

Immobilization of the Polar Group into an Ultramicroporous Metal–Organic Framework Enabling Benchmark Inverse Selective CO₂/C₂H₂ Separation with Record C₂H₂ Production

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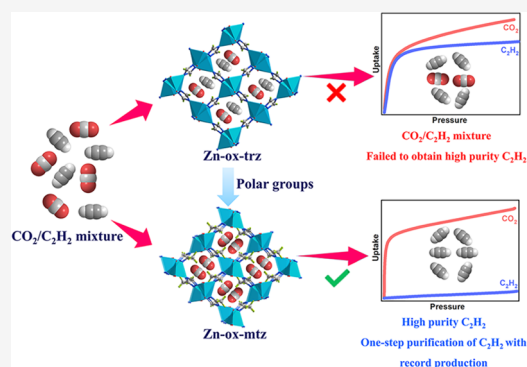
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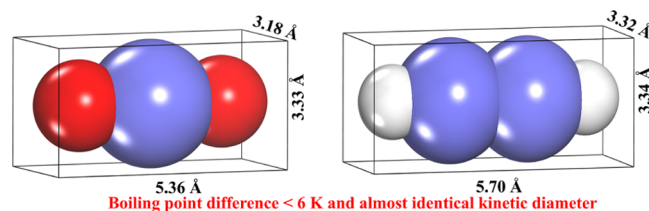
ABSTRACT: One-step harvest of high-purity light hydrocarbons without the desorption process represents an advanced and highly efficient strategy for the purification of target substances. The separation and purification of acetylene (C₂H₂) from carbon dioxide (CO₂) by CO₂-selective adsorbents are urgently demanded yet are very challenging owing to their similar physicochemical properties. Here, we employ the pore chemistry strategy to adjust the pore environment by immobilizing polar groups into an ultramicroporous metal–organic framework (MOF), achieving one-step manufacture of high-purity C₂H₂ from CO₂/C₂H₂ mixtures. Embedding methyl groups into prototype stable MOF (Zn-ox-trz) not only changes the pore environment but also improves the discrimination of guest molecules. The methyl-functionalized Zn-ox-mtz thus exhibits the benchmark reverse CO₂/C₂H₂ uptake ratio of 12.6 (123.32/9.79 cm³ cm⁻³) and an exceptionally high equimolar CO₂/C₂H₂ selectivity of 1064.9 at ambient conditions. Molecular simulations reveal that the synergistic effect of pore confinement and surfaces decorated with methyl groups provides high recognition of CO₂ molecules through multiple van der Waals interactions. The column breakthrough experiments suggest that Zn-ox-mtz dramatically achieved the one-step purification capacity of C₂H₂ from the CO₂/C₂H₂ mixture with a record C₂H₂ productivity of 2091 mmol kg⁻¹, surpassing all of the CO₂-selective adsorbents reported so far. In addition, Zn-ox-mtz exhibits excellent chemical stability under different pH values of aqueous solutions (pH = 1–12). Moreover, the highly stable framework and excellent inverse selective CO₂/C₂H₂ separation performance showcase its promising application as a C₂H₂ splitter for industrial manufacture. This work paves the way to developing reverse-selective adsorbents for the challenging gas separation process.



INTRODUCTION

The separation and purification of gaseous mixtures are particularly important in the petrochemical industry to produce high-value downstream chemicals such as fuel, plastics, and polymers.^{1,2} Acetylene (C₂H₂), as the simplest alkyne, is not only a vital gas fuel but also an important precursor chemical and basic building block in the industry, which is generally used to produce high-value chemicals such as acrylic acid, 1,4-butanediol, and 1,4-butanediol.³ C₂H₂ is generally derived from the steam cracking of petroleum or/and naphtha and methane partial combustion, in this context, carbon dioxide (CO₂) contaminant inevitably draws into the product of crude C₂H₂.⁴ Therefore, the removal of CO₂ impurity is a necessary step before further manufacturing high-value-added chemicals. CO₂ and C₂H₂ molecules exhibit highly similar physical properties and possess close molecular shapes and sizes, such as boiling point (C₂H₂: 189.3 K and CO₂: 194.7 K) and molecular size (C₂H₂: 3.34 × 3.32 × 5.70 Å³ and CO₂: 3.33 × 3.18 × 5.36 Å³) (Scheme 1).⁵ In addition, both CO₂ and C₂H₂ are nonpolar linear molecules with almost

Scheme 1. Comparison of the Molecular Structure and Physical Property of CO₂ (Left) and C₂H₂ (Right)



identical kinetic diameters of approximately 3.3 Å. Given their similar physical properties, there is no doubt that the

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separation of the CO₂/C₂H₂ mixture is still a daunting challenging process,^{6–9} in particular, removing the trace amounts of CO₂ from C₂H₂, and their separation has attracted the interest of scientists and engineers due to its scientific problem and industrial relevance. At present, the separation of the CO₂/C₂H₂ mixture mainly utilizes organic solvent extraction or/and cryogenic distillation,^{4,10} which require high energy, are cost-intensive, and are environmentally unfriendly. Adsorptive separation using porous solid adsorbents based on the physical adsorption mechanism, such as pressure swing adsorption (PSA) and temperature swing adsorption (TSA), is an effective alternative technology, which is an economically viable and energy-efficient process and more environmentally friendly. Therefore, the development and design of novel porous adsorbents for the separation and purification of C₂H₂ from a CO₂/C₂H₂ mixture are urgently demanded yet challenging.

Extensive endeavors have been devoted to exploring porous solid adsorbents including but not limited to zeolites, activated carbons, metal–organic frameworks (MOFs), hydrogen-bonded organic frameworks (HOFs), covalent–organic frameworks (COFs), and hybrid ultramicroporous materials (HUMs).^{11–16} Especially, MOFs, also called porous coordination polymers (PCPs), as novel porous organic–inorganic hybrid materials, are constructed from the self-assembly of metal ions or clusters and organic ligands, which become promising adsorbents for gas mixture separation owing to their tunable pore size and pore chemistry.^{12,17,18} The rational design of the pore shape/size and pore chemistry based on the modular feature of MOFs in reticular chemistry and crystal engineering has enabled some MOF adsorbents to exhibit unprecedented adsorption and separation performance for hydrocarbons, including but not limited to C₂H₂/C₂H₄, C₂H₆/C₂H₄, and C₃H₆/C₃H₈.^{19–23} However, the almost same kinetic diameter of CO₂ and C₂H₂ makes it greatly challenging for MOFs to differentiate these gases. Recently, a large number of MOF adsorbents have been reported to be used for CO₂/C₂H₂ separation, with almost all of them exhibiting a C₂H₂-selective adsorption behavior. The C₂H₂-selective MOFs could enhance the C₂H₂–framework interaction by designing interaction sites such as hydrogen-bonding interaction, Lewis basic interaction, and C₂H₂–metal π -complexation, obtaining C₂H₂/CO₂ separation ability.^{24–29} However, such C₂H₂-selective MOF adsorbents need the desorption process to obtain high-purity C₂H₂; furthermore, the strong C₂H₂–framework interactions may cause more energy consumption in the desorption process. Given that the main impurity CO₂ accounts for 3–50% of the C₂H₂ crude,¹¹ the reverse CO₂-selective MOFs, i.e., preferential adsorption of CO₂ over C₂H₂, are more suitable for separation requirements. Compared with other complicated regeneration processes, it could save about 40% energy consumption by directly obtaining the product process.³⁰ Undoubtedly, the judicious design of reverse CO₂-selective MOFs is very important yet greatly difficult, and the reported CO₂-selective MOFs are still very rare.^{9,18} With respect to practical industrial implementation processes, sufficient stability is a prerequisite for gas separation applications, especially the chemical stability tolerance of water, acids, and bases. Furthermore, the trade-off between reverse CO₂/C₂H₂ selectivity and CO₂ uptake is still a great obstacle in state-of-the-art adsorbents. For instance, the benchmark MOF Cu–Fpymo exhibits unprecedentedly high CO₂/C₂H₂ selectivity (>10⁵), while the CO₂ uptake is only 26.6 cm³ g^{–1}, leading to

low C₂H₂ productivity;³¹ SIFSIX-3-Ni and CD-MOFs exhibit CO₂ adsorption uptakes of 98.4 and 60.4 cm³ cm^{–3}, while the reverse CO₂/C₂H₂ selectivities are only 7.7 and 6.6, respectively.^{7,32} Thus, the construction of stable reverse CO₂-selective MOF adsorbents with high CO₂ uptake and high CO₂/C₂H₂ selectivity is a daunting challenge and yet important for the separation and purification of C₂H₂.

Since the kinetic diameters of CO₂ and C₂H₂ are almost identical, the efficient separation of the CO₂/C₂H₂ mixture cannot be realized simply by tuning the pore size, unlike other gaseous mixtures, such as CO₂/N₂ and alkyne/alkene.^{33,34} It is worth noting that there is a key difference in electrostatic potentials (ESPs) and quadrupole moments of CO₂ and C₂H₂. Therefore, it is significant to construct specific functional binding sites within the MOFs that could achieve inverse CO₂-selective behavior for the effective purification of C₂H₂. It is generally believed that ultramicroporous adsorbents featuring a compact pore space and positively charged distribution could maximize the inverse selectivity and decrease the C₂H₂ sorption.³⁵ Additionally, to enhance the stability of MOFs and solve the issue of the trade-off between CO₂ uptake and CO₂/C₂H₂ separation selectivity, inspired by pore functionality within MOFs, we propose the immobilization of the polar group strategy to target the one-step purification of C₂H₂ without an extra desorption process. Based on the difference of electric quadrupole between CO₂ and C₂H₂ molecules, we speculate that the methyl group (–CH₃)-functionalized pore channel could tune the pore environment to strengthen the recognition capability of guests and further enhance the CO₂–framework interaction and decrease the C₂H₂–framework interaction, i.e., the methyl-functionalized MOF could tailor the pore size to the optimal range and have moderate noncovalent van der Waals interactions with CO₂ molecules for sufficient CO₂ affinity. Moreover, the optimal pore size with functional sites could effectively address the trade-off of uptake and selectivity. At the same time, introduction of hydrophobic –CH₃ functional groups could enhance the chemical stability, especially water stability, of the framework, which may be a one-stone-two-bird strategy. In this regard, we successfully achieved the target of inverse CO₂ selection for the CO₂/C₂H₂ mixture via the construction of a methyl group-functionalized pore environment, based on pore chemistry and crystal engineering, to directly obtain high-purity C₂H₂. We chose Zn-ox-trz (ox, oxalate; trz, 1,2,4-triazole) as a prototype MOF, and the immobilization of the methyl group into the organic ligand not only changes the pore environment but also provides the binding affinity sites to enhance CO₂–MOF interactions. As expected, the methyl-functionalized Zn-ox-mtz (mtz, 3-methyl-1,2,4-triazole) exhibits the preferential adsorption of CO₂ over C₂H₂. Gas sorption measurements reveal that Zn-ox-mtz is an excellent CO₂-selective MOF material with a high CO₂/C₂H₂ uptake ratio of 12.6 and a selectivity of 1064.9 at ambient conditions, establishing a new benchmark material for reverse-selective CO₂/C₂H₂ separation, which is much higher than the prototype MOF with a larger pore. Zn-ox-mtz provides the optimal pore environment to accommodate CO₂, and CO₂ was captured into the pores through the robust host–guest interactions by the methyl groups from organic ligands, which is evidenced by molecular simulations. In addition, the column breakthrough experiments and simulations confirm the state-of-the-art CO₂/C₂H₂ separation performance with a benchmark C₂H₂ productivity of 2091 mmol kg^{–1}, and the cycling breakthrough experiments and sorption measurements

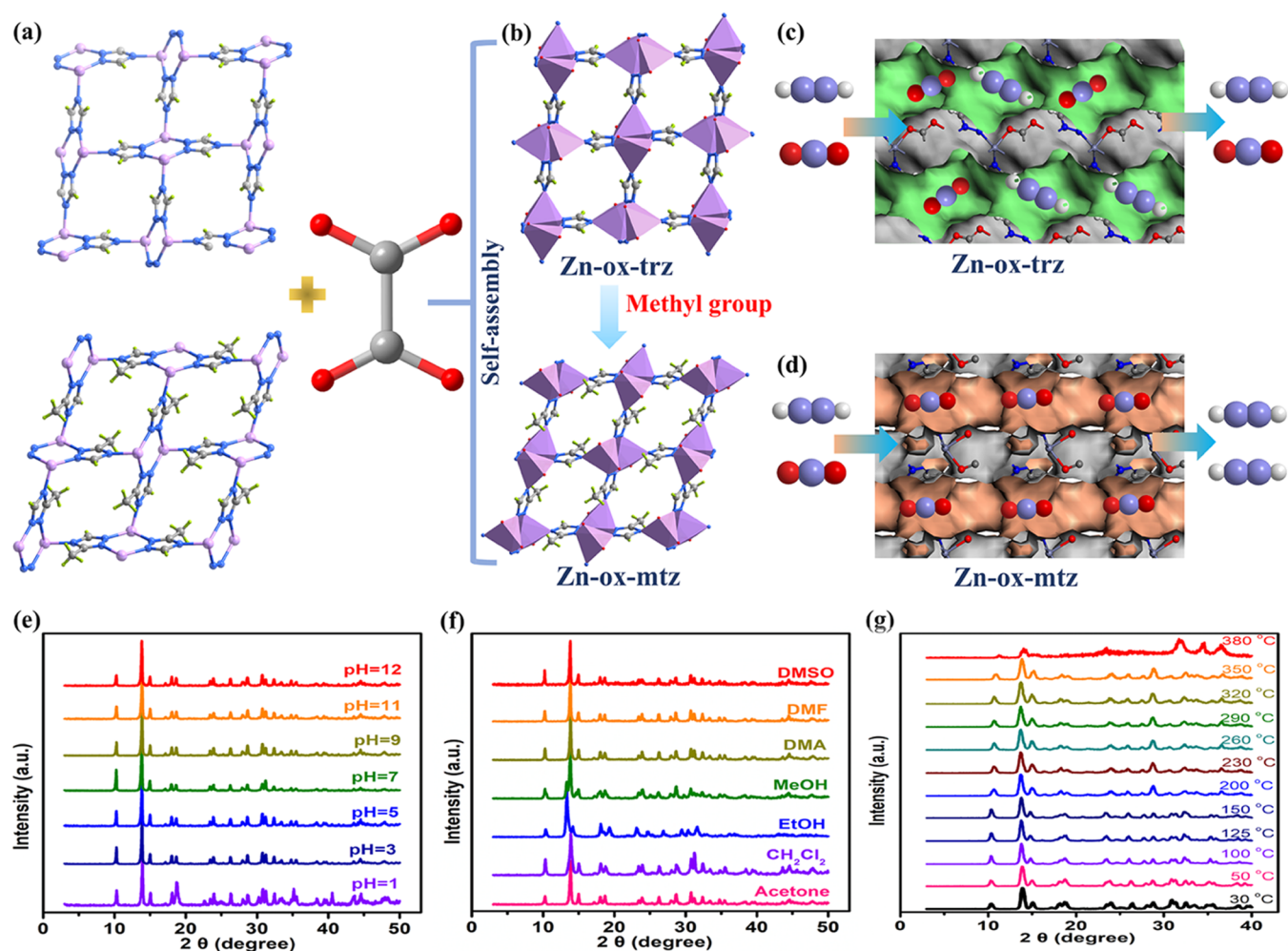


Figure 1. (a) View of the two-dimensional (2D) zinc triazolate layer and oxalate unit. (b) Three-dimensional pillared-layer frameworks along the *a* axis. (c) One-dimensional channel structure of Zn-ox-trz (the channels are expressed in green; Zn-ox-trz exhibits a low recognition for guest molecules: both CO₂ and C₂H₂ could pass through). (d) One-dimensional channel structure of Zn-ox-mtz (the channels are expressed in orange; the methyl-functionalized MOF could effectively improve the recognition of guest molecules: CO₂ molecules are trapped and the high-purity C₂H₂ stream could be straight obtained; Zn, lavender; C, light gray; N, blue; H, light green; O, red). PXRD patterns of Zn-ox-mtz samples: (e) soaking in different pH aqueous solvents for 14 days; (f) soaking in different organic solvents for 14 days. (g) In situ VT-PXRD from room temperature to 380 °C under an Ar atmosphere.

