text{C}_2\text{H}_6$  had multiple interactions with triazole rings (Figure S48). In contrast, no distinct peak change for  $\text{C}_2\text{H}_4$ -loaded MAC-4 was observed, which could be attributed to the weak interactions between  $\text{C}_2\text{H}_4$  and the framework (Figure 8f). These IR spectroscopies qualitatively and partly supported the simulated results.



**Figure 8.** Simulated density distributions in MAC-4 for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (a),  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (b), and  $\text{C}_3\text{H}_6/\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (c) mixtures; d-f) IR spectra of activated MAC-4,  $\text{C}_3\text{H}_6@MAC-4$ ,  $\text{C}_2\text{H}_6@MAC-4$  and  $\text{C}_2\text{H}_4@MAC-4$ .

## Conclusions

In conclusion, we developed a deckgram-scale synthetic route of cheap and robust MOF MAC-4 with the goal of C<sub>2</sub>H<sub>4</sub> purification from C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>6</sub> mixtures. The non-polar pore surfaces with accessible O/N active sites endow the MOF with preferential adsorption for C<sub>3</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>6</sub> over C<sub>2</sub>H<sub>4</sub>, leading to simultaneously high C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>6</sub> uptakes and significant C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> selectivity. MAC-4 not only directly produces high-purity C<sub>2</sub>H<sub>4</sub> ( $\geq 99.9\%$ ) from C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> mixtures, but also provides a high C<sub>3</sub>H<sub>6</sub> ( $\geq 99.5\%$ ) recovery capacity through one adsorption-desorption procedure, which are highest in known materials. In addition, MAC-4 also realized one-step acquisition of C<sub>2</sub>H<sub>4</sub> (99.9%) and C<sub>3</sub>H<sub>6</sub> (99.5%) with the record productivities of 27.4 and 36.2 L kg<sup>-1</sup> from C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> ternary mixtures. The comprehensive advantages on moisture stability, scalability, economic feasibility, separation performance, and reusability laid a solid foundation for MAC-4 to be applied in C<sub>2</sub>H<sub>4</sub> purification and C<sub>3</sub>H<sub>6</sub> recovery from the corresponding mixtures. This presentation would march an important step toward challenging C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> separation in applications and would facilitate the development of MOF-based adsorbents for new separation target as well.

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## Conflict of Interest

The authors declare no conflict of interest.

## Data Availability Statement

The data that support the findings of this study are available in the supplementary material of this article.

**Keywords:** metal–organic framework · scalable synthesis · gas adsorption and separation · ethylene purification · propylene recovery

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## Supporting Information

### **Scalable Synthesis of Robust MOF for Challenging Ethylene Purification and Propylene Recovery with Record Productivity**

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Supporting Information  
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## Scalable Synthesis of Robust MOF for Challenging Ethylene Purification and Propylene Recovery with Record Productivity

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**Abstract:** Ethylene (C<sub>2</sub>H<sub>4</sub>) purification and propylene (C<sub>3</sub>H<sub>6</sub>) recovery are highly relevant in polymer synthesis, yet developing physisorbents for these industrial separation faces the challenges of merging easy scalability, economic feasibility, high moisture stability with great separation efficiency. Herein, we reported a robust and scalable MOF (MAC-4) for simultaneous recovery of C<sub>3</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>4</sub>. Through creating nonpolar pores decorated by accessible N/O sites, MAC-4 displays top-tier uptakes and selectivities for C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>6</sub> over C<sub>2</sub>H<sub>4</sub> at ambient conditions. Molecular modelling combined with infrared spectroscopy revealed that C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>6</sub> molecules were trapped in the framework with stronger contacts relative to C<sub>2</sub>H<sub>4</sub>. Breakthrough experiments demonstrated exceptional separation performance for binary C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> and C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> as well as ternary C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> mixtures, simultaneously affording record productivities of 27.4 and 36.2 L kg<sup>-1</sup> for high-purity C<sub>2</sub>H<sub>4</sub> (≥ 99.9 %) and C<sub>3</sub>H<sub>6</sub> (≥ 99.5 %). MAC-4 was facilely prepared at decigram-scale under reflux condition within 3 hours, making it as a smart MOF to address challenging gas separations.

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## Materials and general methods

The reagents were purchased commercially. Thermalgravimetric analyses (TGA) were tested in a nitrogen stream using a Netzsch TG209F3 equipment ( $10\text{ }^{\circ}\text{C min}^{-1}$ ). Powder X-ray diffraction (PXRD) data were recorded on a Bruker D8 ADVANCE X-ray powder diffractometer ( $\text{Cu K}\alpha$ ,  $\lambda = 1.5418\text{ \AA}$ ). Water sorption was collected by Quantachrome Vstar vapor adsorption equipment. Sorption measurements were performed with an automatic volumetric sorption apparatus (Micrometrics TriStar II 3020), in which the sample was activated at 393 K under vacuum for 4 hours. Breakthrough experiments were performed on a Quantachrome dynaSorb BT equipment. All the IR spectroscopic data are recorded in INVENIO S ATR-FTIR spectrometer.

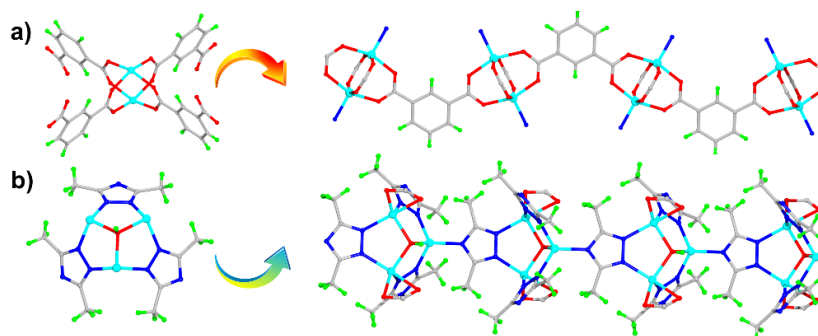
## Synthesis of MAC-4

### Solvothermal synthesis of MAC-4 crystals

MAC-4 crystal was synthesized according to a previously published report.<sup>[1]</sup> The solution of 0.3 mmol 3,5-dimethyl-1,2,4-triazolate (Hdmtrz) (0.028 g) and 0.3 mmol isophthalic acid ( $\text{H}_2\text{ipa}$ ) (0.049 g) in 5 mL of N, N-dimethylformamide (DMF) was added to the solution 5 mL DMF containing 0.45 mmol  $\text{Zn}(\text{OAc})_2 \cdot 2\text{H}_2\text{O}$  (0.089 g). The next solvothermal reactions heated at  $140\text{ }^{\circ}\text{C}$  for 3 days yielded MAC-4 crystals.

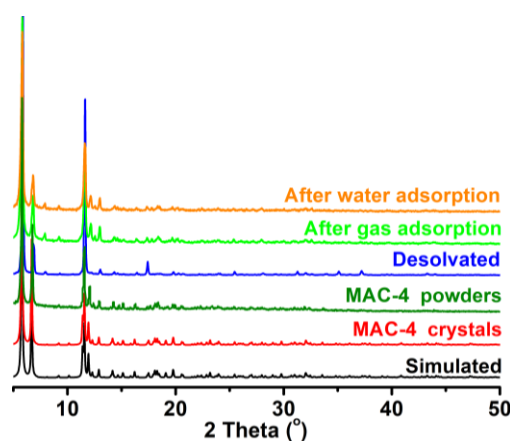
### Scale-up synthesis of MAC-4 microcrystalline

The decagram-scale synthesis of MAC-4 was performed under reflux conditions. 54 mmol  $\text{Zn}(\text{OAc})_2 \cdot 2\text{H}_2\text{O}$  (10.68 g), 36 mmol Hdmtrz (3.36 g), 36 mmol  $\text{H}_2\text{ipa}$  (5.88 g) were stirred in DMF (300 mL) until it was fully dissolved (Figure 1a). Then the solutions were refluxed at  $120\text{ }^{\circ}\text{C}$  for 3 hours. The white microcrystalline of MAC-4 was collected through filtration, and then dried in air environment (Yield: 10.2 g, 77.7% based on  $\text{Zn}^{2+}$  ions) (Figure 1b). Note, the DMF can be recovered by filtrating for continued synthesis of MAC-4 at least three cycles.



**Figure S1.** a) 1D chains composed of  $[\text{Zn}_2(\text{COO})_4]$  SBUs; b) 1D chains composed of  $[\text{Zn}_3(\text{OH})(\text{dmtrz})_3]$  SBUs.

## Powder X-ray diffraction (PXRD)



**Figure S2.** PXRD patterns of MAC-4.

## Thermogravimetric analysis (TGA)

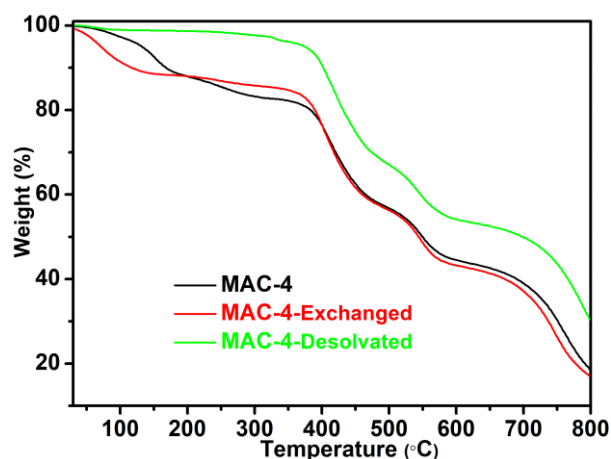


Figure S3. TGA curves of as-synthesized, exchanged, and desolvated samples of MAC-4.

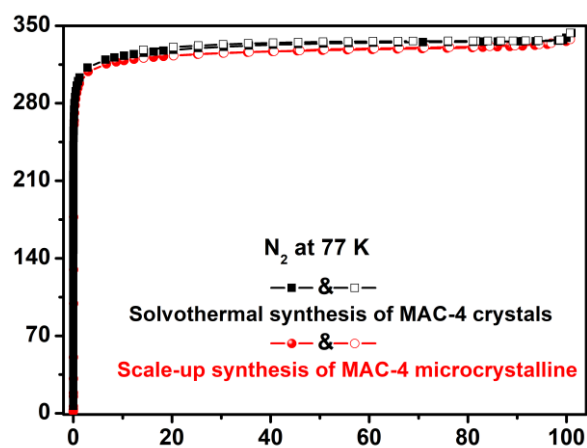
N<sub>2</sub> adsorption isotherms

Figure S4. Comparison of N<sub>2</sub> adsorption isotherms (77 K) of MAC-4 synthesized by different methods.

