

Pore Space Partition within a Metal–Organic Framework for Highly Efficient C₂H₂/CO₂ Separation

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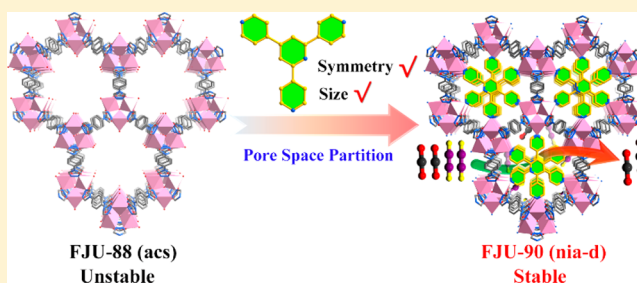
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Supporting Information

ABSTRACT: The pore space partition (PSP) approach has been employed to realize a novel porous MOF (FJU-90) with dual functionalities for the challenging C₂H₂/CO₂ separation under ambient conditions. By virtue of a triangular ligand (Tripp = 2,4,6-tris(4-pyridyl)pyridine), the cylindrical channels in the original FJU-88 have been partitioned into uniformly interconnected pore cavities, leading to the dramatically reduced pore apertures from 12.0 × 9.4 to 5.4 × 5.1 Å². Narrowing down the pore sizes, the resulting activated FJU-90a takes up a very large amount of C₂H₂ (180 cm³ g⁻¹) but much less of CO₂ (103 cm³ g⁻¹) at 298 K and 1 bar, demonstrating it to be the best porous MOF material for this C₂H₂/CO₂ (50%:50%) separation in terms of the C₂H₂ gravimetric productivity. IAST calculations, molecular modeling studies, and simulated and experimental breakthrough experiments comprehensively demonstrate that the pore space partition strategy is a very powerful approach to constructing MOFs with dual functionality for challenging gas separation.



INTRODUCTION

Porous metal–organic frameworks (MOFs) have emerged as very promising materials for gas separation and purification because of their tunable pore sizes in reach sieving effects and their functional pore surfaces in directing the preferential binding of one gas molecule over another.^{1–8} Over the past two decades, a large number of porous MOFs have been realized for different gas separation and purification schemes, ranging from comparatively less challenging ones such as CO₂/N₂ and CO₂/CH₄^{9,10} to more challenging ones such as alkyne/alkene and olefin/paraffin separation.^{11–18} Because C₂H₂ and CO₂ gas molecules have very similar physical properties (boiling points: C₂H₂, 189.3 K; CO₂, 194.7 K; molecular shapes and sizes: C₂H₂, 3.3 × 3.3 × 5.7 Å³; CO₂, 3.2 × 3.3 × 5.4 Å³)¹⁹ and almost identical kinetic diameters of ~3.3 Å, it is very difficult and challenging to realize the porous materials for C₂H₂/CO₂. The first porous MOF or porous coordination polymer for this separation was realized back in 2005 in which the oxygen basic sites play important roles in inducing their stronger interactions with acetylene molecules.²⁰ It took quite a long time for the community to target a few porous MOFs for this separation at room temperature.^{21–26} The unique UTSA-74,²¹ the MOF-Zn-74 isomer, takes up much more acetylene over carbon dioxide under low pressures of up to 1 bar attributed to the accessible Zn²⁺ binding two acetylene

molecules but only one carbon dioxide gas molecules, unlike MOF-Zn-74 which adsorbs similar amounts of acetylene and carbon dioxide under 1 bar. Another porous MOF for this separation is a flexible MOF, UTSA-300a,²³ in which the acetylene molecule can trigger a structural change and thus can open the pores through the C–H...F hydrogen bonding interactions. The acetylene uptake in UTSA-300a is accordingly not very high at about 69 cm³/g under ambient conditions.

The ideal porous materials for gas separation/purification are those with both high gas uptake and separation selectivities, posing daunting challenges for scientists and engineers, a so-called trade-off. We have made some progress over the past several years in addressing these challenges through so-called dual functionalities in which both pore sizes and functional surfaces simultaneously enforce gas separations without the sacrifice of moderate pore volumes or surface areas to take up large numbers of the preferred gas molecules. Although such a dual-functionality approach is quite efficient in realizing porous MOFs for gas separations, the porous MOFs, UTSA-16 for CO₂/N₂ separation and UTSA-100 for C₂H₂/C₂H₄ separation,^{27,28} respectively, were basically discovered unexpectedly

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without any rational design. In this regard, the approach developed by Bu and Feng, termed the pore space partition (PSP),^{29–37} is particularly interesting and important. It means that the pore spaces in some porous MOFs with large pores can be rationally partialized. To further make use of the functional pore surfaces, such a PSP approach might provide us with a much more rational strategy for realizing novel porous MOFs with dual functionalities and thus for gas separation/purification.

Herein we report a rare example (termed **FJU-90**) of such MOFs through this PSP approach to C_2H_2/CO_2 separation. As shown in Figure 1 (left), the mother MOF, **FJU-88**,³⁸ has a