further prove the good recyclability and stability. These results make Zn-ox-mtz a benchmark adsorbent for high-efficiency CO₂/C₂H₂ separation, which is extremely sought-after in the industrial process yet has been scarcely reported. Moreover, the greatly stable framework of Zn-ox-mtz further showcases its promising practical application as a C₂H₂ splitter for industrial manufacture.

RESULTS AND DISCUSSION

Given the impact of pore sizes, environments, and physiochemical properties of the pore surface on the sorption behavior as well as the importance of MOFs with high stability, the tunable and stable Zn-ox-trz was selected as a prototype MOF material. To introduce bulky organic moieties for further adjusting the pore chemistry, the ligand with the methyl group was used to build an isorecticular framework affording Zn-ox-mtz. The Zn-ox-trz sample was easily synthesized by a solvothermal method in light of the previously reported method with some modifications.³³ High-quality single crystals of Zn-ox-mtz could be obtained through the reaction of 3-methyl-1*H*-1,2,4-triazole, oxalate, and ZnCO₃ in a butanol

solution at 453 K for 3 days. Single-crystal X-ray diffraction (SCXRD) revealed that Zn-ox-mtz crystallized in the *P21/c* space group, which is isostructural to Zn-ox-trz. As shown in Figure 1, in both MOFs, each Zn ion adopts a five-coordinated configuration with a distorted trigonal bipyramidal geometry, which is coordinated with three nitrogen atoms from tridentately bridging triazole units and two oxygen atoms from bidentately chelating oxalate units. Zn-ox-mtz is formed by the layers of CH₃-decorated 1,2,4-triazole-bridged Zn ions pillared in an out-of-plane form by the oxalate units to obtain a three-dimensional (3D) framework and a one-dimensional (1D) pore structure; the same is true of Zn-ox-trz, except for 1,2,4-triazole replacing the CH₃-decorated 1,2,4-triazole (Figure 1a,b). Especially, compared to Zn-ox-trz, Zn-ox-mtz possesses free methyl groups lining the pore channels, which decreases the pore apertures to 5.30 × 3.50 Å² from 5.20 × 5.70 Å². The insertion of the methyl group tailors the pore diameter to the optimal range for the adsorption of CO₂ molecules and provides potential binding sites. Thus, the methyl-functionalized MOF not only decreases the pore apertures but also facilitates the host–guest interactions in

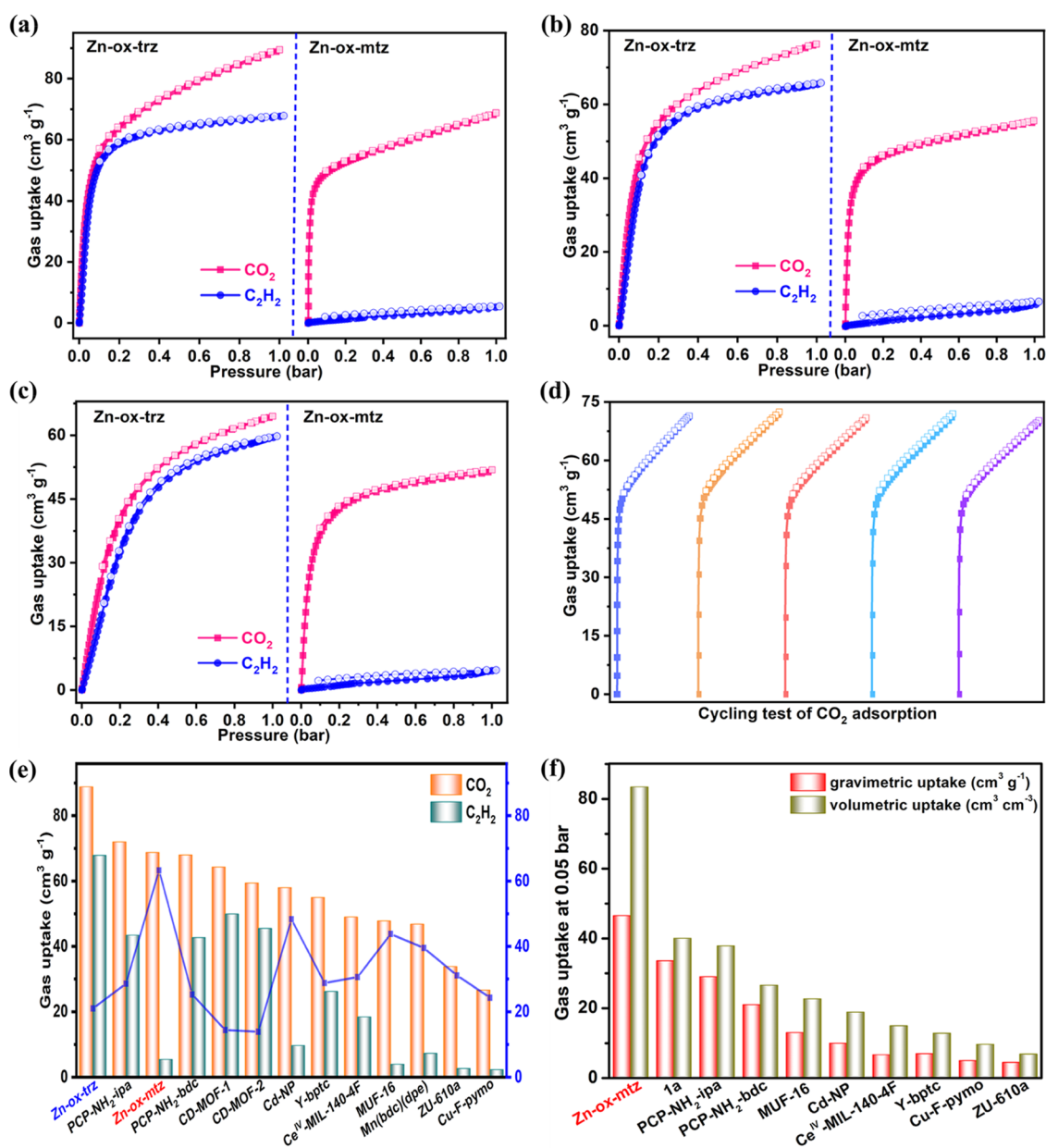


Figure 2. Gas sorption isotherms of Zn-ox-trz (left) and Zn-ox-mtz (right) (a) at 298 K, (b) at 313 K, and (c) at 333 K. (d) Cycling test of CO₂ sorption measurements on Zn-ox-mtz at 298 K from 0 to 1.0 bar. (e) Adsorption capacity of CO₂ and C₂H₂ for representative CO₂-selective adsorbents at 298 K and 1.0 bar (the blue line indicates the adsorption capacity difference between CO₂ and C₂H₂, i.e., blue line value = CO₂ uptake - C₂H₂ uptake). (f) Comparison of CO₂ uptake at 298 K and 0.05 bar among different CO₂-selective materials.

the compact space, which transfers the low recognition ability for guest gases to high recognition ability for adsorbed gases (Figure 1c,d). The bulk phase purity and crystallinity of Zn-ox-trz and Zn-ox-mtz were verified by powder X-ray diffraction (PXRD) (Figures S1 and S2). The surface morphologies of Zn-ox-trz and Zn-ox-mtz were analyzed by scanning electron microscopy (SEM), which indicated that these MOFs are sheet-like (Figures S13 and S14).

From the perspective of practical application, considering the industrial implementation is usually under humid or acidic conditions, the adsorbent materials should possess high water and chemical stabilities. Thus, the chemical stability of Zn-ox-mtz toward acid, water, base solutions, and organic solvents was examined. As shown in Figure 1e,f, Zn-ox-mtz exhibits structural stability of aqueous solutions with different pH

values (pH = 1–12) and different organic solvents for 14 days, which confirmed its highly robust nature for practical implementation under harsh conditions. In addition, the thermal stability of Zn-ox-mtz was also investigated by thermogravimetric analysis (TGA) and in situ variable-temperature powder X-ray diffraction (VT-PXRD); the results of TGA and VT-PXRD indicated that Zn-ox-mtz was thermally stable until 600 K (Figures 1g and S15). Obviously, Zn-ox-mtz exhibits excellent thermal and chemical stability. The ultramicroporous framework and high stability make the methyl-functionalized Zn-ox-mtz an ideal platform for gas separation implementations.

Before evaluating the permanent porosity, the activated samples for two Zn-MOFs could be directly obtained at 373 K for 12 h under a high vacuum. The pore features of the

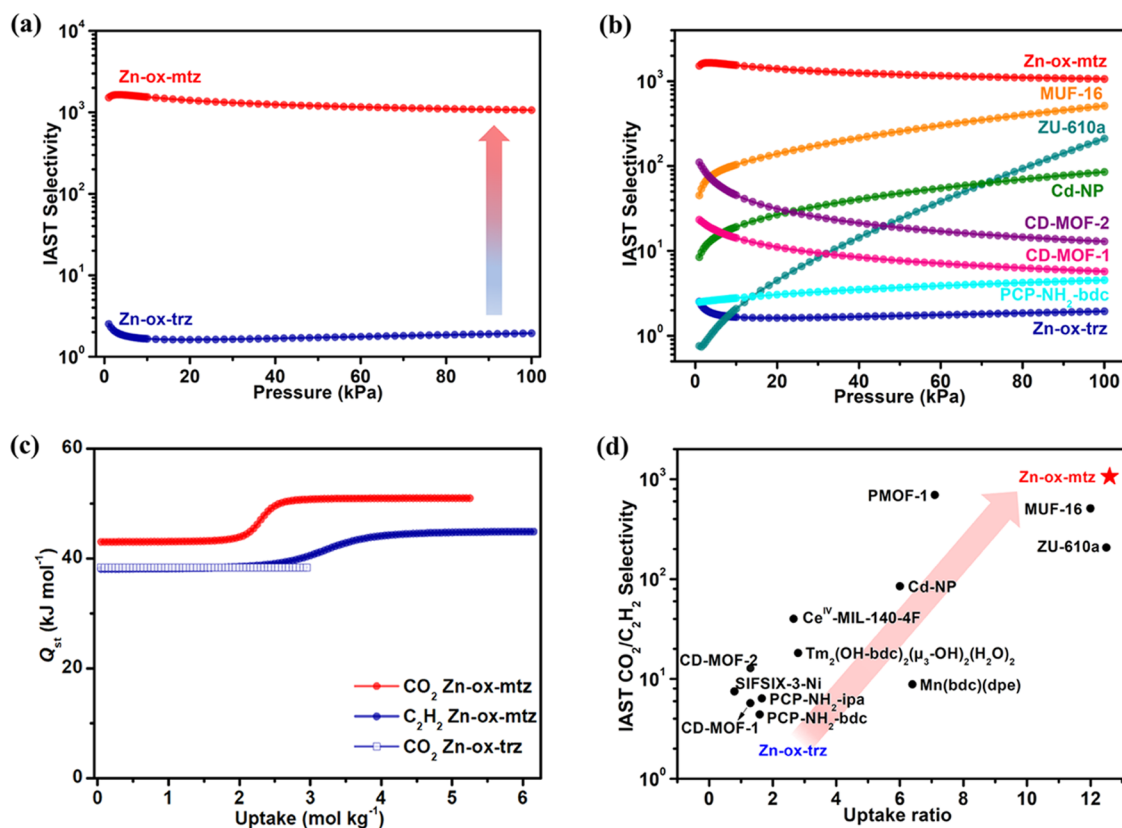


Figure 3. (a) Predicted IAST selectivity curves for an equimolar CO₂/C₂H₂ mixture at 298 K. (b) Comparison of equimolar CO₂/C₂H₂ mixture separation selectivity at 298 K. (c) Isothermic heat of adsorption for Zn-ox-trz and Zn-ox-mtz. (d) Comparison of the CO₂/C₂H₂ uptake ratio and equimolar CO₂/C₂H₂ selectivity with popular CO₂-selective adsorbents at 298 K and 1.0 bar.

activated Zn-MOFs were obtained through CO₂ sorption experiments at 195 K. It could be seen from Figures S3 and S4 that these MOF materials exhibit a completely reversible type I sorption behavior. The saturated CO₂ adsorption capacity of Zn-ox-mtz is 100.16 cm³ g⁻¹, which is lower than that of Zn-ox-trz (132.65 cm³ g⁻¹) owing to the introduction of the -CH₃ group. The Brunauer–Emmett–Teller surface area of Zn-ox-mtz is decreased from 466 m² g⁻¹ in Zn-ox-trz to 344 m² g⁻¹ according to the CO₂ adsorption isotherm (Figures S5 and S6). Additionally, the pore volume calculated on the basis of the saturated CO₂ uptake also decreased from 0.28 cm³ g⁻¹ in Zn-ox-trz to 0.21 cm³ g⁻¹.