## Water adsorption isotherms

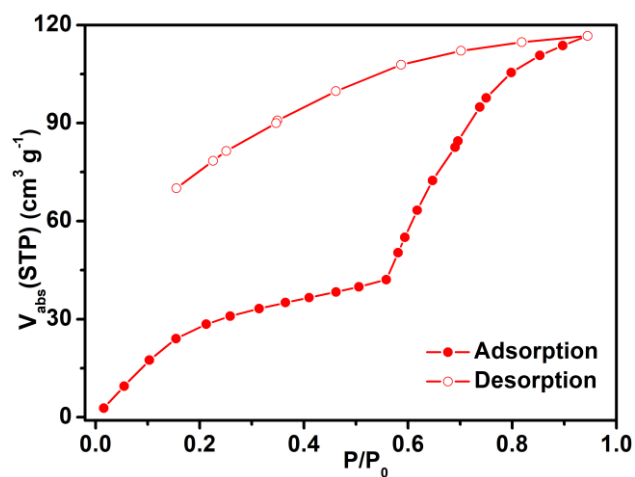


Figure S5. Water vapor adsorption and desorption isotherm of MAC-4 at 298 K.

## Gas adsorption isotherms

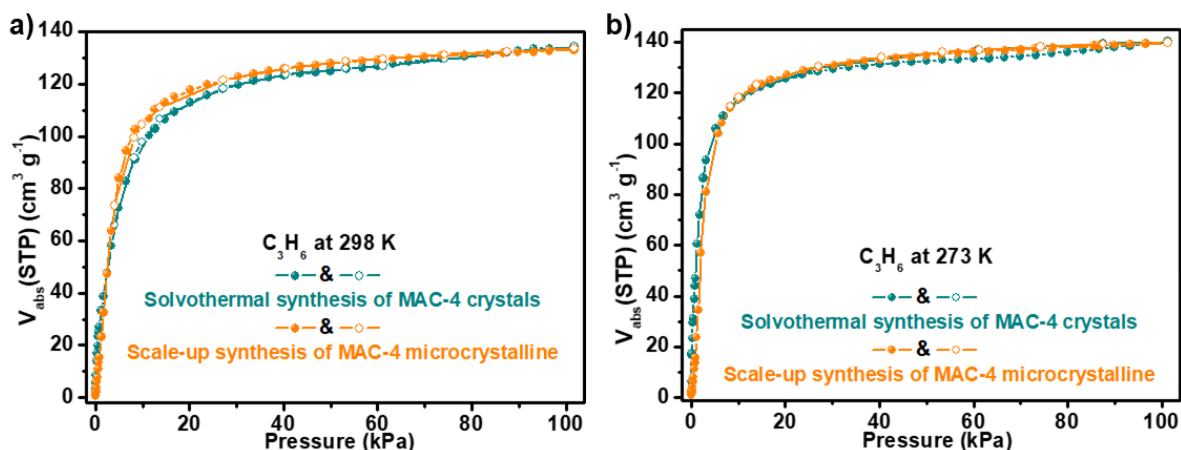


Figure S6. The comparison of adsorption isotherm curves of solvothetical synthesis of MAC-4 crystals samples and scale-up synthesis of MAC-4 microcrystalline samples for  $C_3H_6$  at 298 K a); and 273 K b).

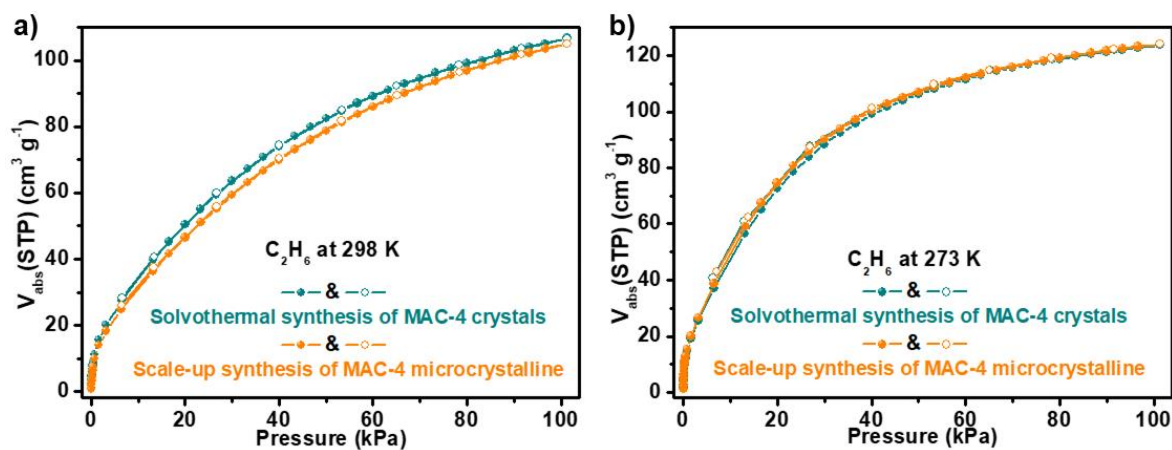


Figure S7. The comparison of adsorption isotherm curves of solvothetical synthesis of MAC-4 crystals samples and scale-up synthesis of MAC-4 microcrystalline samples for  $C_2H_6$  at 298 K a); and 273 K b).

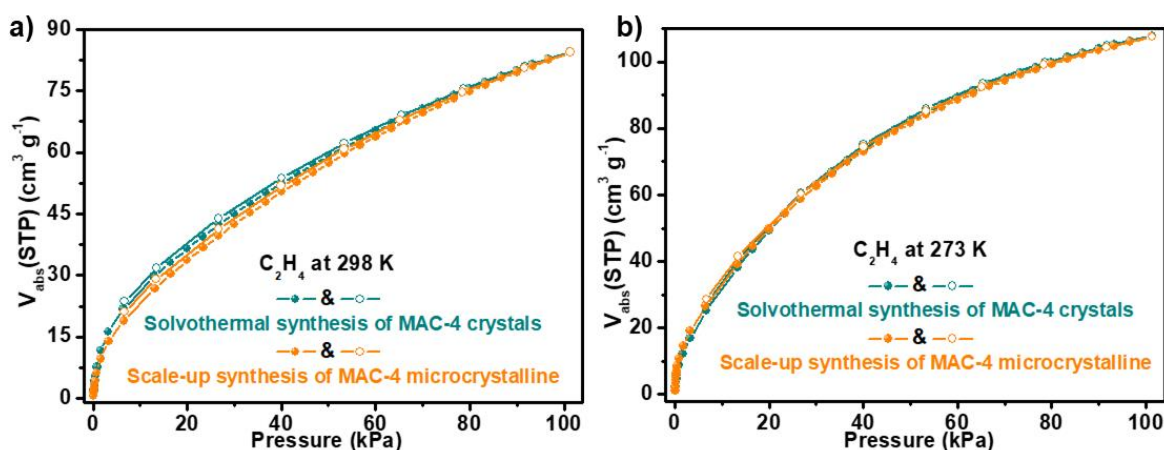


Figure S8. The comparison of adsorption isotherm curves of solvothetical synthesis of MAC-4 crystals samples and scale-up synthesis of MAC-4 microcrystalline samples for  $C_2H_4$  at 298 K a); and 273 K b).

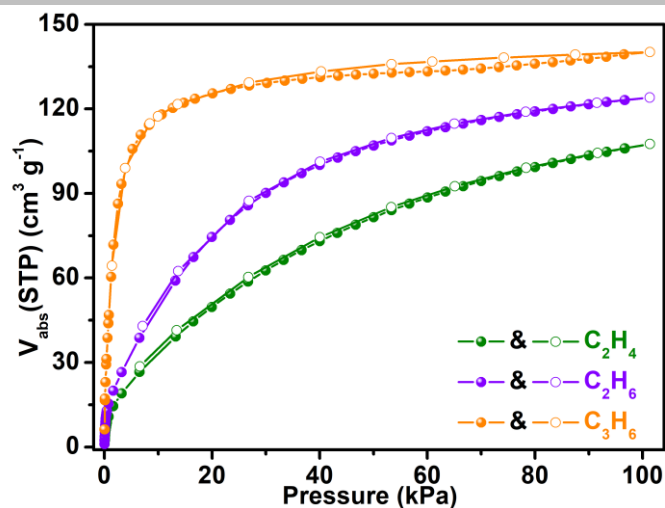


Figure S9.  $C_3H_6$ ,  $C_2H_4$  and  $C_2H_6$  adsorption isotherms of MAC-4 at 273 K.

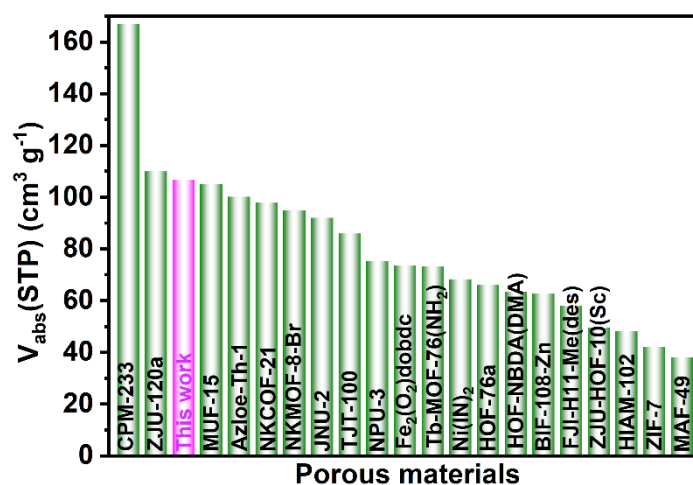


Figure S10. Comparisons of  $C_2H_6$  uptakes in MAC-4 and leading materials at 298 K.

### Fitting adsorption heat of pure component isotherms

The unary isotherms for  $C_3H_6$ ,  $C_2H_6$ , and  $C_2H_4$ , measured at two different temperatures 273 K, and 298 K in MAC-4 were fitted with excellent accuracy using the dual-site Langmuir model, where we distinguish two distinct adsorption sites A and B:

$$q = \frac{q_{sat,A} b_A p}{1 + b_A p} + \frac{q_{sat,B} b_B p}{1 + b_B p} \quad (S1)$$

In eq (S1), the Langmuir parameters  $b_A$ ,  $b_B$  are both temperature dependent

$$b_A = b_{A0} \exp\left(\frac{E_A}{RT}\right); \quad b_B = b_{B0} \exp\left(\frac{E_B}{RT}\right) \quad (S2)$$

In eq (S2),  $E_A$ ,  $E_B$  are the energy parameters associated with sites A, and B, respectively.