Considering the interesting pore chemistry as well as the suitable pore size, the single-component gas sorption isotherms of CO₂ and C₂H₂ for Zn-ox-trz and Zn-ox-mtz were measured at 298, 313, and 333 K in the pressure range of 0.0–1.0 bar, respectively. As shown in Figure 2a–c, although both Zn-ox-trz and Zn-ox-mtz show an inverse CO₂-selective adsorption behavior, they exhibited an apparent difference in the sorption performance for C₂H₂ and CO₂. The CO₂ adsorption capacity of Zn-ox-mtz is 68.78 cm³ g⁻¹ (3.07 mmol g⁻¹) at 298 K and 1.0 bar, which is slightly lower than that of Zn-ox-trz (89.49 cm³ g⁻¹ or ~4.0 mmol g⁻¹). More significantly, Zn-ox-mtz exhibits a negligible C₂H₂ uptake with 5.46 cm³ g⁻¹ (0.24 mmol g⁻¹), which is much lower than that of Zn-ox-trz with 67.85 cm³ g⁻¹ (3.03 mmol g⁻¹). Such an obvious adsorption difference on Zn-ox-mtz gives rise to a high CO₂/C₂H₂ uptake ratio with the value of 12.6, which is 9.5 times higher than that of Zn-ox-trz, establishing a new benchmark for CO₂-selective MOFs for CO₂/C₂H₂ separation under ambient conditions

(Figure 2e). We further notice that the gravimetric CO₂ uptake of Zn-ox-mtz at ambient conditions is higher than or comparable to those of most benchmark CO₂-selective MOFs such as Cd-NP (58.0 cm³ g⁻¹),³⁵ Ce^{IV}-MIL-140-4F (48.9 cm³ g⁻¹),³⁶ Cu-F-pymo (26.6 cm³ g⁻¹),³¹ MUF-16 (47.8 cm³ g⁻¹),³⁷ ZU-610a (33.8 cm³ g⁻¹),³⁸ and PCP-NH₂-bdc (68 cm³ g⁻¹).³⁹ Specially, the volumetric storage capacity is also a key parameter to evaluate the actual separation process, which could take full advantage of the packed-bed space and decrease the energy consumption of the regeneration process. In terms of volumetric storage capacity, Zn-ox-mtz exhibits a remarkable volumetric adsorption capacity for CO₂ with 123.32 cm³; such a high volumetric uptake is significantly higher than that of CO₂-selective adsorbents, including but not limited to MUF-16 (74.7 cm³ cm⁻³),³⁷ Ce^{IV}-MIL-140-4F (110.3 cm³ cm⁻³),³⁶ SIFSIX-3-Ni (98.4 cm³ cm⁻³),⁷ CD-MOFs (60.4 cm³ cm⁻³),³² and PCP-NH₂-ipa (93.6 cm³ cm⁻³).³⁹ Obviously, Zn-ox-mtz displays an excellent trade-off between the gravimetric and volumetric adsorption capacities, which is a key scientific problem and of industrial relevance. In addition, to the best of our knowledge, the excellent uptake ratio is superior to all of those reported benchmark CO₂-selective porous adsorbents such as Cd-NP (6.0),³⁵ Ce(IV)-MIL-140-4F (2.65),³⁶ PCP-NH₂-bdc (1.59) and PCP-NH₂-ipa (1.6),³⁹ PMOF-1 (7.1),⁴⁰ and een-MOF (2.64)⁴¹ (Table S4, Supporting Information). Significantly, unlike most CO₂-selective adsorbent materials that present limited CO₂ uptake in the low-pressure region, the CO₂ uptake on Zn-ox-mtz increases sharply. At 298 K and 0.05 bar, the CO₂ uptake reaches 46.54 cm³ g⁻¹ (2.08 mmol g⁻¹), which is

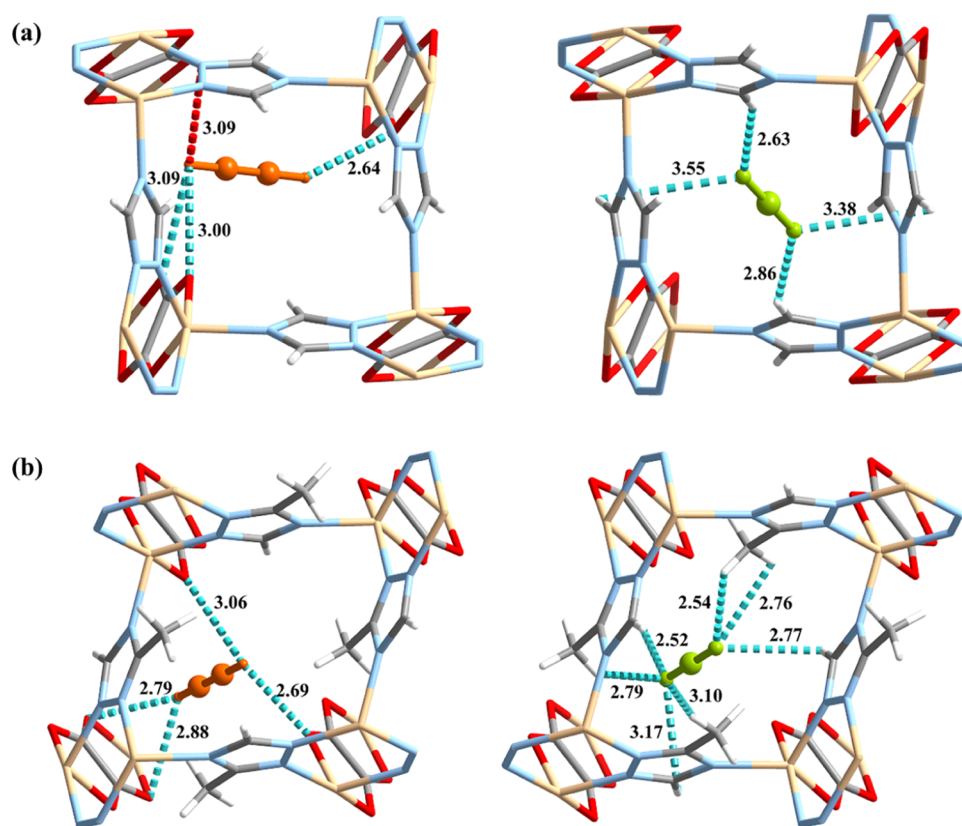


Figure 4. Adsorption binding sites in (a) Zn-ox-trz for C_2H_2 (left) and CO_2 (right), (b) C_2H_2 (left) and CO_2 (right) molecule binding sites in Zn-ox-mtz by theoretical calculations. Distances are given in Å.

apparently higher than those of PCP-NH₂-bdc (21 cm³ g⁻¹)³⁹ and MUF-16 (13 cm³ g⁻¹).³⁷ To the best of our knowledge, this uptake level is the highest among all reported CO₂-selective MOF materials (Figure 2f). Such an excellent gas adsorption capacity could endow Zn-ox-mtz with a prominent capacity to capture trace amounts of CO₂ contaminants, which is vital in industrial implementation. Continuous CO₂ sorption experiments on Zn-ox-mtz were performed to assess its cycling stability. After five cycles, Zn-ox-mtz showed no obvious reduction in its CO₂ uptake (Figure 2d).

To evaluate the separation potential of Zn-ox-trz and Zn-ox-mtz for the CO₂/C₂H₂ mixture, the ideal adsorbed solution theory (IAST) was used to assess the adsorptive selectivity toward the equimolar CO₂/C₂H₂ mixture. As shown in Figure 3a, Zn-ox-trz exhibits a low CO₂/C₂H₂ selectivity of 1.9 at 298 K and 1.0 bar owing to the very similar adsorption isotherms of CO₂ and C₂H₂. After the insertion of the -CH₃ group into the structure, Zn-ox-mtz exhibits a dramatically enhanced CO₂/C₂H₂ selectivity of 1064.9, which is 560 times higher than that of Zn-ox-trz. This selectivity value under the same conditions is greatly higher than that of the most reported CO₂-selective materials such as MUF-16 (510),³⁷ SIFSIX-3-Ni (7.5),⁷ [Tm₂(OH-bdc)₂(μ₃-OH)₂(H₂O)₂](18.2),⁴² Cd-NP (85),³⁵ and PCP-NH₂-ipa (6.4)³⁹ (Figure 3b). It is worth noting that the calculated CO₂/C₂H₂ separation selectivity serves as a qualitative description of the mixture separation capacity, but it is only for qualitative comparison. In addition, the coverage-dependent isosteric heats of adsorption (Q_{st}), which quantitatively evaluates the interactions between adsorbed gas and the framework, for CO₂ on Zn-ox-mtz was calculated to be 43.02 kJ mol⁻¹ at near-zero coverage (Figure 3c). The Q_{st}

values of Zn-ox-trz for CO₂ and C₂H₂ are 38.09 and 38.39 kJ mol⁻¹, respectively, which is in good agreement with the sorption isotherms. In addition, compared to Zn-ox-trz, the higher heat of adsorption of CO₂ for Zn-ox-mtz indicates a higher binding affinity, which can be seen in the adsorption isotherm in the low-pressure region (Figure S17). The adsorption and separation properties are further evaluated in multiple dimensions including CO₂/C₂H₂ selectivity, CO₂/C₂H₂ uptake ratio, and CO₂ uptake; Zn-ox-mtz exhibits excellent performance among these evaluation criteria (Figures S18 and S19). We realize that the combination of high adsorption capacity and good selectivity is still rare in MOF adsorbents, and previously reported CO₂-selective MOFs generally display either low capacity or poor selectivity.^{7,31,32,38,39,43,44} With adsorption capacity and selectivity as parallel goals, Zn-ox-mtz shows the best trade-off between them, establishing a new benchmark for reverse CO₂/C₂H₂ adsorption (Figure 3d). By virtue of the outstanding CO₂ adsorption capacity, moderate isosteric heats of adsorption, benchmark uptake ratio, and high inverse selectivity, Zn-ox-mtz could be the most promising porous adsorbent for the direct one-step purification of C₂H₂ from the CO₂/C₂H₂ mixture.

To gain a profound understanding on the effect of the incorporation of the methyl group on the pore chemistry and the origin of markedly enhanced gas selectivity, grand canonical Monte Carlo (GCMC) simulations on Zn-ox-trz and Zn-ox-mtz were carried out to investigate the host-guest interactions between the framework and the adsorbed gas molecules. As outlined in Figure 4a, in Zn-ox-trz, each C₂H₂ molecule interacts with three oxygen atoms from two oxalate

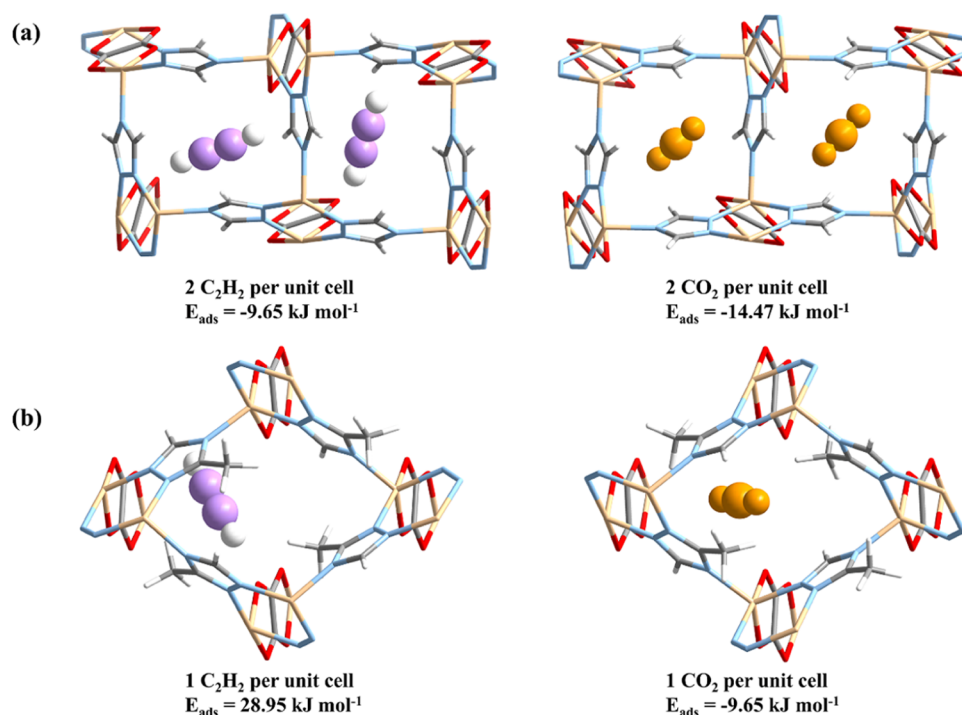


Figure 5. Adsorption energies of (a) C₂H₂ (left) and CO₂ (right) in Zn-ox-trz and (b) C₂H₂ (left) and CO₂ (right) in Zn-ox-mtz by density functional theory calculations.

ligands to form three C–H···O interactions (H–O, 2.64–3.09 Å) and one nitrogen atom from the triazole ligand to form one C–H···N interaction (H–N, 3.09 Å), and each CO₂ molecule interacts with four triazole ligands to form four C–H···O interactions (H–O, 2.63–3.55 Å). Thus, the similar host–guest interactions result in a close adsorption behavior and low separation potential. After methyl group functionalization, the pore environment becomes compact; in addition, the free methyl groups lining the pore channels provide binding bites for CO₂ molecules. As shown in Figure 4b, the C₂H₂ molecule adsorbed in Zn-ox-mtz interacts only with three oxalates and four oxygen atoms to form four C–H···O interactions (H–O, 2.69–3.06 Å), while the CO₂ molecule interacts not only with three hydrogens of the triazole to form three C–H···O interactions (H–O, 2.52, 2.77, and 3.17 Å) but also with three –CH₃ groups to form four C–H···O interactions (H–O, 2.54, 2.76, 2.79, and 3.10 Å). From another point of view, to clearly explain the reason for the decrease in C₂H₂ uptake in Zn-ox-mtz, we further mapped the ESP of gas molecules and pore surfaces of MOFs using density functional theory (DFT) calculations (Figure S7). As shown in Figure S7a,b, it is obvious that CO₂ and C₂H₂ possess opposite electrostatic potentials. In the prototype and methyl-functionalized MOFs, the positive potential is found on the hydrogen atom in the ligands and near the Zn center, respectively, as well as a negative potential is found near the oxygen and nitrogen atoms of the ligands (Figure S7c,d). Compared to prototype MOF, methyl-functionalized MOF exhibits a much positively charged pore surface owing to more hydrogen atoms of methyl groups lining the pore channel. In the prototype MOF, Zn-ox-trz has a wide open pore space, where both C₂H₂ and CO₂ could achieve their own optimal adsorption configurations in different orientations. After methyl insertion, the pore space becomes more compact and more hydrogen lines the channel, forming the positively charged pore environment. The

dimensions of the Zn-ox-mtz pores are well matched to CO₂ molecule sizes, which allows the CO₂ molecules to be encompassed by multiple noncovalent contacts, and these contacts support the CO₂-selective adsorption behavior since the electrostatic potential of CO₂ is complementary to the methyl-functionalized pore surface potential (Figure S7a,d). However, C₂H₂ is polarized oppositely to CO₂ and it is electrostatically repelled by the methyl groups in Zn-ox-mtz (Figure S7b,d). In short, compared to the prototype MOF, ultramicroporous characteristics featuring a compact pore space and positive charge distribution at the pore wall of Zn-ox-mtz could significantly decrease the C₂H₂ adsorption capacity and maximize the inverse CO₂/C₂H₂ selectivity. Evidently, the immobilization of –CH₃ groups allows the framework to bind more strongly with CO₂ compared with C₂H₂ within the pore channel, thus leading to the significant adsorption performance difference between CO₂ and C₂H₂.