The unary isotherm fit parameters are provided in **Fehler! Verweisquelle konnte nicht gefunden werden..**

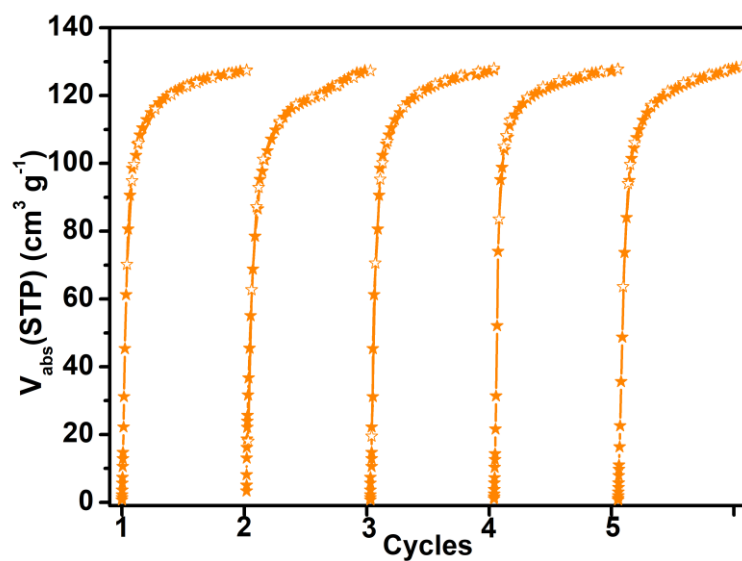
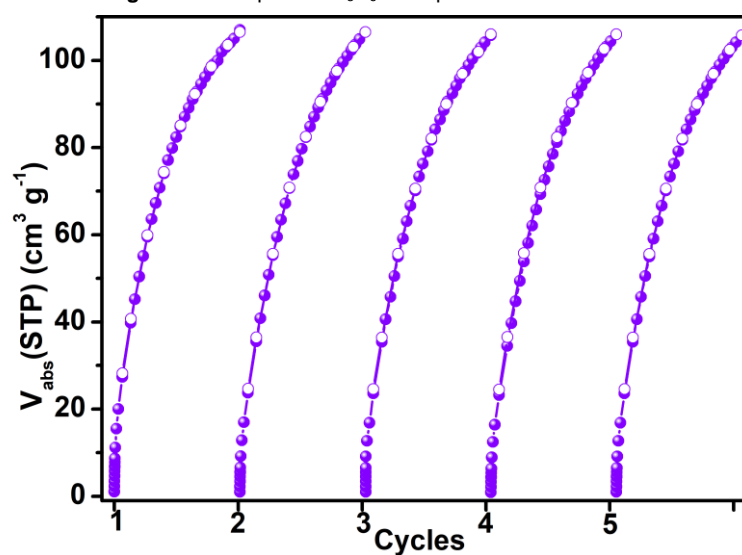
The isosteric heat of adsorption,  $Q_{st}$ , is defined as

$$Q_{st} = -RT^2 \left( \frac{\partial \ln p}{\partial T} \right)_q \quad (S3)$$

where, the derivative in the right member of eq (S3) is determined at constant adsorbate loading,  $q$ . the derivative was determined by analytic differentiation of the combination of eq (S1), eq (S2), and eq (S3).

**Table S1.** Dual-site Langmuir fits for C<sub>3</sub>H<sub>6</sub>, C<sub>2</sub>H<sub>6</sub>, and C<sub>2</sub>H<sub>4</sub> in MAC-4.

	Site A			Site B		
	$\frac{q_{A,sat}}{\text{mol/kg}}$	$\frac{b_{A0}}{\text{Pa}^{-1}}$	$\frac{E_A}{\text{kJ mol}^{-1}}$	$\frac{q_{B,sat}}{\text{mol/kg}}$	$\frac{b_{B0}}{\text{Pa}^{-1}}$	$\frac{E_B}{\text{kJ mol}^{-1}}$
C <sub>3</sub> H <sub>6</sub>	5.4	4.253E-10	31.7	0.7	4.062E-07	24
C <sub>2</sub> H <sub>6</sub>	6.3	8.897E-09	19	0.6	2.389E-07	23
C <sub>2</sub> H <sub>4</sub>	6.8	5.481E-09	18	0.7	1.012E-06	17

**Gas adsorption cycles****Figure S11.** Repetitive C<sub>3</sub>H<sub>6</sub> adsorption curves at 298 K.**Figure S12.** Repetitive C<sub>2</sub>H<sub>6</sub> adsorption curves at 298 K.



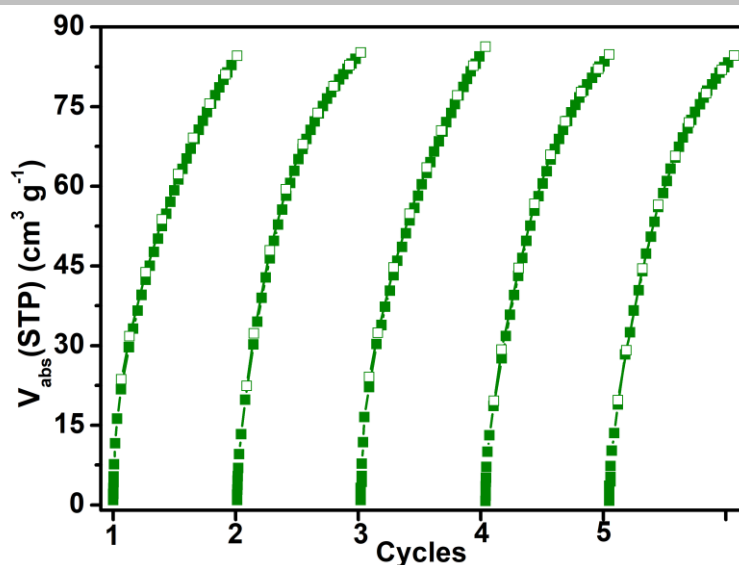


Figure S13. Repetitive C<sub>2</sub>H<sub>4</sub> adsorption curves at 298 K.

### Estimation of production cost of MAC-4

Table S2. The raw material cost of various adsorbents.

Material	Price (\$ g <sup>-1</sup> )	Source
Zn(OAc) <sub>2</sub> ·2H <sub>2</sub> O	0.003 \$ g <sup>-1</sup>	Greagent
Hdmtrz	2.469 \$ g <sup>-1</sup>	Adamas
H <sub>2</sub> IPA	0.007 \$ g <sup>-1</sup>	Adamas
DMF	0.018 \$ mL <sup>-1</sup>	Sigma-Aldrich
MAC-4	1.349 \$ g <sup>-1</sup>	Synthesis

Note: Material cost was calculated by using the required amounts of metal salts and organic ligands precursor. Additionally, the cost of the operation and utility cost for hydrothermal reaction, filtrate, and drying, etc. are not considered.

### Gas selectivity prediction via IAST

The experimental isotherm data for pure C<sub>3</sub>H<sub>6</sub>, C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> were fitted using a dual-site Langmuir-Freundlich (L-F) model:

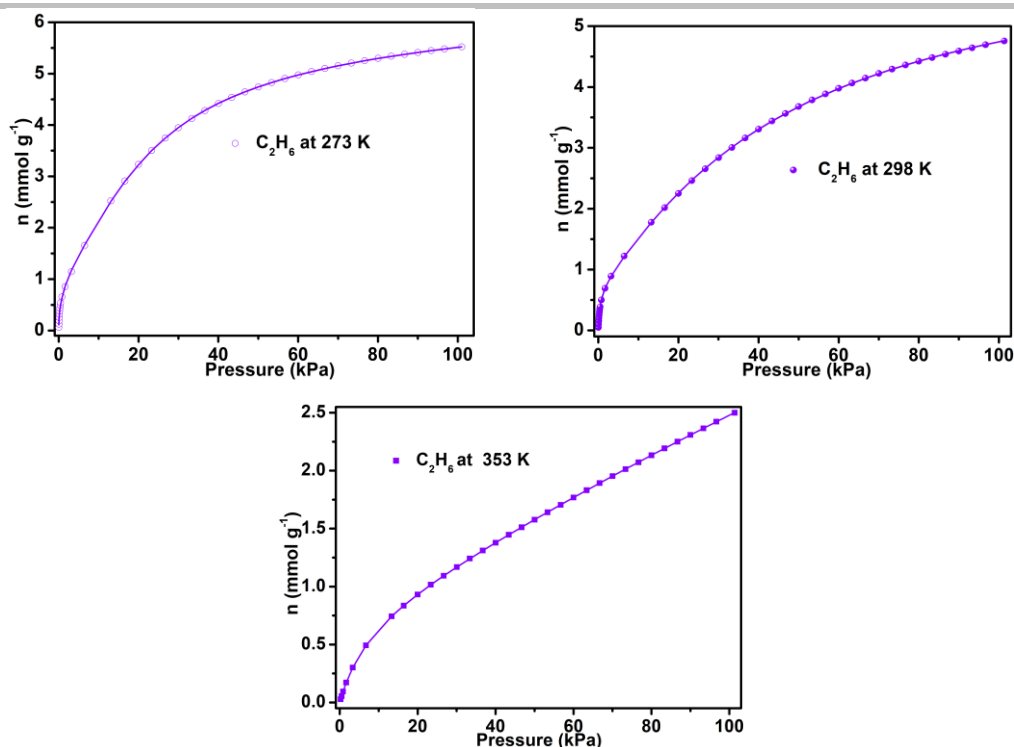
$$q = \frac{a_1 * b_1 * P^{c_1}}{1 + b_1 * P^{c_1}} + \frac{a_2 * b_2 * P^{c_2}}{1 + b_2 * P^{c_2}}$$

Where  $q$  and  $p$  are adsorbed amounts and the pressure of component  $i$ , respectively.

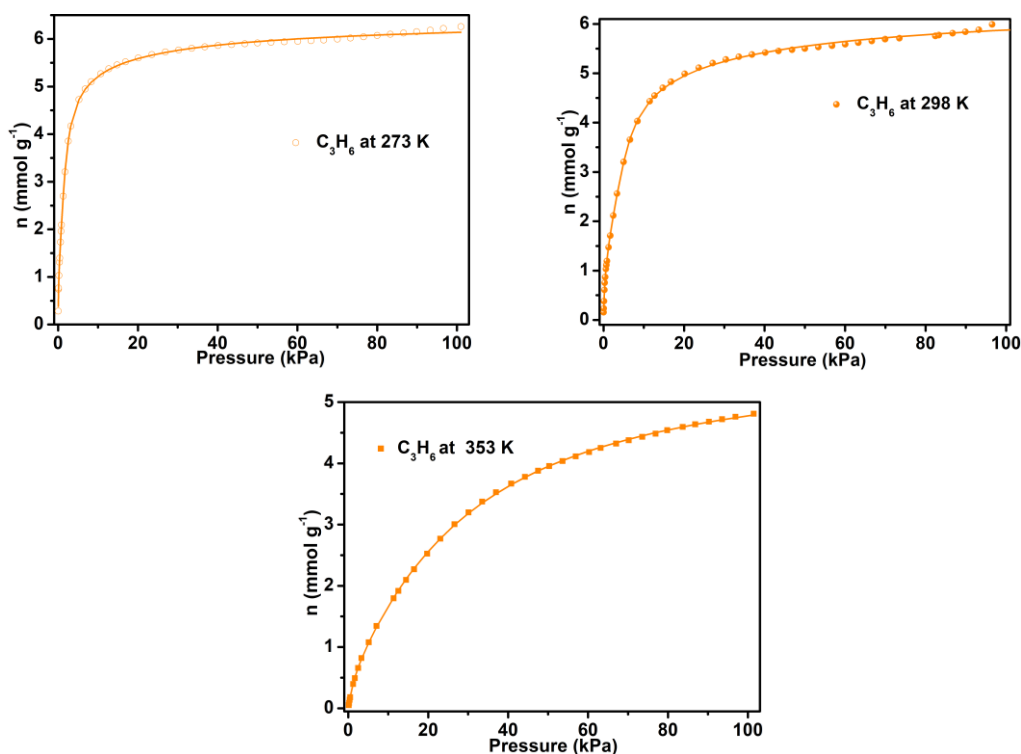
The adsorption selectivities for binary mixtures defined by