Density functional theory calculations were performed to further access the adsorption energy of guest molecules (C₂H₂ and CO₂) in prototype Zn-ox-trz and methyl-functionalized Zn-ox-mtz (the detailed calculations are demonstrated in the Supporting Information). According to the defined formula, the more negative the adsorption energy value, the stronger the binding affinity is on the same adsorbent. Considering the adsorbed molecule quantity in one unit cell from an experimental perspective, the calculated averages of the adsorption energy of C₂H₂ and CO₂ on Zn-ox-trz are –9.65 and –14.47 kJ mol⁻¹ (Figure 5a), respectively, indicating a stronger binding affinity to CO₂ over C₂H₂, which is in good agreement with the adsorption behaviors. In the –CH₃-functionalized Zn-ox-mtz, the calculated adsorption energies of C₂H₂ and CO₂ are 28.95 and –9.65 kJ mol⁻¹ (Figure 5b), respectively, and this result suggests that the binding affinity between the framework and C₂H₂ is very weak and there is a stronger host–guest interaction between CO₂ and the

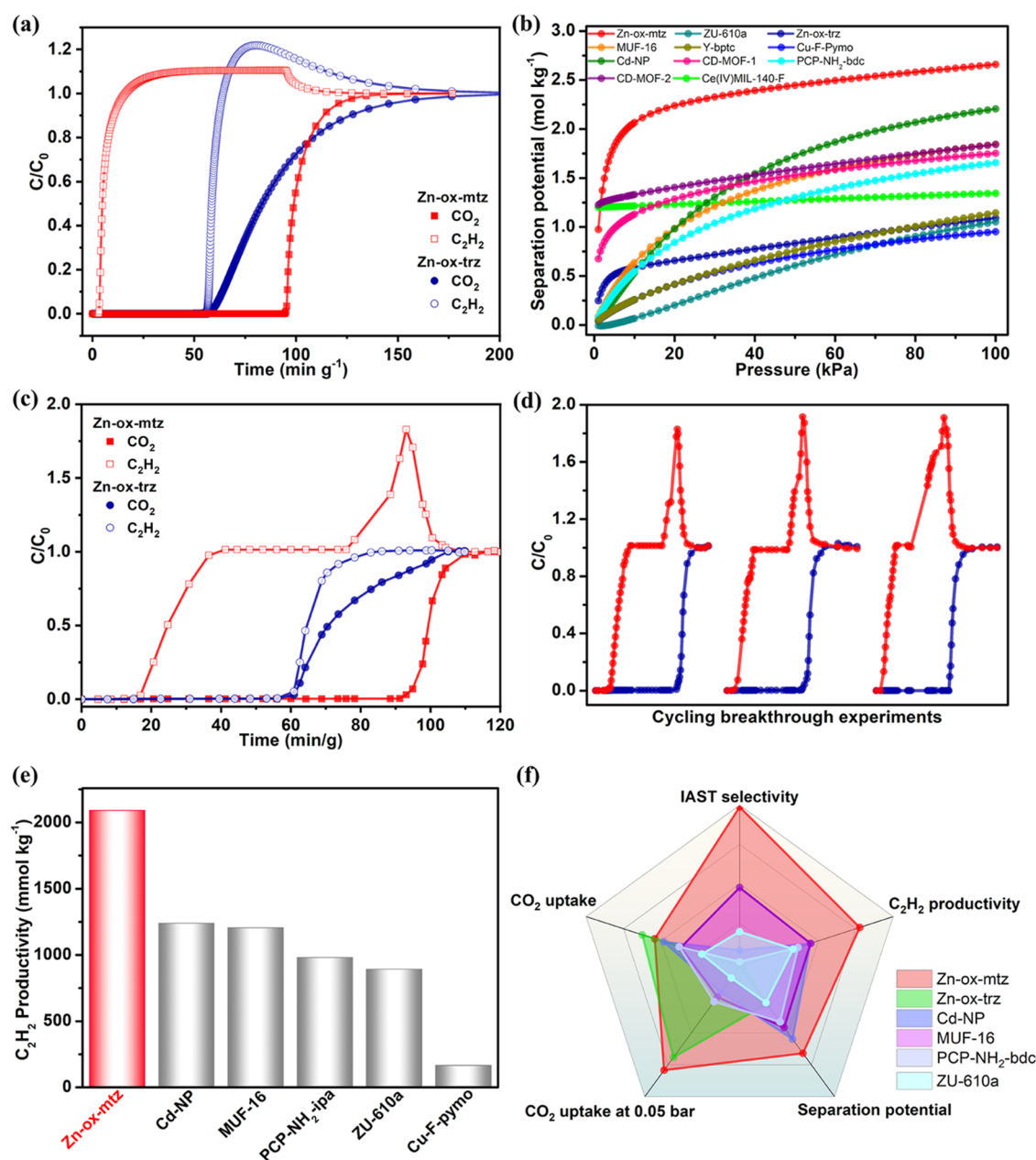


Figure 6. (a) Simulated breakthrough curves for an equimolar CO₂/C₂H₂ mixture in the fixed bed packed with Zn-ox-trz and Zn-ox-mtz at 298 K and 1.0 bar. (b) Separation potential of the selected MOF materials for the equimolar CO₂/C₂H₂ mixture. (c) Experimental column breakthrough curves for the equimolar CO₂/C₂H₂ mixture on Zn-ox-trz and Zn-ox-mtz at 298 K and 1.0 bar. (d) Cycling tests of the equimolar CO₂/C₂H₂ mixture on Zn-ox-mtz at 298 K and 1.0 bar. (e) Comparison of C₂H₂ productivity with the reported benchmark porous materials at ambient conditions. (f) Comparison of the comprehensive separation performance with reported excellent reverse CO₂-selective MOFs.

skeleton. This could be attributed to the suitable binding sites for CO₂ and the strong recognition capacity for the CO₂/C₂H₂ mixture, provided by the -CH₃-functionalized framework. The different adsorption energy behaviors on Zn-ox-trz and Zn-ox-mtz indicate the profound effect of immobilization of the -CH₃ group on CO₂ and C₂H₂ adsorption performance.

To effectively validate the positive impact of methyl groups on CO₂/C₂H₂ separation, transient breakthrough simulations for an equimolar CO₂/C₂H₂ mixture on Zn-ox-trz and Zn-ox-mtz in a fixed bed were carried out at 298 K and 1.0 bar (Figure 6a). The methodology used in the transient breakthrough simulations is the same as described by Krishna.^{45,46} A summary of the methodology is also included in the Supporting Information. The results displayed that Zn-ox-trz

presented weak CO₂/C₂H₂ separation capacity and Zn-ox-mtz accomplished highly efficient separation. The separation potential, as a combined metric for adsorption capacity and selectivity,^{47,48} was performed to qualitatively prove their separation performances. As shown in Figure 6b, the amounts of pure C₂H₂ that could be recovered by Zn-ox-mtz reached up to 2.66 mol kg⁻¹ for the equimolar CO₂/C₂H₂ mixture, greatly surpassing the performance of other selected reverse adsorbents. Next, to further access the practical CO₂/C₂H₂ separation capacity of Zn-ox-mtz, dynamic column breakthrough experiments were performed, where the equimolar CO₂/C₂H₂ gas mixture flowed over the Zn-ox-trz and Zn-ox-mtz packed column at the mass flow rate of 2 mL min⁻¹ under ambient conditions. Because of the low CO₂/C₂H₂ separation

performance, Zn-ox-trz could not remove CO₂ from the equimolar CO₂/C₂H₂ binary mixture to produce polymer-grade C₂H₂ in the effluent stream (Figure 6c). In contrast, a clean separation of the CO₂/C₂H₂ mixture was presented with a great separation window, and an outstanding direct one-step purification of C₂H₂ could be achieved with the Zn-ox-mtz. The breakthrough interval time between CO₂ and C₂H₂ is approx. 78 min g⁻¹, which exceeds that of top-performing adsorbents such as Cd-NP (15 min g⁻¹)³⁵ and ZU-610a (28 min g⁻¹) under the same conditions.³⁸ The C₂H₂ gas was first eluted with high purity (>99.6%) from the packed column on Zn-ox-mtz, giving a highly excellent C₂H₂ productivity of 2091 mmol kg⁻¹ of the adsorbent material. The C₂H₂ productivity of Zn-ox-mtz is state-of-the-art in the CO₂-selective materials, much higher than that on benchmark MOFs Cu-F-pymo (166 mmol kg⁻¹),³¹ PCP-NH₂-ipa (980 mmol kg⁻¹),³⁹ and Cd-NP (1240 mmol kg⁻¹)³⁵ (Figure 6e). CO₂ gas was trapped as an impurity in the packed column for a long time with dynamic adsorption amounts of 119 cm³ cm⁻³, which was in accordance with the CO₂ sorption isotherms; in addition, this dynamic capacity of CO₂ is higher than the previously reported excellent inverse selective materials such as Cd-NP (38 cm³ cm⁻³)³⁵ and ZJU-610a (43 cm³ cm⁻³).³⁸ As a result, Zn-ox-mtz exhibits a high separation factor for an equimolar CO₂/C₂H₂ mixture with the value of 6.28 at ambient conditions, which was calculated from breakthrough experiments and reflects the actual separation performance. This separation factor value is higher than or comparable to those of Ce(IV)-MIL-140-4F (4.9),³⁶ NH₄-IM (4.6), and NH₄-MM (6.5).⁴⁹ Furthermore, multiple equimolar CO₂/C₂H₂ gas mixture breakthrough experiments were carried out, which indicates that Zn-ox-mtz could maintain a good CO₂ retention time and C₂H₂ productivity (Figure 6d), suggesting its good recyclability for this challenging CO₂/C₂H₂ separation.

For industrial implementations of CO₂/C₂H₂ separation, the ideal CO₂-selective adsorbent material should display several properties, including (i) high CO₂ uptake capacity, (ii) good CO₂/C₂H₂ selectivity, (iii) excellent thermal and chemical stability, (iv) high C₂H₂ productivity, (v) high uptake in a low-pressure region, and (vi) moderate isosteric heats of adsorption. We have shown that Zn-ox-mtz could meet all of these criteria, while other CO₂-selective MOFs have better presented one or more of the properties mentioned above. In point-of-separation performance, Zn-ox-mtz exhibits the record C₂H₂ productivity with 2091 mmol kg⁻¹ among other state-of-the-art MOFs, establishing a new benchmark for inverse CO₂-selective MOFs. In addition, Zn-ox-mtz displays excellent CO₂ uptake and CO₂/C₂H₂ selectivity, especially its CO₂ uptake in the low-pressure area is superior to current excellent inverse CO₂-selective materials (Table S4). Poor chemical stability, especially water stability, of MOFs is still a drawback for their practical application. In this regard, the immobilization of the methyl group could dramatically improve the hydrophobicity, and Zn-ox-mtz shows good chemical stability toward water, acid, and base. In comprehensive consideration of the CO₂ adsorption capacity, CO₂ uptake in a low-pressure area, CO₂/C₂H₂ selectivity, C₂H₂ productivity, separation potential, and framework stability, Zn-ox-mtz displays the best one-step separation performance for the CO₂/C₂H₂ mixture compared to that of the reported inverse CO₂-selective adsorbents in references (Figure 6f). These advances enable Zn-ox-mtz to become one ideal adsorbent for challenging CO₂/C₂H₂ separation.

CONCLUSIONS

In summary, we propose a feasible approach to explore CO₂-selective MOF materials for a superior separation strategy to advance C₂H₂ production. By virtue of pore chemistry and crystal engineering, we dexterously achieved efficient inverse CO₂/C₂H₂ adsorption and separation via the immobilization of a methyl group into the prototype MOF. This specific capture of CO₂ over C₂H₂ is mainly attributed to methyl-functionalized Zn-ox-mtz, which provides high recognition of CO₂ molecules through multiple van der Waals interactions, thus establishing the benchmark inverse CO₂/C₂H₂ separation and record C₂H₂ production. As evidenced by sorption measurements, theoretical calculations, and breakthrough experiments, high-purity C₂H₂ could be directly harvested from the CO₂/C₂H₂ mixture via a single adsorption process with a high production of 2091 mmol kg⁻¹. Together with cheap precursors, high framework stability, and excellent separation capacity, Zn-ox-mtz would be a promising candidate adsorbent for the CO₂/C₂H₂ separation process. This study elaborates on the effectiveness of optimized pore environments through introduction of polar groups within MOFs, which will open more opportunities to develop advanced porous solid materials with dramatic separation performance and inspire the construction of MOFs aimed at the separation process with similar physical properties in an adsorptive separation field.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/jacs.3c03265>.

Full experimental details, including material synthesis, crystal data, PXRD patterns, TGA curves, SEM images, CO₂ sorption data, grand canonical Monte Carlo simulations, density functional theory calculations, breakthrough experiments, transient breakthrough simulations, and comparison of CO₂-selective adsorbents (PDF)

Accession Codes

CCDC 2248518 contains the supplementary crystallographic data for this paper. These data can be obtained free of charge via www.ccdc.cam.ac.uk/data_request/cif, or by emailing data_request@ccdc.cam.ac.uk, or by contacting The Cambridge Crystallographic Data Centre, 12 Union Road, Cambridge CB2 1EZ, UK; fax: +44 1223 336033.

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Notes

The authors declare no competing financial interest.

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Immobilization of Polar Group into an Ultramicroporous Metal-Organic Framework Enabling Benchmark Inverse Selective CO₂/C₂H₂ Separation with Record C₂H₂ Production

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Experimental section

Materials and Methods

All raw reagents and chemicals were purchased from commercial providers and used directly without further purification.

The powder X-ray diffraction (PXRD) patterns were collected on the Rigaku Miniflex 600 at 40 kV and 15 mA with a scan rate of $5.0^\circ \text{ min}^{-1}$ using Cu K α ($\lambda = 1.5418 \text{ \AA}$) radiation in the air atmosphere, scanning the 2θ range of $3\text{-}50^\circ$ with a step size of 0.02° . The thermogravimetric analysis (TGA) was performed on a Rigaku standard thermogravimetry-differential thermal analysis (TG-DTA) analyzer from room temperature to 800°C under Argon atmosphere with a heating rate of $10^\circ\text{C min}^{-1}$, using an empty and clean Al_2O_3 crucible as a reference. In situ variable temperature PXRD (VT-PXRD) patterns were also collected on a Rigaku Miniflex 600 at 40 kV and 15 mA with a scan rate of $8.0^\circ \text{ min}^{-1}$ using Cu K α ($\lambda = 1.5418 \text{ \AA}$) radiation in the air atmosphere, scanning the 2θ range of $3\text{-}40^\circ$ with a step size of 0.02° .

Synthesis of Zn-ox-trz and Zn-ox-mtz

Synthesis of Zn-ox-mtz ($\text{Zn}_2(\text{ox})(\text{mtz})_2 \cdot 2\text{H}_2\text{O}$). A mixture of ZnCO_3 (0.125 g), oxalic acid (0.09 g), 3-methyl-1H-1,2,4-triazole (0.415 g), H_2O (4 mL) and BuOH (2 mL) was placed in a 20 ml Teflon autoclave, which was stirred for 30 minutes at room temperature and then was heated in a convection oven at 180°C for 3 days.

Synthesis of Zn-ox-trz. Zn-ox-trz was prepared according to the previously reported method with some modifications.¹ The mixture of zinc oxalate (0.66 g) 1,2,4-triazole (0.5 g) was added into 6.6 mL methanol in a 20 mL Teflon autoclave, which was stirred

for 30 minutes at room temperature and then was heated in a convection oven at 180 °C for 2 days.

Single crystal X-ray diffraction analysis

The single crystal X-ray diffraction data of **Zn-ox-mtz** were collected at 100 K, via Rigaku XtaLAB Pro MM007HF DW diffractometer with Cu-K α radiation ($2\lambda = 1.54184 \text{ \AA}$). The structure was solved and refined using Olex2 software with the SHELXT and SHELXL program, respectively. The crystal details are listed in Table S3, and the crystallographic data of **Zn-ox-mtz** can be obtained freely from the Cambridge Crystallographic Data Centre (CCDC: 2248518).

Gas sorption measurements

CO₂ and C₂H₂ sorption isotherms were collected on the BSD-PM2 instrument. N₂ (99.9999%), C₂H₂ (99.9%), CO₂ (99.99%), He (99.999%) were purchased from Liquid Air (China). Prior to the gas sorption analysis, the samples were washed with methanol several times and activated under dynamic vacuum overnight at 100 °C. The precise control of 298, 313, and 333 K were implemented by the BSD 3H-2000 of Beishide Instrument Technology, which contains a cycle system of water. The sample was degassed at 60 °C under high vacuum for 1 h to regenerate at every interval of two independent sorption isotherms.

Fitting of experimental data on pure component isotherms

The unary isotherm data for CO₂, measured at three different temperatures 298 K, 313 K, and 333 K in Zn-ox-trz and **Zn-ox-mtz** were fitted with excellent accuracy using the dual-site Langmuir model, where we distinguish two distinct adsorption sites A and B:

$$q = \frac{q_{sat,A} b_A p}{1 + b_A p} + \frac{q_{sat,B} b_B p}{1 + b_B p} \quad (S1)$$

In eq (S1), the Langmuir parameters b_A, b_B are both temperatures dependent.

$$b_A = b_{A0} \exp\left(\frac{E_A}{RT}\right); \quad b_b = b_{B0} \exp\left(\frac{E_B}{RT}\right) \quad (S2)$$

In eq (S2), E_A, E_B are the energy parameters associated with sites A, and B, respectively.

The fit parameters are provided in Table S1 for the two MOFs.

The unary isotherm data for C₂H₂, measured at three different temperatures 298 K, 313 K, and 333 K in Zn-ox-trz and **Zn-ox-mtz**, could be fitted with the 1-site Langmuir-Freundlich model:

$$q = \frac{q_{sat} b p^v}{1 + b p^v} \quad (S3)$$

In eq (S3), the Langmuir-Freundlich parameter b is temperature dependent.

$$b = b_0 \exp\left(\frac{E}{RT}\right) \quad (S4)$$

In eq (S4), E is the energy parameter. The fit parameters are provided in

Table S2 for the two MOFs.

Isosteric heat of adsorption

The isosteric heat of adsorption, Q_{st} , is defined as

$$Q_{st} = -RT^2 \left(\frac{\partial \ln p}{\partial T} \right)_q \quad (S5)$$

where the derivative in the right member of eq (S5) is determined at constant adsorbate loading, q . The derivative was determined by analytic differentiation of the combination

of eq (S1), eq (S2), and eq (S5) for the dual-site Langmuir fits. For the 1-site Langmuir-Freundlich fits, the isosteric heat of adsorption, Q_{st} , was determined by analytic differentiation of the combination of eq (S3), eq (S4), and eq (S5).

IAST calculations

For screening MOFs for separation of binary mixtures of components 1 and 2, the adsorption selectivity, S_{ads} , is defined by

$$S_{ads} = \frac{q_1/q_2}{y_{10}/y_{20}} \quad (S6)$$

In eq (S6), y_{10}, y_{20} are the mole fractions of the bulk gas phase mixture.

The 50/50 CO₂ (1)/C₂H₂ (2) mixture separations are envisaged to be carried out in fixed bed adsorbers. In such devices, the separations are dictated by a combination of adsorption selectivity and uptake capacity. Using the shock wave model for fixed bed adsorbers, Krishna²⁻³ has suggested that the appropriate metric is the separation potential, Δq . The appropriate expression describing the productivity of pure C₂H₂ in the adsorption phase of fixed-bed operations is

$$\Delta q = q_1 \frac{y_{20}}{y_{10}} - q_2 \quad (S7)$$

In eq (S7) $y_{10} = y_{20} = 0.5$ is the mole fractions of the feed mixture during the adsorption cycle. In the derivation of eq (S7), it is assumed that the concentration “fronts” traversed the column in the form of shock waves during the desorption cycle. The molar loadings q_1, q_2 of the two components are determined using the Ideal Adsorbed Solution Theory (IAST) of Myers and Prausnitz using the unary isotherm fits

as data inputs.⁴ The physical significance of Δq_i is the maximum productivity of pure C₂H₂ that is achievable in PSA operations.

Grand canonical Monte Carlo simulations

The GCMC simulations were carried out for the adsorption of C₂H₂ and CO₂ in Zn-MOFs using Sorption Tools in Materials Studio package. The skeleton of Zn-MOFs and gas molecules were regarded as rigid bodies. The optimal adsorption sites were simulated under 298 K and 1.0 bar by the fixed loading task and Metropolis method. The atomic partial charges of the host skeleton of Zn-MOFs and all gas molecules were obtained from QEq method. The equilibration steps and the production steps were set to 5.0×10^6 and 1.0×10^7 , respectively. The gas-skeleton interaction and the gas-gas interaction were characterized by the standard universal force field (UFF). The cut-off radius used for the Lennard-Jones interactions is 15.5 Å and the long-range electrostatic interactions were considered by the Ewald summation method.

Density-functional theory calculations

All density functional theory (DFT) calculations were performed using the Vienna Ab initio Simulation Package (VASP)^{5,6} at the level of generalized gradient approximation (GGA) using Perdew-Burke-Ernzerhof (PBE) exchange-correlation functional.⁷ Projector-augmented wave (PAW) potentials were used to describe the effective cores.^{8,9} The valence electrons of all atoms were expanded in a plane wave basis set with a cutoff energy of 400 eV. The atomic structures were relaxed using either the conjugate gradient algorithm or the quasi-Newton scheme as implemented in the VASP code until the forces were less than 0.05 eV/Å for all unconstrained atoms, and the

energy convergence criteria for all self-consistent field calculations were set as 10^{-5} eV. The Brillouin zone integration was sampled with $2 \times 2 \times 2$ Monkhorst-Pack mesh k-points.¹⁰

The adsorption energy was defined as

$$E_{\text{ads}} = E(\text{MOF/M}) - E(\text{MOF}) - E(\text{M}) \quad (\text{S8})$$

where the $E(\text{MOF/M})$, $E(\text{MOF})$ and $E(\text{M})$ represent the total energies of MOF with the adsorbate, the optimized MOF structure and the isolated gas molecules, respectively.

Zn-ox-trz:

$$E_{\text{ads}}(2\text{CO}_2) = -0.3 \text{ eV} = -28.95 \text{ kJ mol}^{-1}$$

$$E_{\text{ads}}(\text{CO}_2) = -0.15 \text{ eV} = -14.47 \text{ kJ mol}^{-1}$$

$$E_{\text{ads}}(2\text{C}_2\text{H}_2) = -0.2 \text{ eV} = -19.30 \text{ kJ mol}^{-1}$$

$$E_{\text{ads}}(\text{C}_2\text{H}_2) = -0.1 \text{ eV} = -9.65 \text{ kJ mol}^{-1}$$

Zn-ox-mtz:

$$E_{\text{ads}}(\text{CO}_2) = -0.1 \text{ eV} = -9.65 \text{ kJ mol}^{-1}$$

$$E_{\text{ads}}(\text{C}_2\text{H}_2) = 0.3 \text{ eV} = 28.95 \text{ kJ mol}^{-1}$$

Breakthrough experiments

Breakthrough experiments of **Zn-ox-mtz** and Zn-ox-trz for the equimolar $\text{CO}_2/\text{C}_2\text{H}_2$ mixtures were performed on a homemade dynamic separation device ($\text{CO}_2/\text{C}_2\text{H}_2$, 50/50, v/v, mass flow rate = 2 mL min^{-1}). Prior to the breakthrough experiment, the as-synthesized sample was firstly activated at 373 K for 12 h at the activation station, after activation, the sample was packed into a self-made adsorption column stain steel column and further flushing the packed column with helium gas for 1 h under room

temperature at a flow rate of 10 mL min⁻¹. The outlet gas from the column was monitored using gas chromatography (Agilent GC 490).

Transient breakthrough simulations

Transient breakthrough simulations were carried out for the same set of operating conditions as in the experimental data sets, using the methodology described in earlier publications.^{2,3,11,12}

We summarize below the simulation methodology used to perform transient breakthrough calculations for fixed bed adsorbers; see schematics in Figure S20 and Figure S21. For an n -component gas mixtures in plug flow through a fixed bed maintained under isothermal conditions, the molar concentrations in the gas phase at any position and instant of time are obtained by solving the following set of partial differential equations for each of the species i in the gas mixture.

$$\frac{\partial c_i(t, z)}{\partial t} + \frac{\partial (v(t, z)c_i(t, z))}{\partial z} + \frac{(1-\varepsilon)}{\varepsilon} \rho \frac{\partial \bar{q}_i(t, z)}{\partial t} = 0; \quad i = 1, 2, \dots, n \quad (\text{S9})$$

In eq (S9), t is the time, z is the distance along the adsorber, ρ is the framework density, ε is the bed voidage, v is the interstitial gas velocity, and $\bar{q}_i(t, z)$ is the *spatially averaged* molar loading within the crystallites of radius r_c , monitored at position z , and at time t . The time $t = 0$, corresponds to the time at which the feed mixture is injected at the inlet to the fixed bed.

The radial distribution of molar loadings, q_i , within a spherical MOF crystallite, of radius r_c , is obtained from a solution of a set of differential equations describing the uptake.

$$\rho \frac{\partial q_i(r,t)}{\partial t} = -\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 N_i) \quad (\text{S10})$$

The intra-crystalline fluxes N_i in eq (S10) are related to gradients in the chemical potential gradients by the Maxwell-Stefan equations.^{11,12}

$$N_i = -\rho \mathcal{D}_i \frac{q_i}{RT} \frac{\partial \mu_i}{\partial r} \quad (\text{S11})$$

In eqs (S10) and (S11), R is the gas constant, T is the temperature, ρ represents the framework density of the microporous crystalline material, r is the radial distance coordinate, and the component loadings q_i are defined in terms of moles per kg of framework. The \mathcal{D}_i characterize and quantify the interaction between species i and pore walls. The M-S diffusivity \mathcal{D}_i equals the corresponding diffusivity for a unary system, determined at the same pore occupancy.