$$S_{i/j} = \frac{x_i^* y_j}{x_j^* y_i}$$

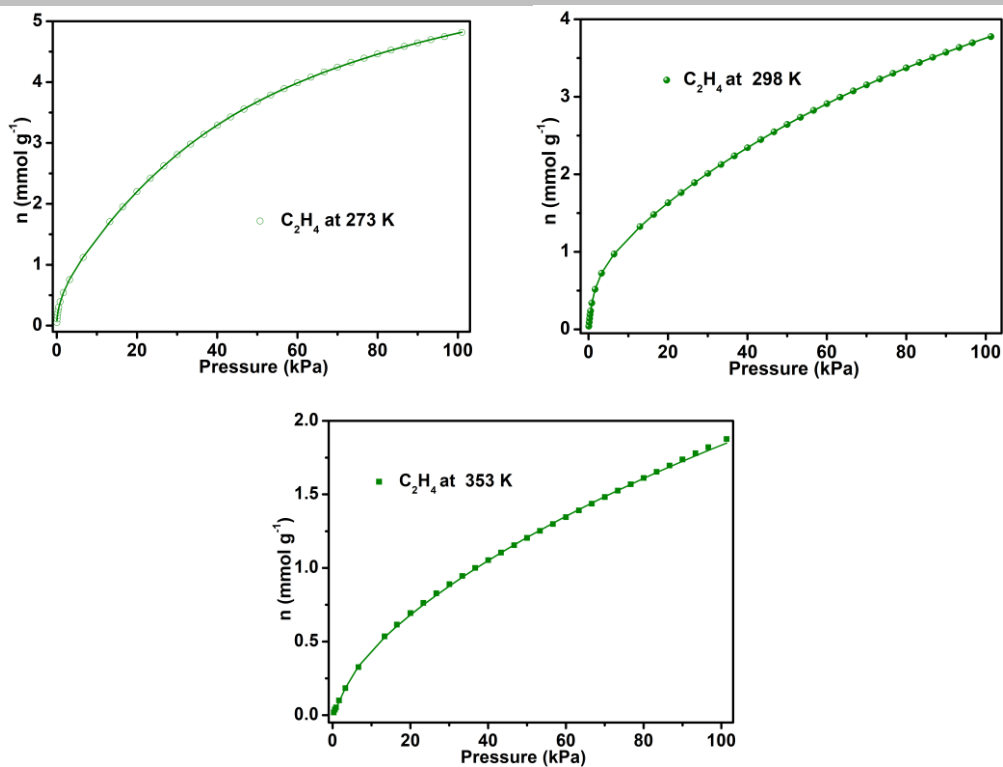
were respectively calculated using the Ideal Adsorption Solution Theory (IAST). Where  $x_i$  is the mole fraction of component  $i$  in the adsorbed phase and  $y_i$  is the mole fraction of component  $i$  in the bulk.



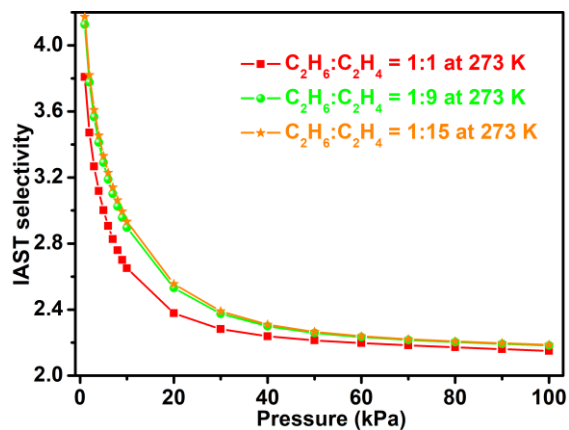
**Figure S14.**  $C_2H_6$  adsorption isotherms of MAC-4 with fitted by dual L-F model, 273 K:  $a_1 = 2.44243$ ,  $b_1 = 0.00296$ ,  $c_1 = 1.89301$ ,  $a_2 = 5.86278$ ,  $b_2 = 0.13443$ ,  $c_2 = 0.47539$ ,  $\chi^2 = 0.00041$ ,  $R^2 = 0.99992$ ; 298 K:  $a_1 = 5.58896$ ,  $b_1 = 0.01072$ ,  $c_1 = 1.18007$ ,  $a_2 = 0.77584$ ,  $b_2 = 1.89883$ ,  $c_2 = 0.97692$ ,  $\chi^2 = 0.00002$ ,  $R^2 = 0.99999$ ; 353 K:  $a_1 = 11.54749$ ,  $b_1 = 0.00088$ ,  $c_1 = 1.14146$ ,  $a_2 = 0.87088$ ,  $b_2 = 0.12614$ ,  $c_2 = 1.00959$ ,  $\chi^2 = 6.818E-7$ ,  $R^2 = 1$ .



**Figure S15.**  $C_3H_6$  adsorption isotherms of MAC-4 with fitted by dual L-F model, 273 K:  $a_1 = 4.63475$ ,  $b_1 = 0.66052$ ,  $c_1 = 0.56825$ ,  $a_2 = 1.96456$ ,  $b_2 = 0.34334$ ,  $c_2 = 2.14875$ ,  $\chi^2 = 0.00154$ ,  $R^2 = 0.99962$ ; 298 K:  $a_1 = 5.36762$ ,  $b_1 = 0.32974$ ,  $c_1 = 0.64812$ ,  $a_2 = 1.22382$ ,  $b_2 = 0.0082$ ,  $c_2 = 2.97596$ ,  $\chi^2 = 0.00201$ ,  $R^2 = 0.99957$ ; 353 K:  $a_1 = 5.06649$ ,  $b_1 = 0.01649$ ,  $c_1 = 1.20353$ ,  $a_2 = 0.68958$ ,  $b_2 = 0.60603$ ,  $c_2 = 1.08723$ ,  $\chi^2 = 0.00018$ ,  $R^2 = 0.99994$ .



**Figure S16.**  $\text{C}_2\text{H}_4$  adsorption isotherms of MAC-4 with fitted by dual L-F model, 273 K:  $a_1 = 9.43954$ ,  $b_1 = 0.04569$ ,  $c_1 = 0.52526$ ,  $a_2 = 1.87921$ ,  $b_2 = 0.002$ ,  $c_2 = 1.73163$ ,  $\text{Chi}^2 = 0.00008$ ,  $R^2 = 0.99998$ ; 298 K:  $a_1 = 6.88414$ ,  $b_1 = 0.00606$ ,  $c_1 = 1.04001$ ,  $a_2 = 0.87108$ ,  $b_2 = 0.64858$ ,  $c_2 = 0.97491$ ,  $\text{Chi}^2 = 3.3222\text{E-}6$ ,  $R^2 = 1$ ; 353 K:  $a_1 = 6.50703$ ,  $b_1 = 0.00649$ ,  $c_1 = 0.8607$ ,  $a_2 = 0.17791$ ,  $b_2 = 0.07126$ ,  $c_2 = 1.81603$ ,  $\text{Chi}^2 = 0.00011$ ,  $R^2 = 0.99973$ .



**Figure S17.** IAST selectivity curves of MAC-4 for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  at 273 K.

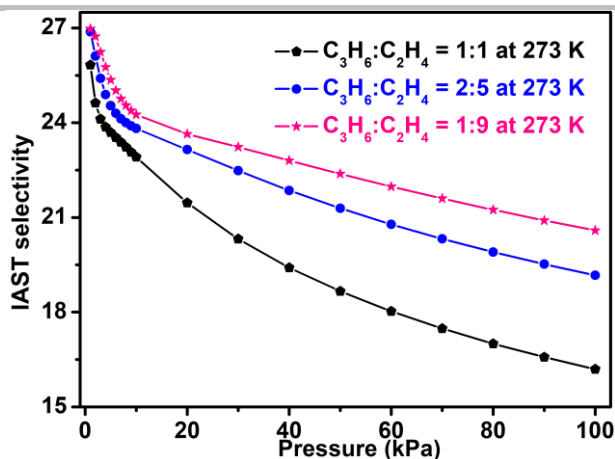


Figure S18. IAST selectivity curves of MAC-4 for  $C_3H_6/C_2H_4$  at 273 K.

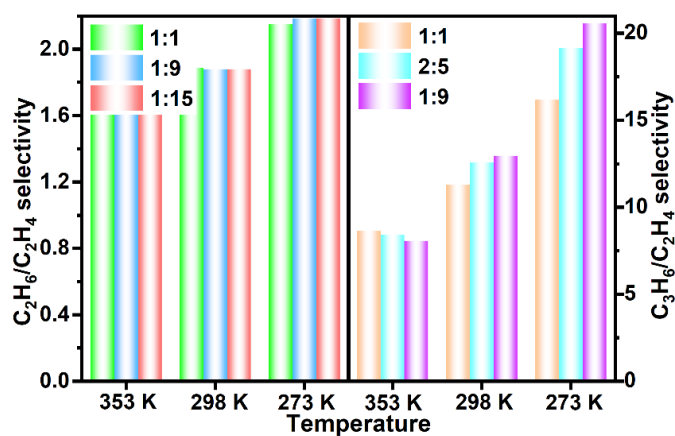


Figure S19. IAST selectivity values of MAC-4 for  $C_2H_6/C_2H_4$  and  $C_3H_6/C_2H_4$  at 353, 298, and 273 K.

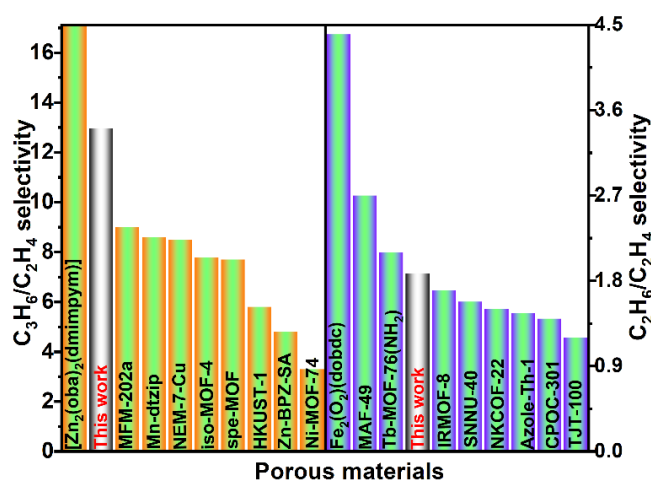


Figure S20. Comparison of  $C_3H_6/C_2H_4$  (left) and  $C_2H_6/C_2H_4$  (right) selectivities in MAC-4 and some benchmark adsorbents at 298 K.