At any time, t , during the transient approach to thermodynamic equilibrium, the spatial-averaged component loading within the crystallites of radius r_c is calculated using.

$$\bar{q}_i(t) = \frac{3}{r_c^3} \int_0^{r_c} q_i(r,t) r^2 dr \quad (\text{S12})$$

Summing eq (S12) over all n species in the mixture allows calculation of the *total average* molar loading of the mixture within the crystallite.

$$\bar{q}_i(t, z) = \sum_{i=1}^n \bar{q}_i(t, z) \quad (\text{S13})$$

The term $\frac{\partial \bar{q}_i(t, z)}{\partial t}$ in eq (S9) is determined by solving the set of eqs (S10), (S11), (S12), and (S13). At any time t , and position z , the component loadings at the outer surface of the particle $q_i(r_c, t, z)$ is in equilibrium with the bulk phase gas mixture with partial pressures $p_i(t, z)$ in the bulk gas mixture. the component loadings at the surface

of the crystallites $q_i(r_c, t, z)$ are calculated using the Ideal Adsorbed Solution Theory (IAST)

The interstitial gas velocity is related to the *superficial* gas velocity by

$$v = \frac{u}{\varepsilon} \quad (\text{S14})$$

At time, $t = 0$, the inlet to the adsorber, $z = 0$, is subjected to a step input of the n -component gas mixture and this step input is maintained till the end of the adsorption cycle when steady-state conditions are reached.

$$t \geq 0; \quad p_i(0, t) = p_{i0}; \quad u(0, t) = u_0 \quad (\text{S15})$$

where $u_0 = v\varepsilon$ is the superficial gas velocity at the inlet to the adsorber.

The adsorber tube is divided into 100 slices, and each spherical crystallite was discretized into 20-50 equi-volume slices. The results thus obtained were confirmed to be of adequate accuracy. Combination of the discretized partial differential equations (PDEs) along with the algebraic equations describing mixture adsorption equilibrium (IAST), results in a set of differential-algebraic equations (DAEs), which are solved using BESIRK.^{11,12} BESIRK is a sparse matrix solver, based on the semi-implicit Runge-Kutta method originally developed by Michelsen, and extended with the Bulirsch-Stoer extrapolation method.^{11,12} Use of BESIRK improves the numerical solution efficiency in solving the set of DAEs. The evaluation of the sparse Jacobian required in the numerical algorithm is largely based on analytic expressions.

We describe below how we compare experimental data on transient breakthroughs with breakthrough simulations using the methodology outlined in the foregoing section.

The following data are available for the experimental breakthroughs.

Inside diameter of tube of diameter: $d = 10$ mm.

Effective length of packed column: L .

The mass of the crystallites of Zn-ox-mtz in the packed tube: $m_{ads} = 1.8867$ g.

The crystal framework density ρ kg m⁻³.

Total pressure, $p_t = 1$ bar and temperature, $T = 298$ K at which the experiments are conducted.

Composition of entering gas phase mixture = 50/50.

The total flow rate of the gas mixture at the entrance to the tube $Q_0 = 2$ mL min⁻¹.

We calculate $(1 - \varepsilon) = \frac{m_{ads}/\rho}{\pi d^2 L/4}$ and $\varepsilon = 1 - \frac{m_{ads}/\rho}{\pi d^2 L/4}$.

The superficial gas velocity at the inlet to the adsorber $u = \frac{Q_0}{\pi d^2/4}$.

The interstitial velocity $v = \frac{u}{\varepsilon}$.

For Zn-ox-trz and Zn-ox-mtz, the diffusional limitations are described by choosing the diffusional time constant $\frac{D_i}{r_c^2} = 1 \times 10^{-4}$ s⁻¹ for both CO₂, and C₂H₂. The chosen diffusivities allow good match with experiments.

Separation factor and gas purity productivity

The breakthrough selectivity (separation factor) was defined,¹³ the values were calculated by the equation:

$$S_b = \frac{q_i/y_i}{q_j/y_j} \quad (S17)$$

where q_i is the equilibrium adsorption capacity of component i , q_j is the equilibrium adsorption capacity of component j ; and y_i and y_j are the molar fractions of component i and j in gas phase, respectively.

The equilibrium adsorption capacity of gas i (q_i) and j (q_j) (mmol g^{-1}) were calculated from the breakthrough curve by the equation:

$$q_i = \frac{f_i(t_1 - t_0) - f_i \int_{t_0}^{t_1} F_i(t) dt}{22.4 \times m} \quad (\text{S18})$$

$$q_j = \frac{f_j(t_1 - t_0) - f_j \int_{t_0}^{t_1} F_j(t) dt}{22.4 \times m} \quad (\text{S19})$$

The calculation method of the C_2H_2 purity (c) is as follows

$$c = \frac{q_{\text{C}_2\text{H}_2}}{q_{\text{C}_2\text{H}_2} + q_{\text{CO}_2}} \quad (\text{S20})$$

The gas breakthrough gas amount (q_i) (mmol g^{-1}) was calculated by integrating the breakthrough curve $F_i(t)$ as following equation:

$$q_i = \frac{f_i \int_0^{t_1} F_i(t) dt}{22.4 \times m} \quad (\text{S21})$$

Where the m represents the adsorbent mass, f_i is the flow rate of gas i (mL min^{-1}); $F_i(t)$ is the function of the breakthrough curve of component i.

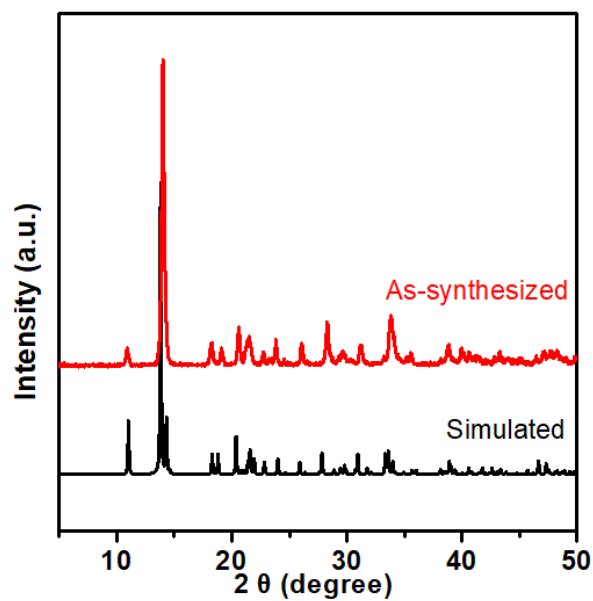


Figure S1. PXRD patterns of Zn-ox-trz. The experimental result of as-synthesized sample and the simulation one from single crystal X-ray diffraction data.

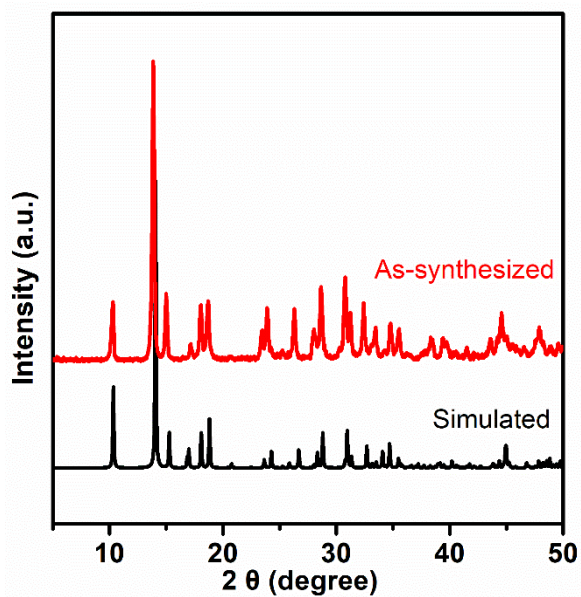


Figure S2. PXRD patterns of Zn-ox-mtz. The experimental result of as-synthesized sample and the simulation one from single crystal X-ray diffraction data.

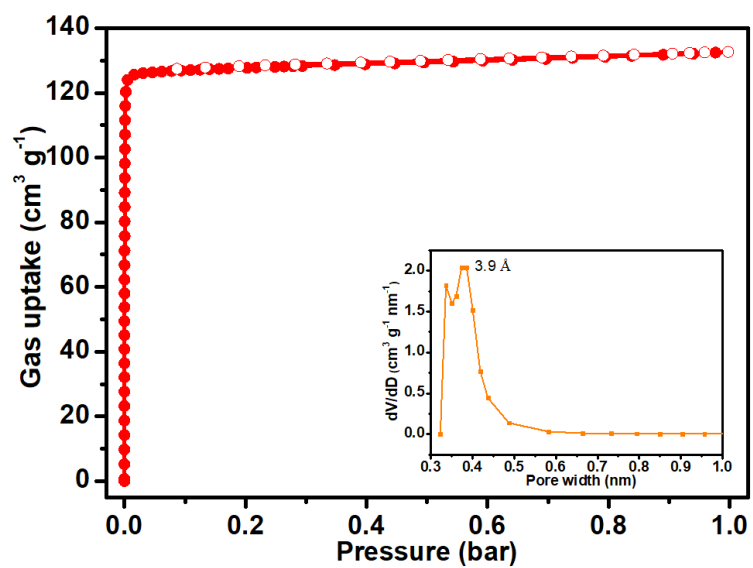


Figure S3. CO₂ sorption isotherms at 195 K on Zn-ox-trz.

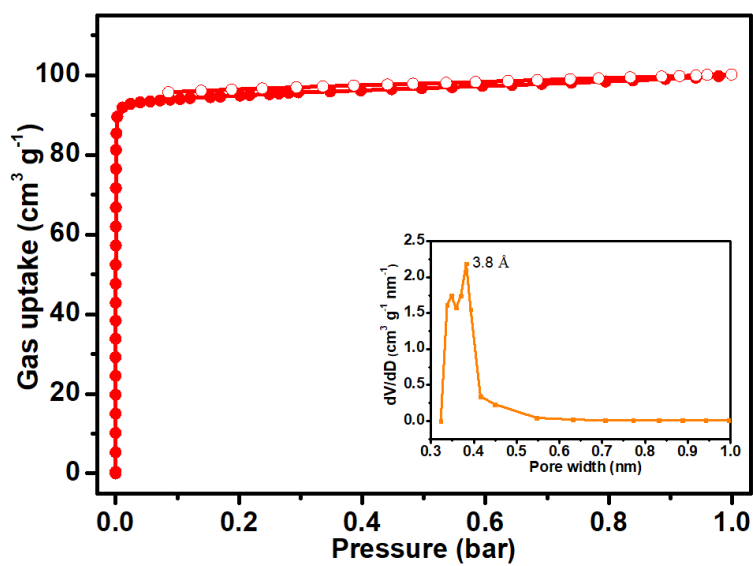


Figure S4. CO₂ sorption isotherms at 195 K on Zn-ox-mtz.

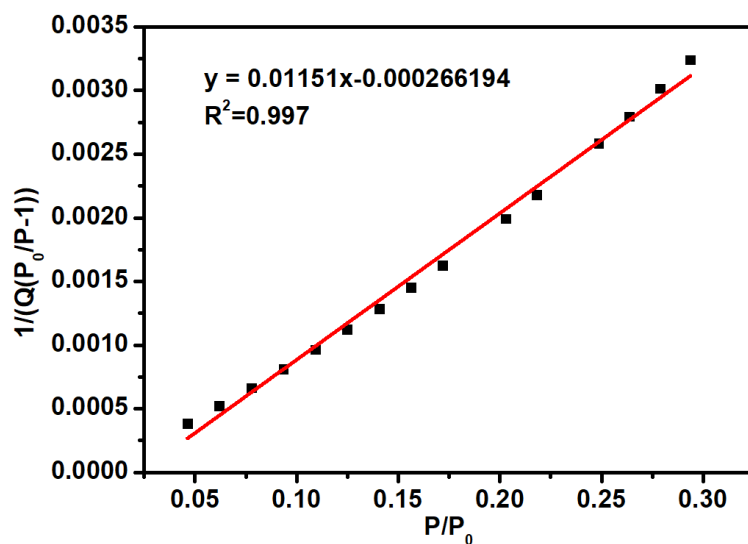


Figure S5. BET surface area plots of Zn-ox-trz.

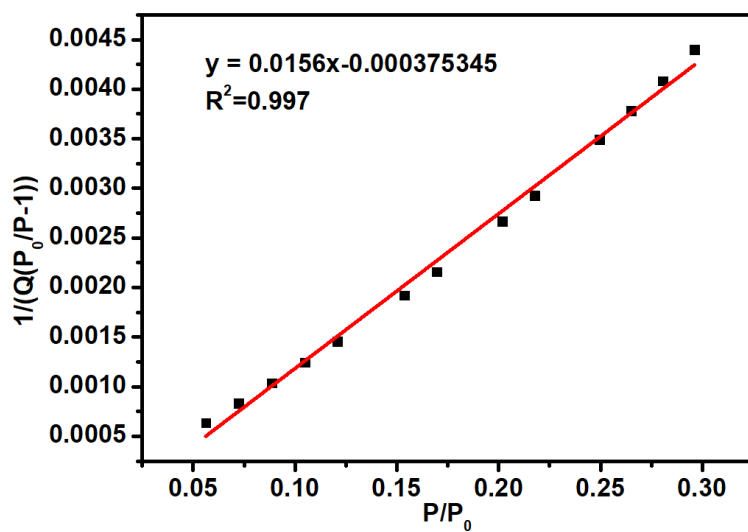


Figure S6. BET surface area plots of Zn-ox-mtz.

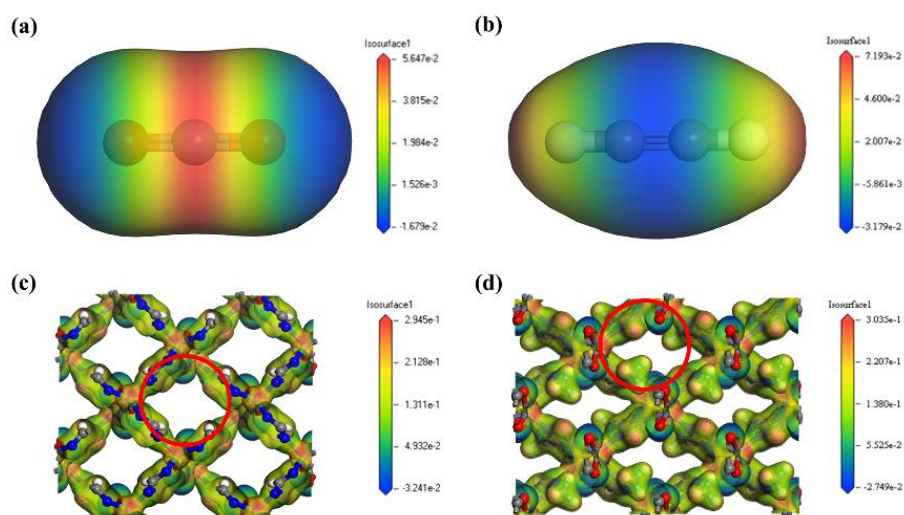


Figure S7. The electrostatic potential of gas molecules: (a) CO₂ molecule, (b) C₂H₂ molecule; and pore surfaces: (c) Zn-ox-trz framework, (d) **Zn-ox-mtz** framework.

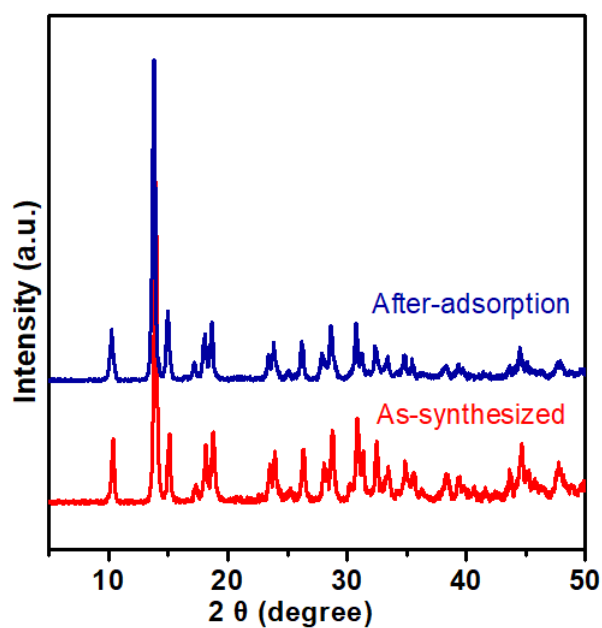


Figure S8. PXRD patterns of **Zn-ox-mtz**. The experimental result of as-synthesized sample and the sample of after-sorption experiments.

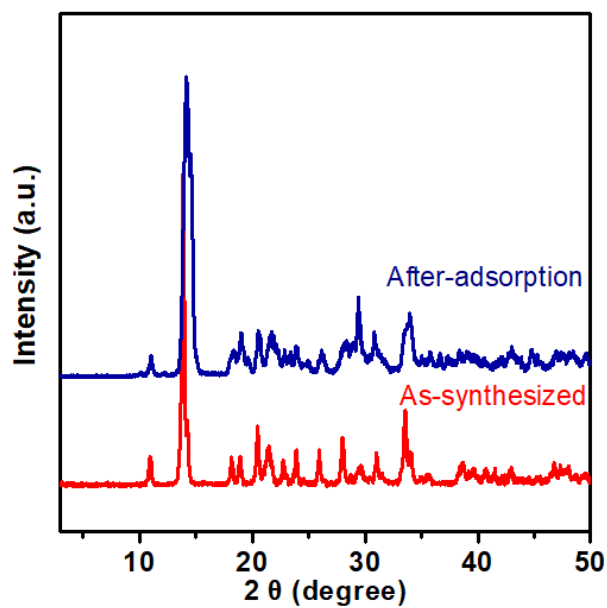


Figure S9. PXRD patterns of Zn-ox-trz. The experimental result of as-synthesized sample and the sample of after-sorption experiments.

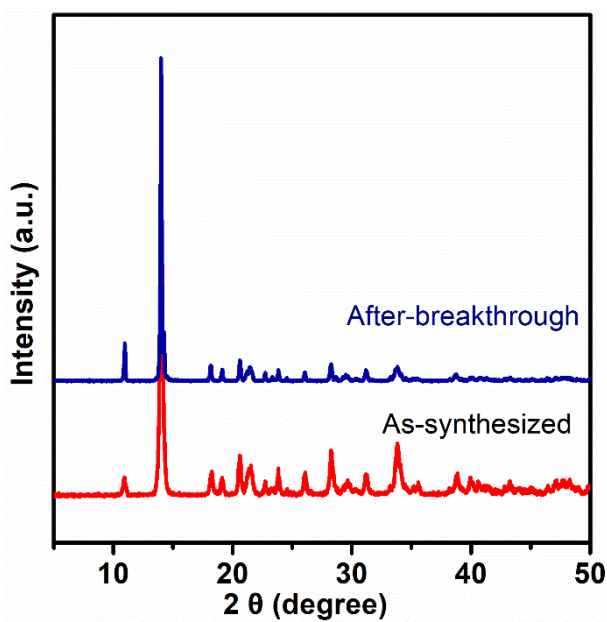


Figure S10. PXRD patterns of Zn-ox-trz. The experimental result of as-synthesized sample and the sample of after-breakthrough experiments.

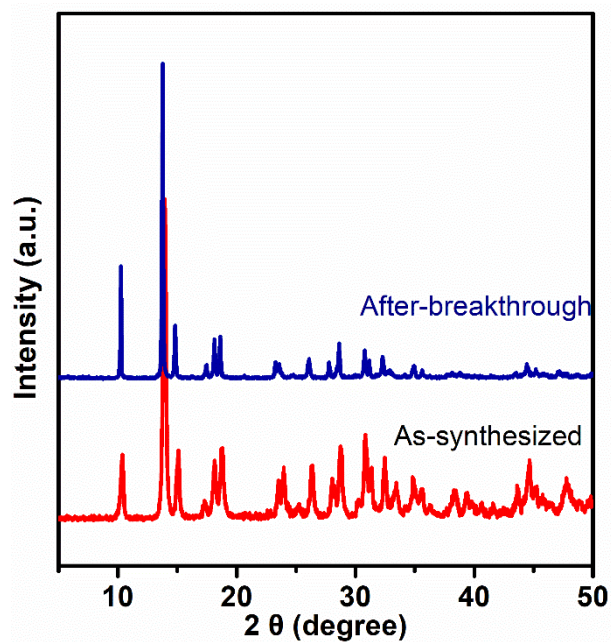


Figure S11. PXRD patterns of **Zn-ox-mtz**. The experimental result of as-synthesized sample and sample of after-breakthrough experiments.

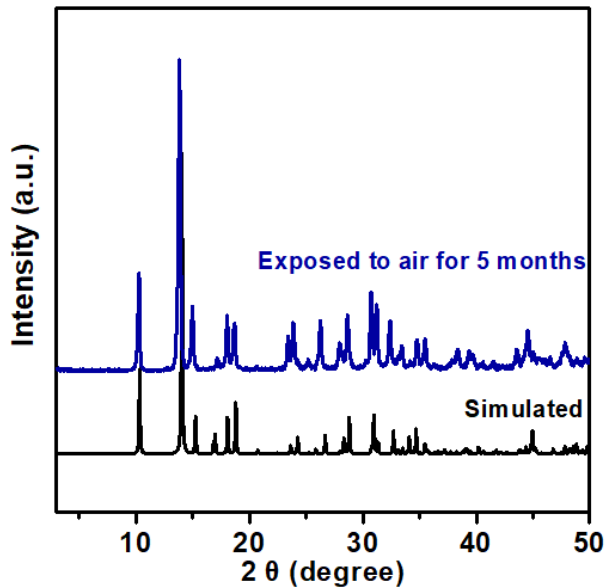


Figure S12. PXRD patterns of **Zn-ox-mtz**. The experimental result of sample exposed to air for 5 months and the simulation one from single crystal X-ray diffraction data.

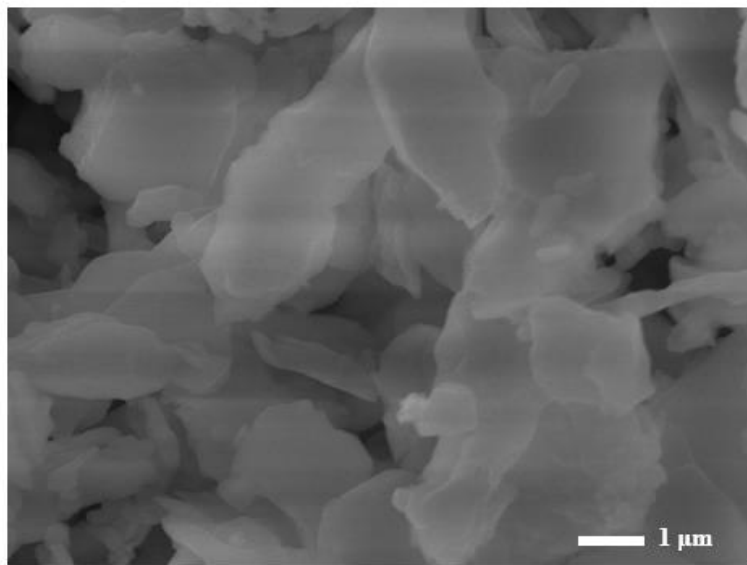


Figure S13. The SEM image of Zn-ox-mtz.

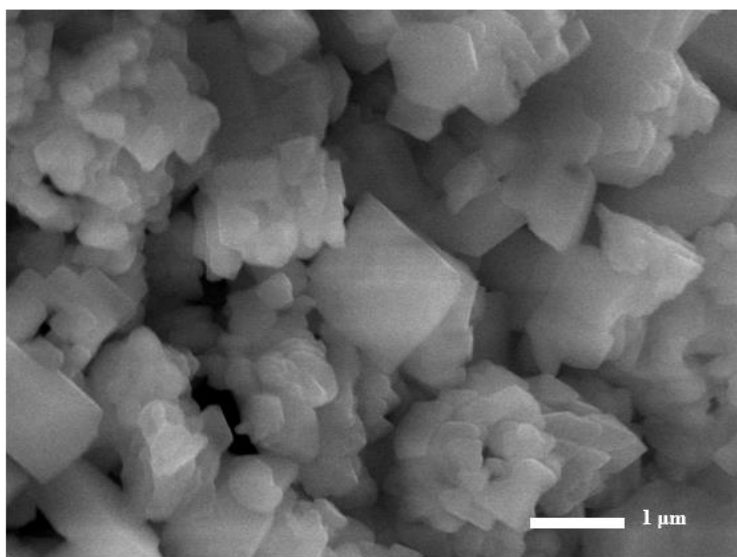


Figure S14. The SEM image of Zn-ox-trz.

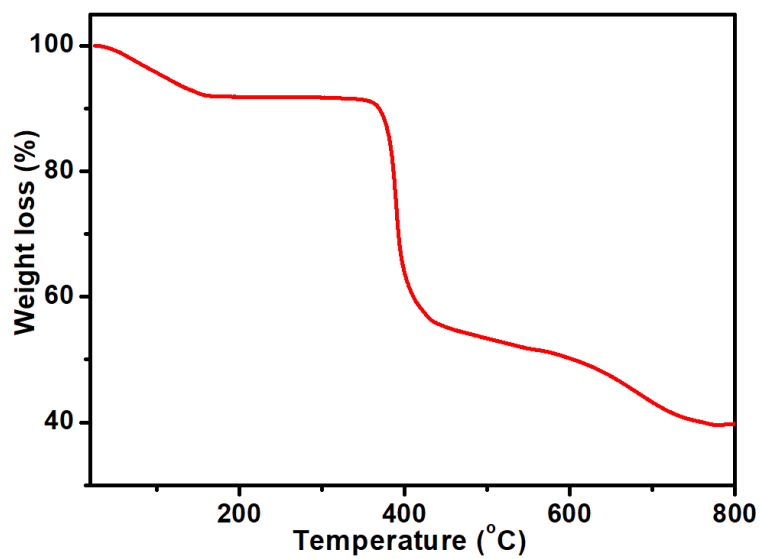


Figure S15. TG curve of Zn-ox-mtz under argon atmosphere.

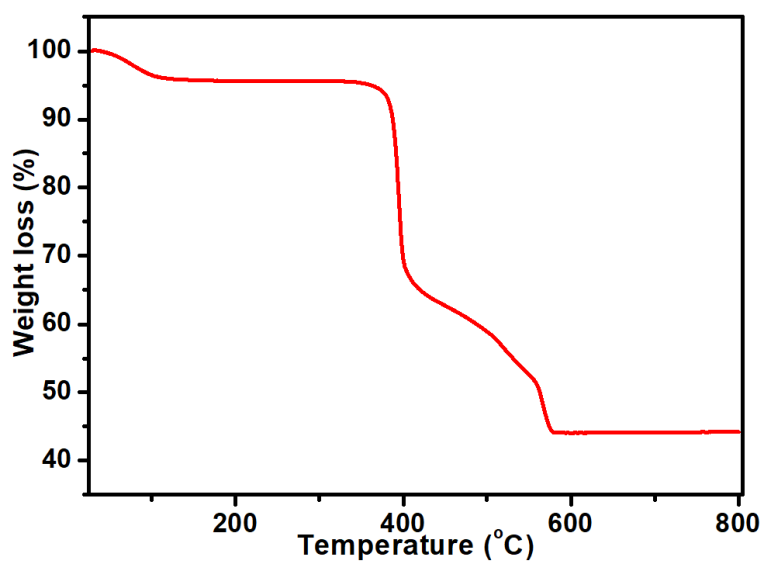


Figure S16. TG curve of Zn-ox-trz under argon atmosphere.

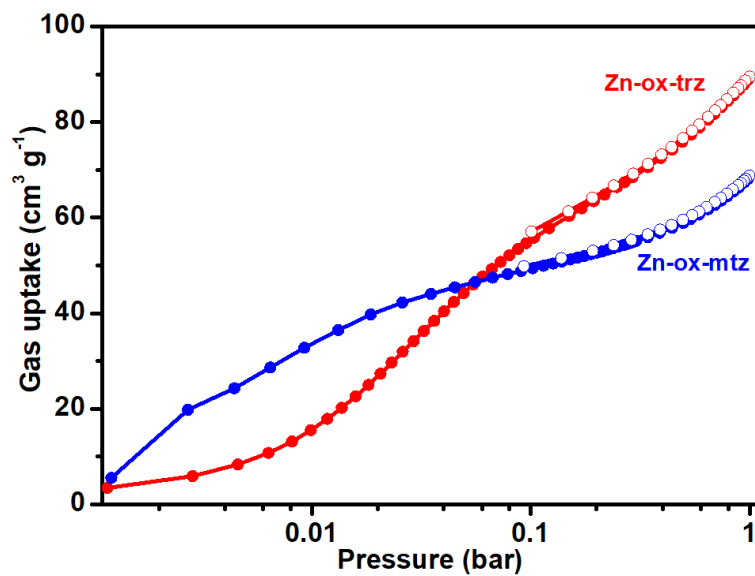


Figure S17. The comparison of CO₂ uptake profiles between Zn-ox-trz and Zn-ox-mtz at 298 K and 1.0 bar.