## Separation potential

For separation of binary 50/50 C<sub>2</sub>H<sub>6</sub>(1)/C<sub>2</sub>H<sub>4</sub>(2), 50/50 C<sub>3</sub>H<sub>6</sub>(1)/C<sub>2</sub>H<sub>4</sub>(2) mixtures, the maximum productivity of purified C<sub>2</sub>H<sub>4</sub> that is theoretically achievable in a fixed bed adsorber is determined by the metric defined by Krishna<sup>[2,3]</sup> as the separation potential,  $\Delta Q$ , derived on the basis of the shock wave model

For 50/50 C<sub>2</sub>H<sub>6</sub>(1)/C<sub>2</sub>H<sub>4</sub>(2) mixtures:  $\Delta Q = (q_{C_2H_6})_{50} - q_{C_2H_4}$ ; For 50/50 C<sub>3</sub>H<sub>6</sub>(1)/C<sub>2</sub>H<sub>4</sub>(2) mixtures:  $\Delta Q = (q_{C_3H_6})_{50} - q_{C_2H_4}$

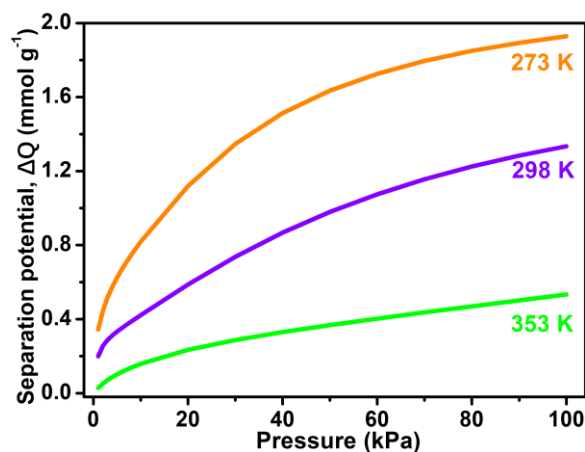


Figure S21. Separation potential of MAC-4 for C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> mixtures at 273, 298, and 353K.

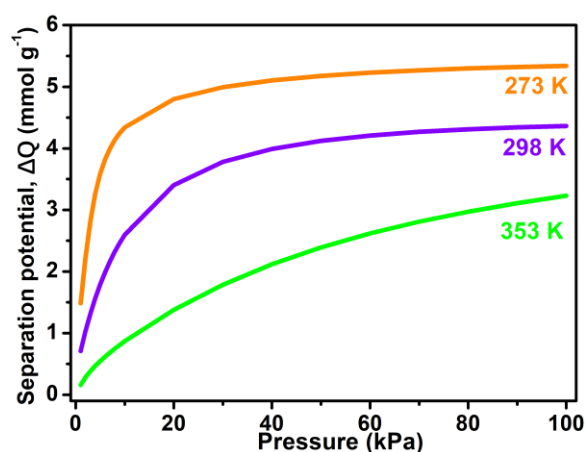
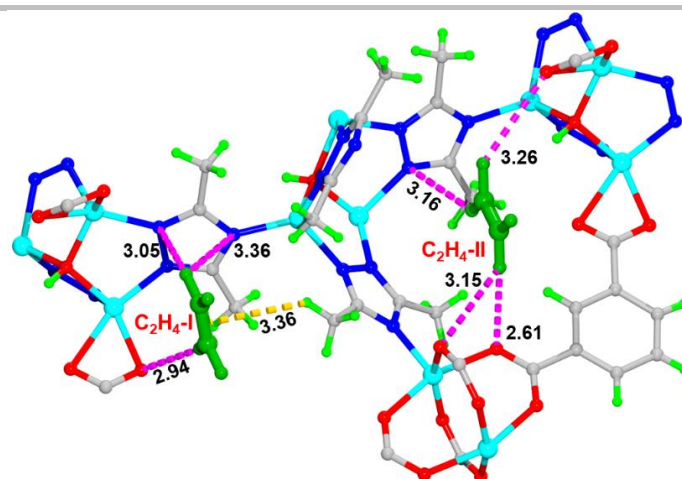


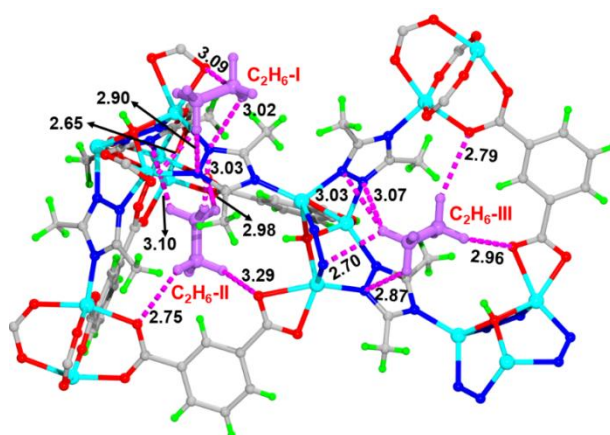
Figure S22. Separation potential of MAC-4 for C<sub>3</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> mixtures at 273, 298, and 353K.

## GC MC simulation

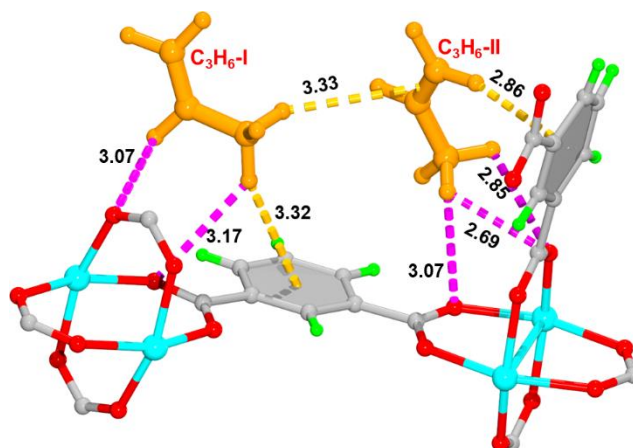
Grand canonical Monte Carlo (GCMC) simulations were performed for the gas adsorption in the framework by the Sorption module of Material Studio (Accelrys. Materials Studio Getting Started). The framework was considered to be rigid, and the optimized gas molecules were used. The partial charges for atoms of the framework were derived from QEq method and QEq neutral 1.0 parameter. One unit cell was used during the simulations. The interaction energies between the gas molecules and framework were computed through the Coulomb and Lennard-Jones 6-12 (LJ) potentials. All parameters for the atoms were modeled with the universal force field (UFF) embedded in the MS modeling package. A cutoff distance of 12.5 Å was used for LJ interactions, and the Coulombic interactions were calculated by using Ewald summation. For each run, the  $3 \times 10^6$  maximum loading steps,  $3 \times 10^6$  production steps were employed. The binding energy was calculated by following equation:  $E_{\text{bind}} = E_{\text{framework+gas}} - E_{\text{framework}} - E_{\text{gas}}$ , in which  $E_{\text{framework+gas}}$  is the total energy of the framework and the adsorbed gas molecule,  $E_{\text{framework}}$  and  $E_{\text{gas}}$  are the energies of the framework and gas molecule. The exchange-correlation functional used in calculations was in the framework of the generalized gradient approximation (GGA) proposed by Perdew, Burke and Ernzerhof (PBE). DNP basis set was used to describe the atomic orbital. The SCF convergence was set to  $1 \times 10^{-6}$ .



**Figure S23.** Adsorption sites for  $C_2H_4$ -I and  $C_2H_4$ -II at 298 K under 100 kPa (H, green; Zn, turquoise; C, gray; O, red; N, blue).



**Figure S24.** Adsorption sites for  $C_2H_6$ -I,  $C_2H_6$ -II and  $C_2H_6$ -III at 298 K under 100 kPa (H, green; Zn, turquoise; C, gray; O, red; N, blue).



**Figure S26.** Adsorption sites for  $C_3H_6$ -I and  $C_2H_6$ -II at 298 K under 100 kPa (H, green; Zn, turquoise; C, gray; O, red; N, blue).

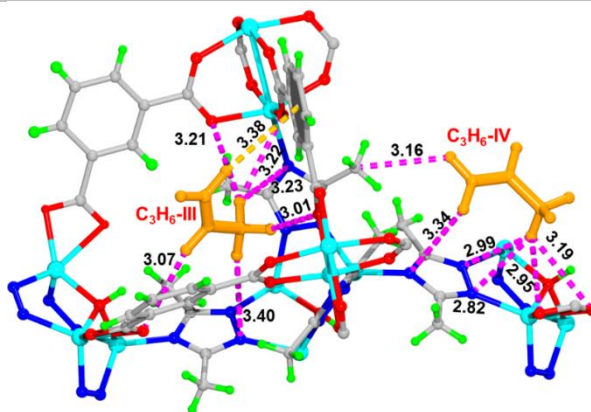


Figure S26. Adsorption sites for  $C_3H_6$ -I and  $C_2H_6$ -IV at 298 K under 100 kPa (H, green; Zn, turquoise; C, gray; O, red; N, blue).

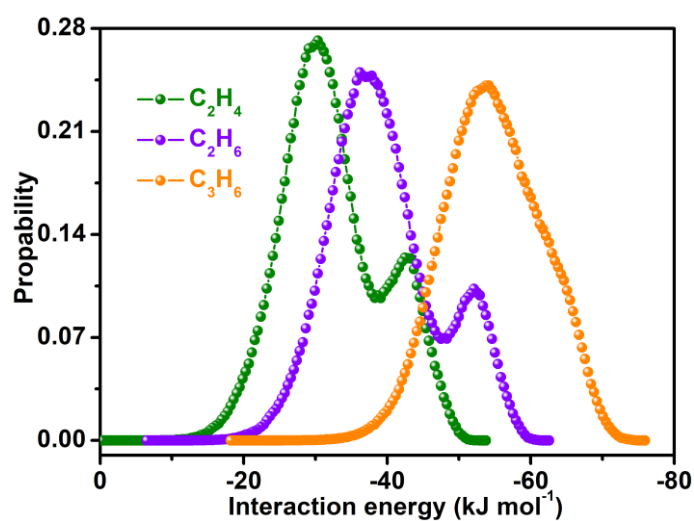


Figure S27. Interaction energy distribution of  $C_2H_4$ ,  $C_2H_6$ , and  $C_3H_6$  in the MAC-4.

## Breakthrough experiments

The breakthrough experiments were performed on the Quantachrome dynaSorb BT equipments at 273, 298 and 353 K and 100 kPa with Ar as the carrier gas. The activated MAC-4 (about 0.88 g) was filled into a packed column of  $\phi$  4.2 mm  $\times$  80 mm, and then the packed column was washed with Ar at a rate of 7 mL min<sup>-1</sup> at 343 K for 50 minutes to further activate the samples. Between two breakthrough experiments, the adsorbent was regenerated by Ar flow of 7 mL min<sup>-1</sup> for 35 min at 343 K to guarantee a complete removal of the adsorbed gas.

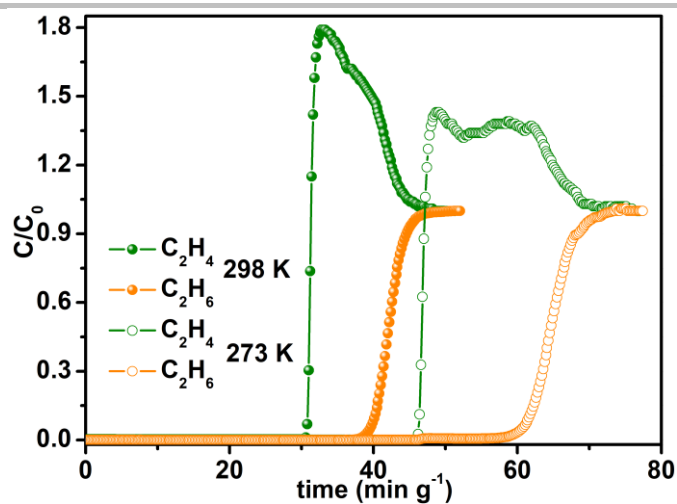


Figure S28. Breakthrough curves of MAC-4 for equimolar  $C_2H_6/C_2H_4$  (10/10, v/v) mixtures at 298 and 273 K with Ar as the carrier gas (80%, vol%).

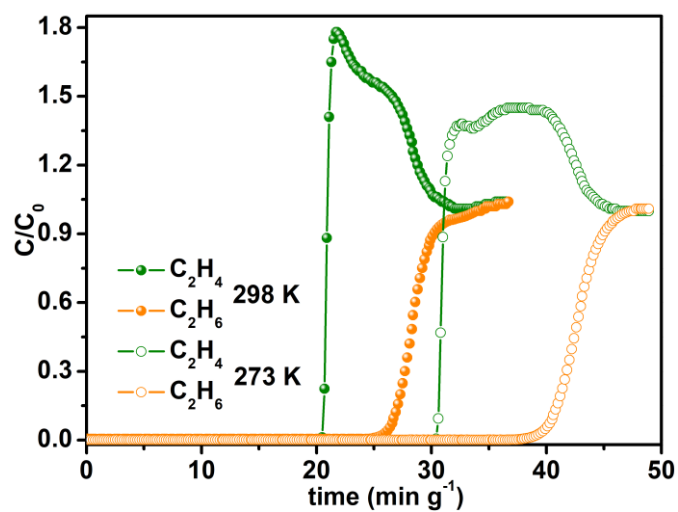


Figure S29. Breakthrough curves of MAC-4 for equimolar  $C_2H_6/C_2H_4$  (20/20, v/v) mixtures at 298 and 273 K with Ar as the carrier gas (60%, vol%).

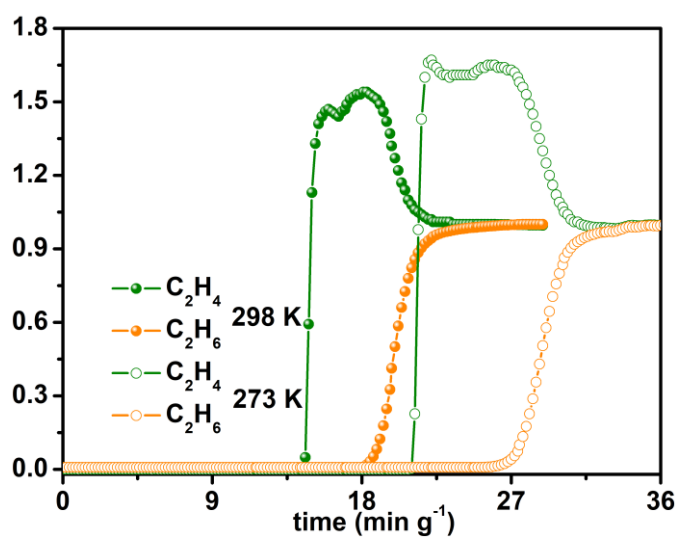


Figure S30. Breakthrough curves of MAC-4 for equimolar  $C_2H_6/C_2H_4$  (30/30, v/v) mixtures at 298 and 273 K with Ar as the carrier gas (40%, vol%).



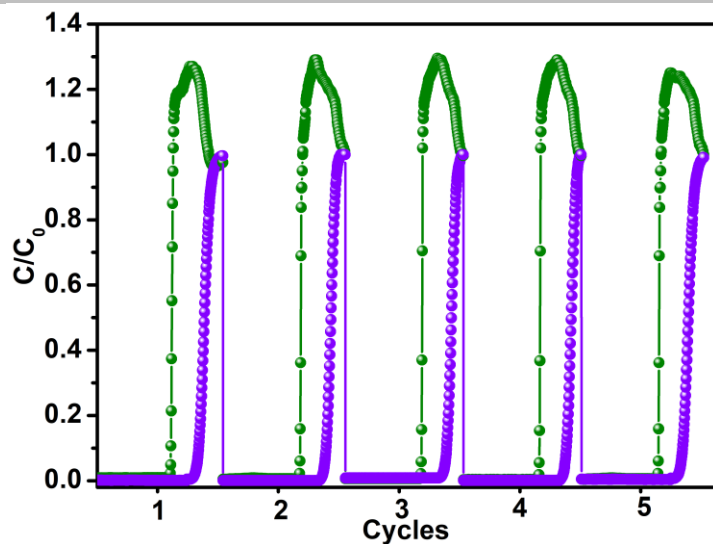


Figure S31. Breakthrough cycles of MAC-4 for  $C_2H_6/C_2H_4$  mixtures at 298 K.

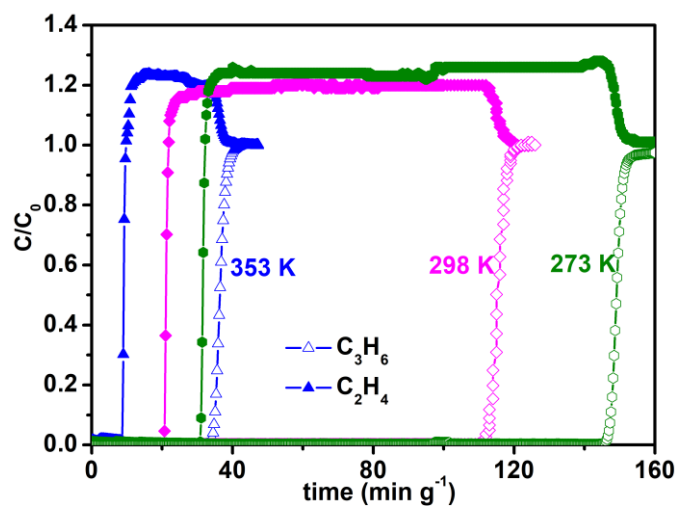


Figure S32. Breakthrough curves for  $C_3H_6/C_2H_4$  (v/v, 10/25) mixtures at 353, 298 and 273 K.

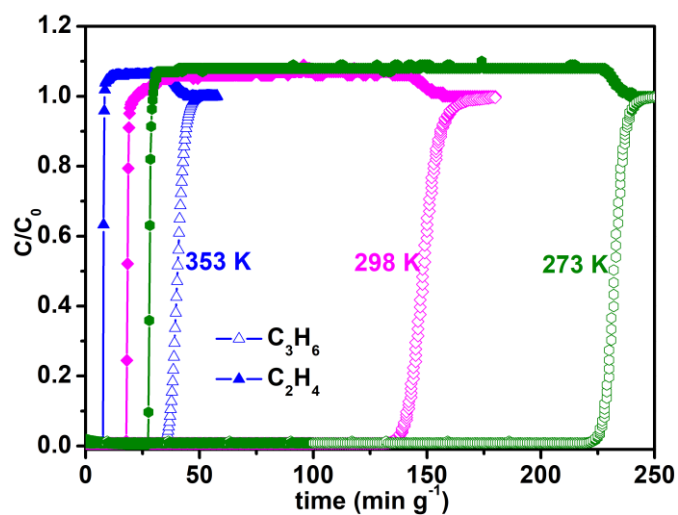
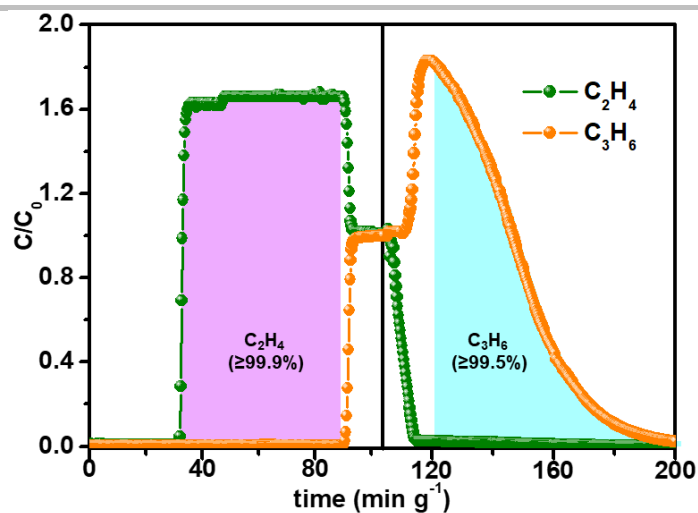
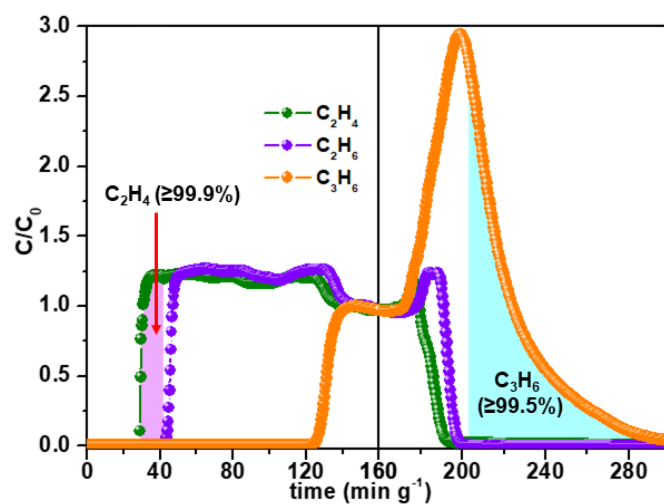


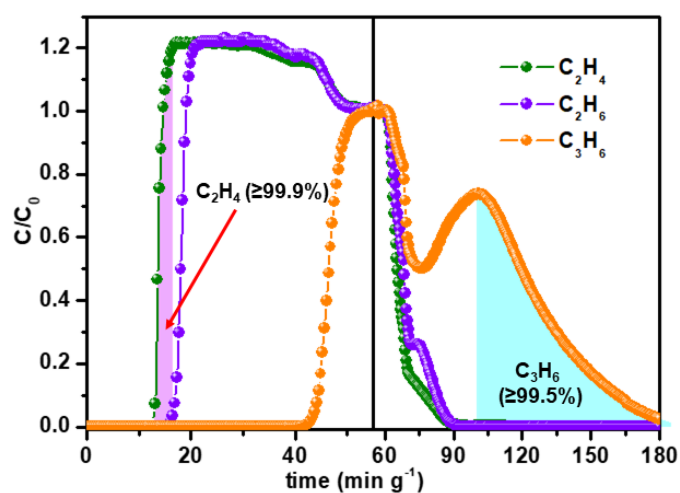
Figure S33. Breakthrough curves for  $C_3H_6/C_2H_4$  (v/v, 4/36) mixtures at 353, 298 and 273 K.