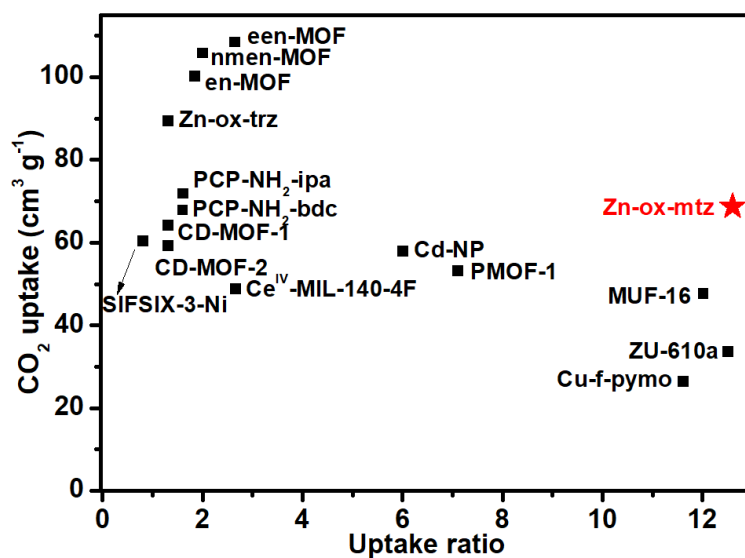


Figure S18. Comparison of CO₂/C₂H₂ uptake ratio and CO₂ uptake with representative CO₂-selective adsorbents at ambient conditions.

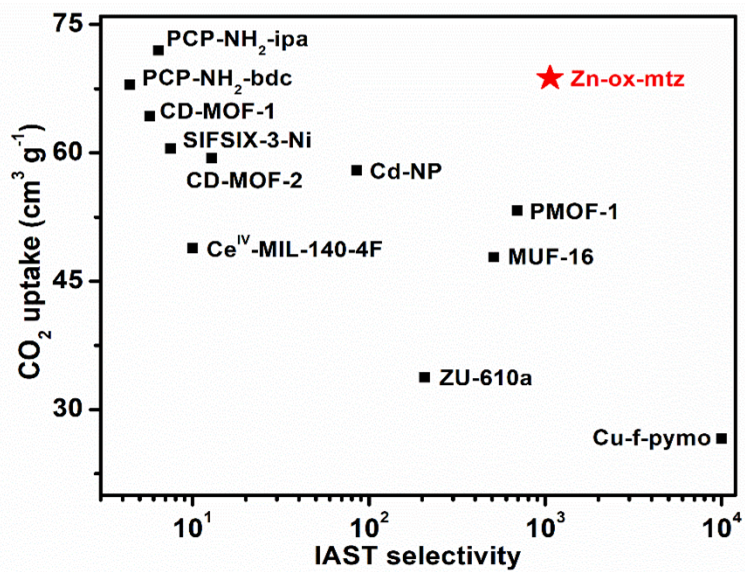


Figure S19. Comparison of equimolar CO₂/C₂H₂ selectivity and CO₂ uptake with representative CO₂-selective adsorbents at ambient conditions.

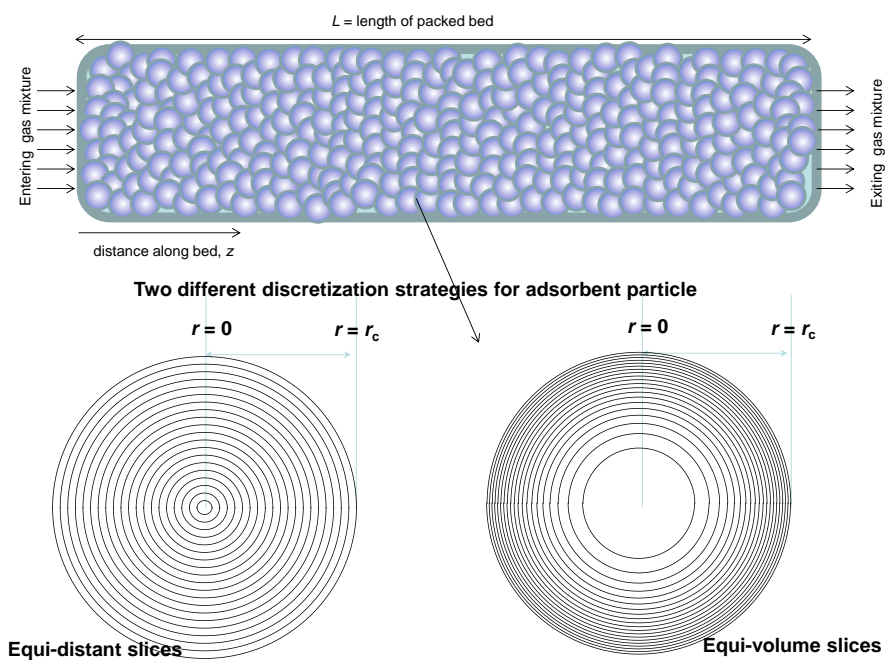


Figure S20. Two different discretization schemes for a single spherical crystallite.

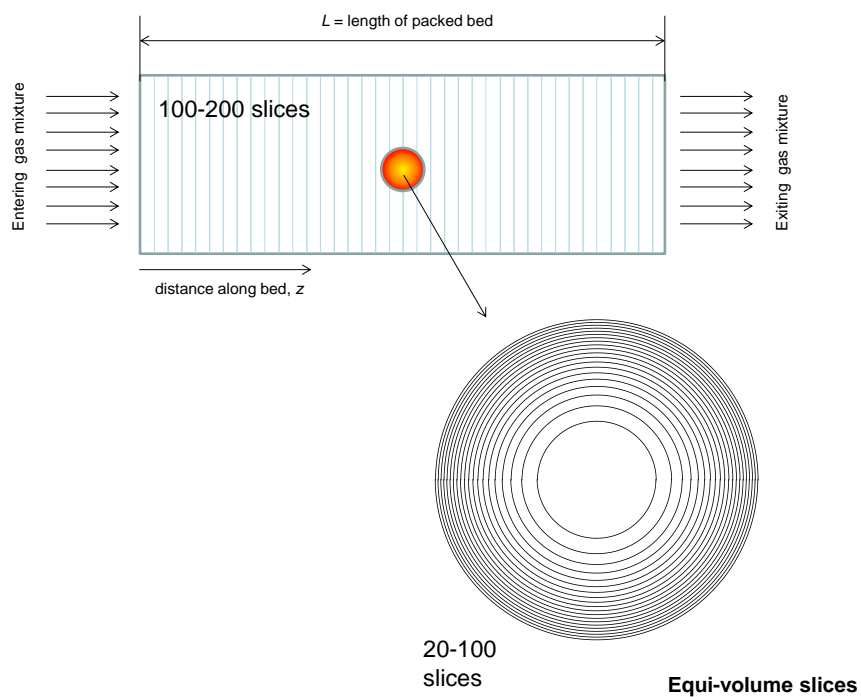


Figure S21. Discretization scheme for fixed bed adsorber.

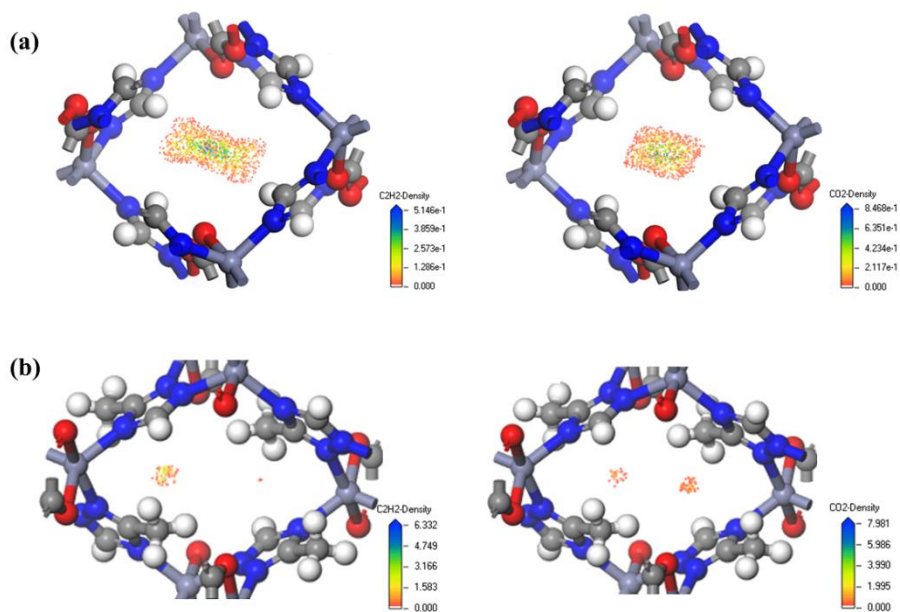


Figure S22. Adsorption density distribution calculated by GCMC simulation at 298 K and 1.0 bar for C_2H_2 and CO_2 in (a) Zn-ox-trz and (b) Zn-ox-mtz.

Table S1. Dual-site Langmuir fits for CO₂ in Zn-ox-trz and **Zn-ox-mtz**.

	Site A			Site B		
	$\frac{q_{A,sat}}{\text{mol/kg}}$	$\frac{b_{A0}}{\text{Pa}^{-1}}$	$\frac{E_A}{\text{kJ mol}^{-1}}$	$\frac{q_{B,sat}}{\text{mol/kg}}$	$\frac{b_{B0}}{\text{Pa}^{-1}}$	$\frac{E_B}{\text{kJ mol}^{-1}}$
Zn-ox-trz	3.2	6.150×10^{-11}	38	3	4.766×10^{-14}	45
Zn-ox-mtz	2.3	4.245×10^{-11}	43	3	3.472×10^{-15}	51

Table S2. 1-site Langmuir-Freundlich fits for C₂H₂ in Zn-ox-trz and **Zn-ox-mtz**.

	$\frac{q_{sat}}{\text{mol kg}^{-1}}$	$\frac{b_0}{\text{Pa}^{-\nu}}$	$\frac{E}{\text{kJ mol}^{-1}}$	ν
Zn-ox-trz	3.0	6.560×10^{-15}	52.6	1.37
Zn-ox-mtz	3.5	1.375×10^{-6}	4.5	0.78

Table S3. Crystallographic parameters and refinement details of **Zn-ox-mtz**.

Zn-ox-mtz	
Formula	C ₄ H ₆ N ₃ O ₃ Zn
<i>Mr</i> (g mol ⁻¹)	209.49
Crystal system	monoclinic
Space group	<i>P2₁/c</i>
<i>a</i> (Å)	8.6166(2)
<i>b</i> (Å)	7.8948(1)
<i>c</i> (Å)	10.5066(2)
<i>α</i> (°)	90
<i>β</i> (°)	96.968(2)
<i>γ</i> (°)	90
<i>V</i> (Å ³)	709.45(2)
<i>Z</i>	4
<i>D_c</i> (g cm ⁻³)	1.961
F (000)	420.0
<i>μ</i> (mm ⁻¹)	4.558
GOF on <i>F</i> ²	1.149
<i>R_I</i> , <i>wR₂</i> [<i>I</i> >2σ(<i>I</i>)] ^a	0.0387, 0.1001
<i>R_I</i> , <i>wR₂</i> [all data] ^b	0.0442, 0.1018

^a $R_1 = \sum ||F_o| - |F_c|| / \sum |F_o|$. ^b $wR_2 = \{ \sum [w(F_o^2 - F_c^2)^2] / \sum w(F_o^2)^2 \}^{1/2}$

Table S4. Summary of adsorption and separation metrics of CO₂-selective materials reported in the literatures at 1 bar and room temperature.^a

Materials	CO ₂ (cm ³ g ⁻¹ / cm ³ cm ⁻³)	C ₂ H ₂ (cm ³ g ⁻¹ / cm ³ cm ⁻³)	Uptake ratio	IAST	Ref.
Mn(bdc)(dpe)	46.8/64.7	7.4/10.2	6.3	8.8	14
Co(HL ^{dc}) ^b	239.5/320	140/187	1.7	1.7	15
SIFSIX-3-Ni	60.5/98.4	73.9/120.2	0.8	7.5	16
CD-MOF-1	64.3/-	49.9/-	1.3	5.7	17
CD-MOF-2	59.4/-	45.5/-	1.3	12.8	17
MUF-16	47.8/74.7	4.0/6.3	12	510	18
Cd-NP	58.0/109.4	9.7/18.3	6.0	85	19
PCP-NH ₂ -ipa	72.0/93.6	43.4/56.4	1.6	6.4	20
PCP-NH ₂ -bdc	68.0/86.2	42.7/54.0	1.59	4.4	20
Ce(IV)-MIL-1404F	48.9/110.3	18.3/41.4	2.65	~10	21
Cu-F-pymo	26.6/51.5	2.3/4.5	11.6	>10 ⁵	22
Tm ₂ (OH-bdc) ₂ (μ ₃ -OH) ₂ (H ₂ O) ₂	130.6/155.5	47.0/56.0	2.8	18.2	23
Zn(atz) (BDC-Cl ₄) _{0.5}	34.5/56.8	17.9/29.5	1.9	2.4	24
PMOF-1 ^c	53.3/79.6	7.5/11.2	7.1	694	25
ZU-610a	33.8/51.7	2.7/4.1	12.5	207	26
Y-bptc	55.0/73.1	26.2/36.5	2.1	4.1	27
en-MOF	100.352/-	54.432/-	1.8	-	28
nmen-MOF	96.32/-	53.312/-	2.0	-	28

een-MOF	108.64/-	41.22/-	2.6	-	28
Zn-ox-trz	89.49/157.8	67.9/119.6	1.3	1.9	This work
Zn-ox-mtz	68.8/123.3	5.5/9.9	12.6	1064.9	This work

Note:

^a At the proof stage of this article, we found that the recently published Al(HCOO)₃, ALF, had higher CO₂/C₂H₂ inverse selectivity and C₂H₂ production.²⁹

^b data collected at 195 K.

^c data collected at 273 K.

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