**Figure S34.** Breakthrough curves for  $C_3H_6/C_2H_4$  (v/v, 20/20) mixtures at 273 K, followed by desorption curves under Ar ( $7\ mL\ min^{-1}$ ) sweeping at 323 K.



**Figure S35.** Breakthrough curves for  $C_2H_6/C_3H_6/C_2H_4$  mixture (v/v/v, 5/5/5) mixtures at 298 K, followed by desorption curves under Ar ( $7\ mL\ min^{-1}$ ) sweeping at 323 K.



**Figure S36.** Breakthrough curves for  $C_2H_6/C_3H_6/C_2H_4$  mixture (v/v/v, 5/5/5) mixtures at 353 K, followed by desorption curves under Ar ( $7\ mL\ min^{-1}$ ) sweeping at 323 K.

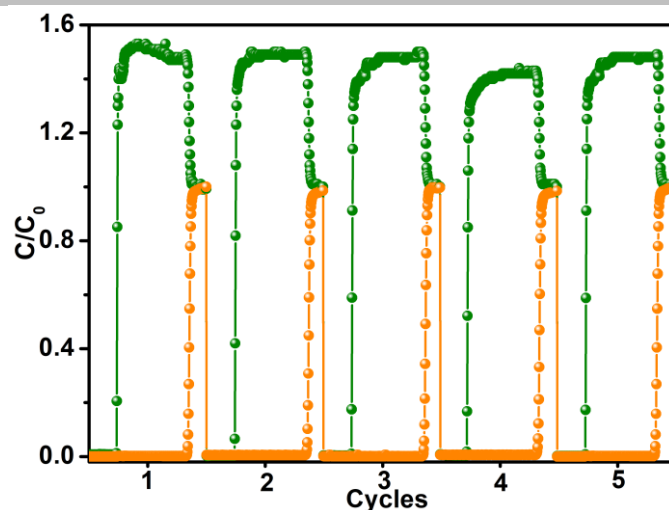


Figure S37. Breakthrough cycles of MAC-4 for  $C_3H_6/C_2H_4$  mixtures at 298 K.

### Transient breakthrough simulations vs experiments with inert gas

The transient breakthrough experiments were conducted with mass of MAC-4  $m_{ads} = 0.88$  g; length of packed bed,  $L = 80$  mm; diameter of packed bed = 4.2 mm. The mixtures examined were:

$C_3H_6/C_2H_4/Ar$  mixtures (20/20/60 v/v) with Ar as the carrier gas, and a total flow rate of  $8.0 \text{ mL min}^{-1}$  (353 K and 298 K, 100 kPa);

$C_2H_6/C_2H_4/Ar$  mixtures (5/5/90, 1/9/90, and 1/15/84, v/v/v) with Ar as the carrier gas, and a total flow rate of  $7 \text{ mL min}^{-1}$  (353 K and 298 K, 100 kPa);

$C_3H_6/C_2H_6/C_2H_4/Ar$  mixtures (5/5/5/85, 10/2/25/63, v/v/v/v, ) with Ar as the carrier gas, and a total flow rate of  $8 \text{ mL min}^{-1}$  (353 K and 298 K, 100 kPa).

Transient breakthrough simulations were carried out for the exact same set of operating conditions as in the above mentioned experiments, using the methodology described in earlier publications.<sup>[2-7]</sup> In these simulations, intra-crystalline diffusion influences are ignored. There is good match between the experiments and simulations in every case.

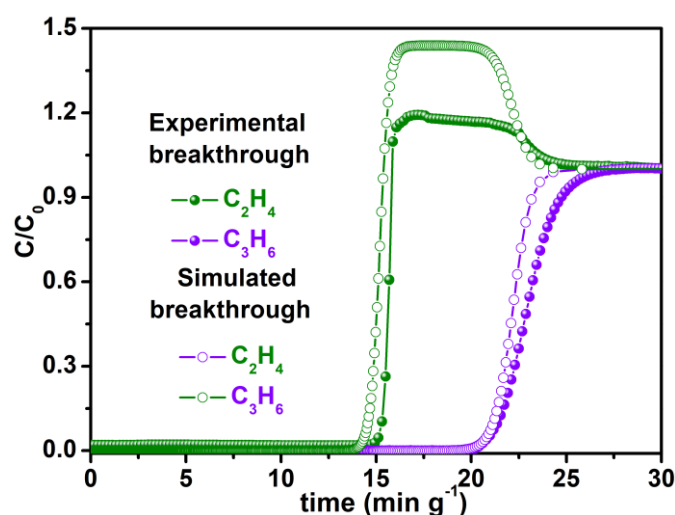


Figure S38. Comparison of the transient breakthrough curves and experimental breakthrough curves for  $C_2H_6/C_2H_4$  (5/5) mixtures at 353 K.

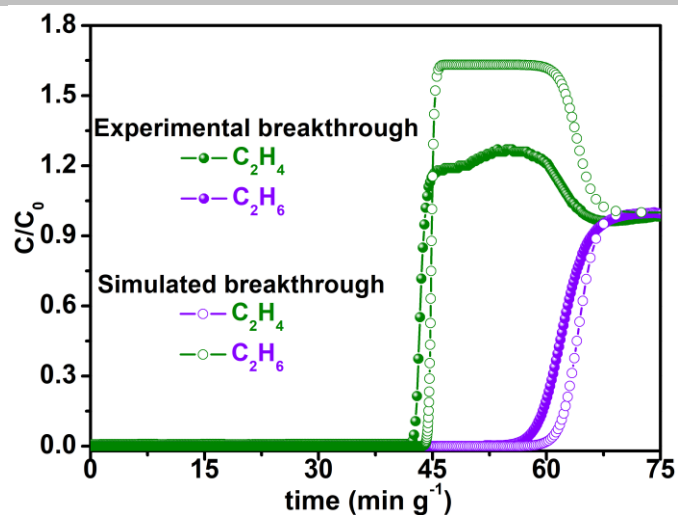


Figure S39. Comparison of the transient breakthrough curves and experimental breakthrough curves for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (5/5) mixtures at 298 K.

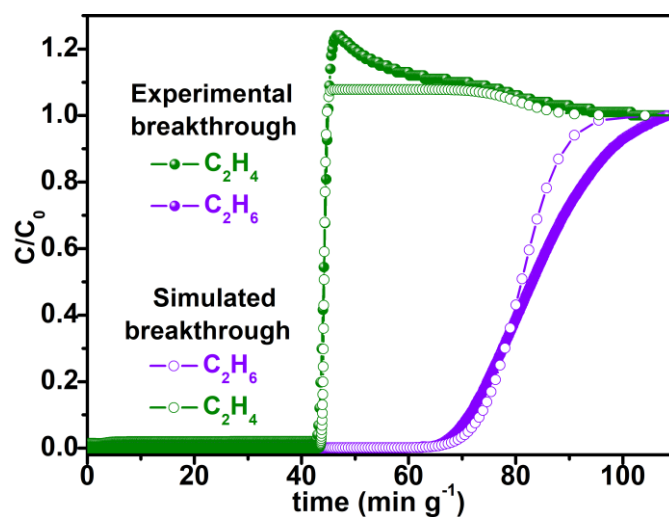


Figure S40. Comparison of the transient breakthrough curves and experimental breakthrough curves for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (1/9) mixtures at 298 K.

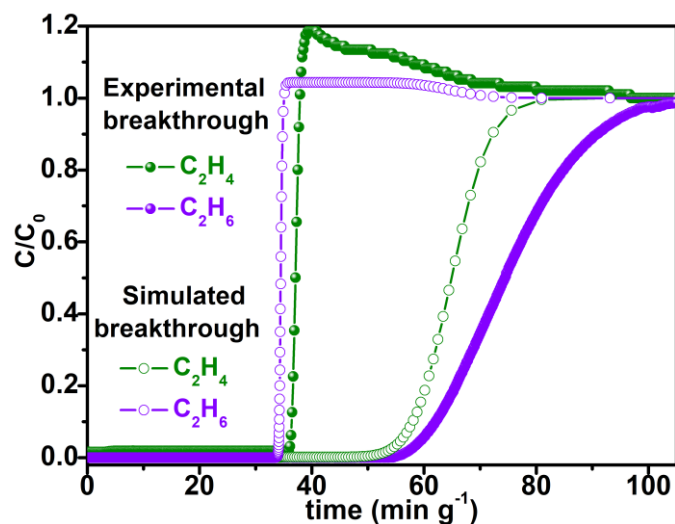


Figure S41. Comparison of the transient breakthrough curves and experimental breakthrough curves for  $\text{C}_2\text{H}_6/\text{C}_2\text{H}_4$  (1/15) mixtures at 298 K.

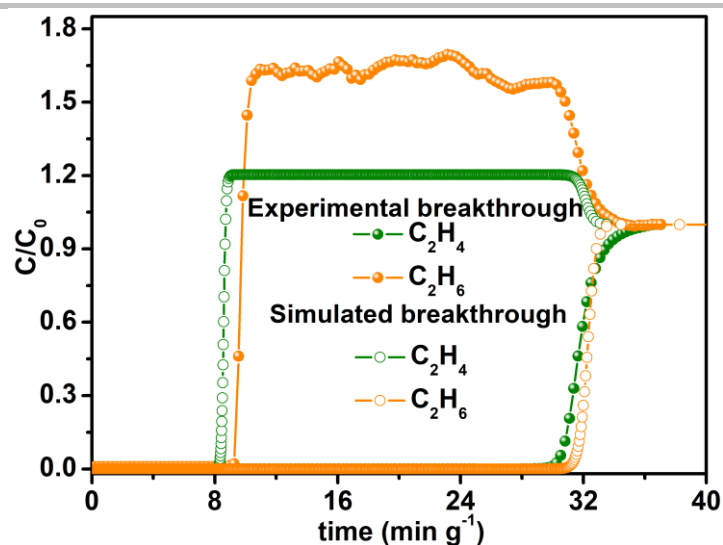


Figure S42. Comparison of the transient breakthrough curves and experimental breakthrough curves for  $C_3H_6/C_2H_4$  (20/20) mixtures at 353 K.

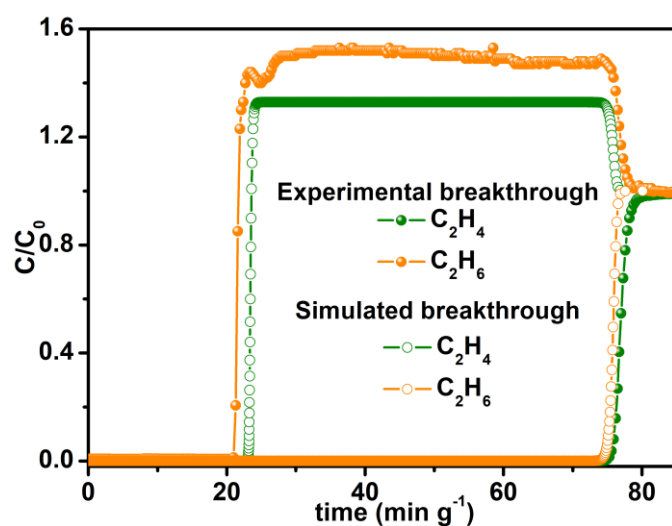


Figure S43. Comparison of the transient breakthrough curves and experimental breakthrough curves for  $C_3H_6/C_2H_4$  (20/20) mixtures at 298 K.

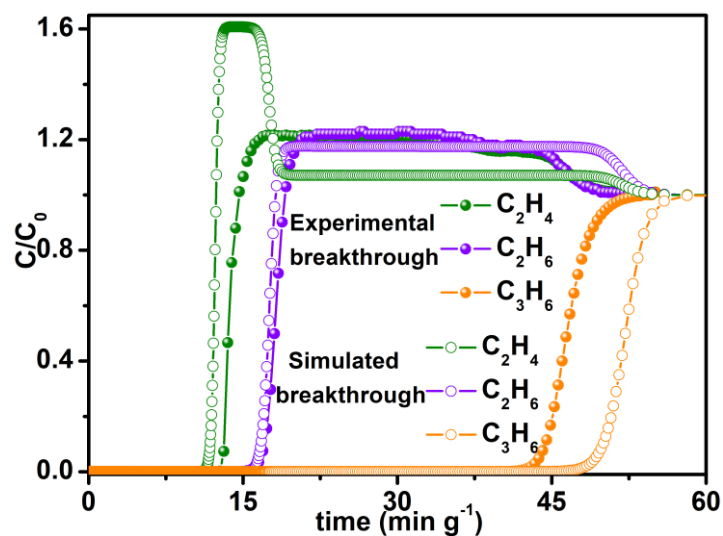
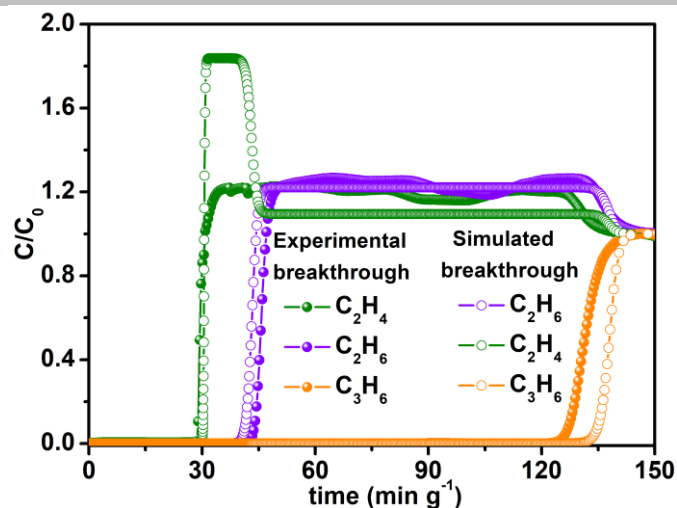


Figure S44. Comparison of the transient breakthrough curves and experimental breakthrough curves for  $C_3H_6/C_2H_6/C_2H_4$  (5/5/5) mixtures at 353 K.



**Figure S45.** Comparison of the transient breakthrough curves and experimental breakthrough curves for  $C_3H_6/C_2H_6/C_2H_4$  (5/5/5) mixtures at 298 K.

### Transient breakthrough simulations without inert gas

Having established the accuracy of the transient breakthrough simulations, a set of simulations were carried out without inert gas in a fixed bed packed with MAC-4  $m_{ads} = 0.88$  g; length of packed bed,  $L = 80$  mm; diameter of packed bed = 4.2 mm. The total pressure is 100 kPa, and two different temperatures were used: 298 K and 353 K. The following mixtures were simulated.

50/50  $C_2H_6(1)/C_2H_4(2)$  mixtures

50/50  $C_3H_6(1)/C_2H_4(2)$  mixtures

33.33/33.33/33.33  $C_3H_6(1)/C_2H_6(2)/C_2H_4(3)$  mixtures

The breakthrough data are presented in terms of the dimensionless concentrations at the exit of the fixed bed,  $\frac{C_A}{C_{A0}}$ , as function of the

modified time parameter  $\frac{(Q_0 = \text{flow rate mL min}^{-1}) \times (\text{time in min})}{(\text{g MOF packed in tube})} = \frac{Q_0 t}{m_{ads}} = \text{mL g}^{-1}$ .

From the transient breakthrough simulations, the productivity of 99.9%  $C_2H_4$  was determined from a material balance.

Notation:

$b$	Langmuir constant, $\text{Pa}^{-1}$
$E$	energy parameter, $\text{J mol}^{-1}$
$L$	length of packed bed adsorber, m
$m_{ads}$	mass of adsorbent packed in fixed bed, g
$p_i$	partial pressure of species $i$ in mixture, Pa
$p_t$	total system pressure, Pa
$q_i$	component molar loading of species $i$ , $\text{mol kg}^{-1}$
$q_t$	total molar loading in mixture, $\text{mol kg}^{-1}$
$q$	component molar loading of species $i$ , $\text{mol kg}^{-1}$
$q_{sat}$	saturation loading, $\text{mol kg}^{-1}$
$Q_0$	volumetric flow rate of gas mixture entering fixed bed, $\text{m}^3 \text{s}^{-1}$
$Q_{st}$	isosteric heat of adsorption, $\text{kJ mol}^{-1}$
$T$	absolute temperature, K
$u$	superficial gas velocity in packed bed, $\text{m s}^{-1}$
$\varepsilon$	voidage of packed bed, dimensionless
$\rho$	framework density, $\text{kg m}^{-3}$

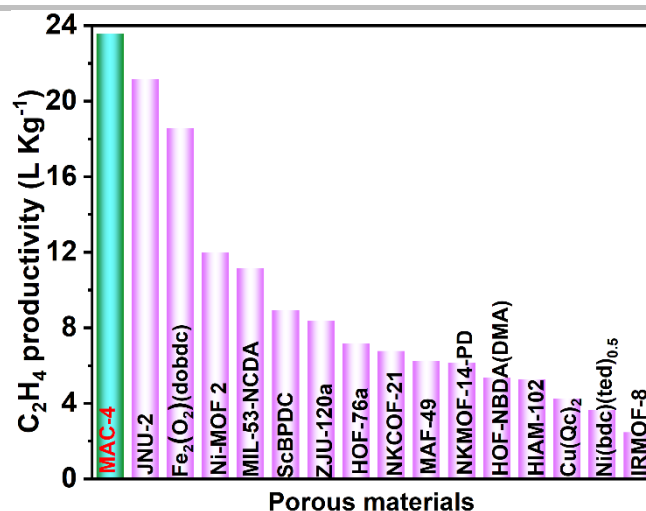


Figure S46. Comparison of C<sub>2</sub>H<sub>4</sub> productivity from equimolar C<sub>2</sub>H<sub>6</sub>/C<sub>2</sub>H<sub>4</sub> mixture in MAC-4 and reported porous adsorbents.

### Infrared spectroscopy study

Infrared (IR) measurements were performed on a Bruker INVENIO S ATR-FTIR spectrometer. The samples of gas-loaded MAC-4 were prepared by the method described below: The sample of MAC-4 was filled into a glass tube and heated at 140 °C under vacuum for 4h. After the sample cooling down, C<sub>2</sub>H<sub>4</sub>, C<sub>3</sub>H<sub>6</sub>, and C<sub>2</sub>H<sub>6</sub> was introduced into the sample respectively with Micrometrics TriStar II 3020 instrument until the pressure reach to 100 kPa at 298 K and the state is maintained for two hours. Then gas loading sample were picked out for infrared measurement immediately.

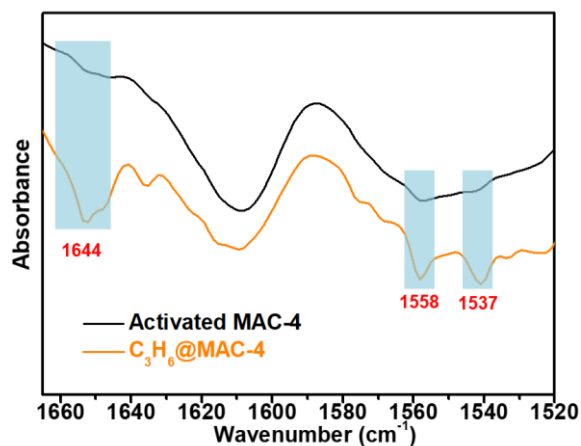


Figure S47. Comparison of IR spectra at 1660-1520 cm<sup>-1</sup> of activated and C<sub>3</sub>H<sub>6</sub>-loaded MAC-4.

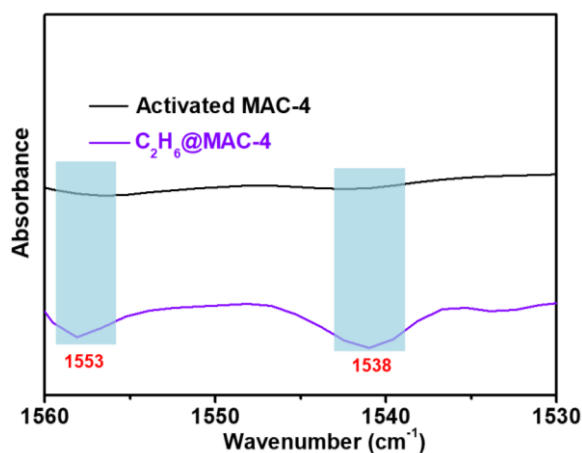


Figure S48. Comparison of IR spectra at 1560-1530 cm<sup>-1</sup> of activated and C<sub>2</sub>H<sub>6</sub>-loaded MAC-4.

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- [1] Y. Ling, F. Yang, M. Deng, Z. Chen, X. Liu, L. Weng, Y. Zhou, *Dalton Trans.* **2012**, 41, 4007-4011.
- [2] R. Krishna, *RSC Adv.* **2017**, 7, 35724-35737.
- [3] R. Krishna, *ACS Omega* **2020**, 5, 16987-17004.
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- [7] R. Krishna. *Precision Chemistry* **2023**, 1, 83-93.

## Author contributions

**Gang-Ding Wang:** Synthesis, characterization, adsorption experiments, writing - original draft. **Yong-Zhi Li:** Breakthrough experiments, writing - review & editing. **Rajamani Krishna:** Breakthrough simulation,  $Q_{st}$  calculation. **Wen-Yan Zhang:** Formal analysis. **Lei Hou:** Formal analysis, writing - review & editing, supervision, methodology, funding acquisition. **Yao-Yu Wang:** Resources. **Zhonghua Zhu:** Formal analysis.