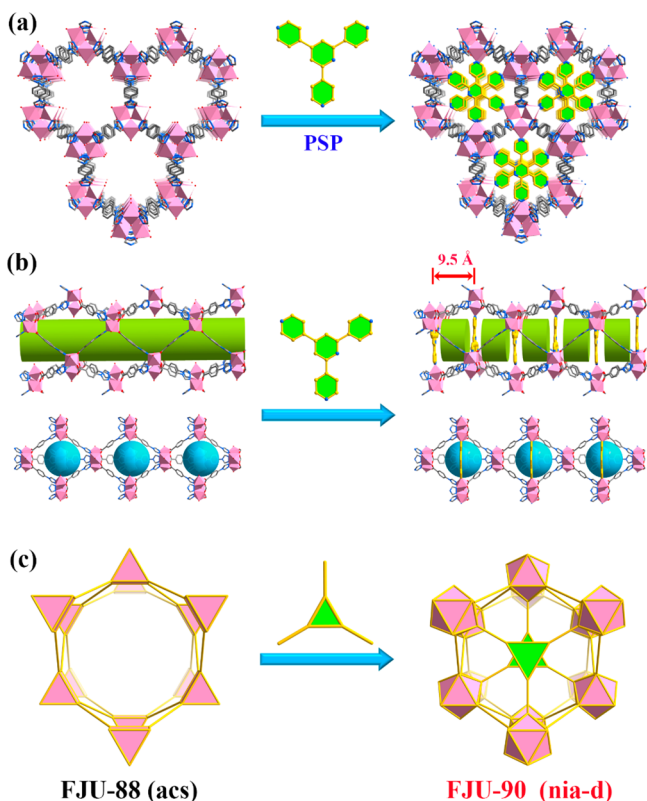


Figure 1. Illustration of pore space partition (PSP) through symmetry- and size-matching-regulated ligand insertion. (a) Viewed along the crystallographic c axis of the cylindrical channel before and after partitioning. (b) Side view of the 1D cylindrical channel and trigonal bipyramidal nanocages before and after partitioning. (c) Polyhedral drawing of the connected network in **FJU-88** and **FJU-90** before and after partitioning. Color code: Co, rose; O, red; N, light blue; C, gray or gold; Guest molecules and hydrogen atoms have been omitted for clarity.

very large one-dimensional pore space (pore sizes of about $10.1 \times 10.1 \text{ \AA}^2$ and $12.0 \times 9.4 \text{ \AA}^2$) which is not good for gas separation. Once the pore spaces were partialized through the immobilization of a C_3 -symmetric 2,4,6-tris(4-pyridyl)pyridine (Tripp) regulated ligand, the pore spaces were rationally partialized to up to 9.5 Å with an aperture size of only $5.4 \times 5.1 \text{ \AA}^2$. The resulting activated **FJU-90a** takes up a very large amount of acetylene ($180 \text{ cm}^3 \text{ g}^{-1}$) but much less carbon dioxide ($103 \text{ cm}^3 \text{ g}^{-1}$) at 298 K and 1 bar, demonstrating it to be the best porous MOF material for this C_2H_2/CO_2 (50%:50%) separation in terms of the C_2H_2 gravimetric productivity. Molecular modeling studies and simulated and experimental breakthroughs have well supported the results in

which both optimized pore sizes and pore surfaces of O atoms for the $HC\equiv C-H\cdots O$ hydrogen bonding interactions have collaborative roles in this very challenging gas separation.

EXPERIMENTAL SECTION

Materials and Physical Measurements. All reagents and solvents were commercially available and directly used without further purification. Organic ligands 4-(4*H*-1,2,4-triazol-4-yl)benzoic acid (HCPT)³⁹ and 2,4,6-tris(4-pyridyl)pyridine (Tripp)⁴⁰ were synthesized according to the previously reported procedure. A PerkinElmer 240C elemental analyzer was used to obtain elemental analyses of C, H, and N. A Fourier-transform infrared spectrum (FTIR, KBr pellets) was recorded on a Thermo Nicolet 5700 FT-IR instrument from 4000 to 400 cm^{-1} . Thermogravimetric analysis (TGA) was carried out under an air atmosphere from room temperature to $600 \text{ }^\circ\text{C}$ using a Shimadzu TGA-50 analyzer at a heating rate of $5 \text{ }^\circ\text{C min}^{-1}$. Powder X-ray diffraction (PXRD) patterns were recorded by a PANalytical X'Pert³ powder diffractometer equipped with a Cu sealed tube ($\lambda = 1.54184 \text{ \AA}$) at 40 kV and 40 mA over the 2θ range of $5\text{--}40^\circ$. The simulated pattern was produced using the Mercury V1.4 program and single-crystal diffraction data.

Synthesis of FJU-88. **FJU-88** was previously synthesized.³⁸ A mixture of HCPT (94 mg, 0.5 mmol) and $CoCl_2 \cdot 6H_2O$ (120 mg, 0.5 mmol) was dissolved in a mixed solution of $DMA-H_2O-HBF_4$ (21 mL, 10:3:1 v/v/v) and then held in a $120 \text{ }^\circ\text{C}$ oven for 1 day. After cooling to room temperature, the light-orange rod-shaped single crystals were obtained (yield 65%, based on HCPT).

Synthesis of FJU-90. A mixture of HCPT (94 mg, 0.5 mmol), Tripp (100 mg, 0.32 mmol), and $CoCl_2 \cdot 6H_2O$ (120 mg, 0.5 mmol) was dissolved in the mixed solution of $DMA-H_2O-HBF_4$ (21 mL, 10:3:1 v/v/v) and then held in a $120 \text{ }^\circ\text{C}$ oven for 1 day. After cooling to room temperature, the orange polyhedral-shaped crystals that formed were collected, washed with DMA, and dried in air (yield 62%, based on HCPT). Elemental analysis calculated (%) for $[Co_3(\mu_3-OH)(CPT)_3(Tripp)]Cl_2(DMA)_{5.5}(H_2O)_8$ ($C_{69}H_{98.5}Co_3N_{18.5}O_{20.5}Cl_2$): C, 46.98; H, 5.59; N, 14.69. Found: C, 47.04; H, 5.72; N, 14.37.

Single-Crystal X-ray Diffraction (SCXRD) Studies. Data collection and structural analysis of crystal **FJU-90** was collected on the Rigaku Oxford single-crystal diffractometer equipped with graphite monochromatic $Cu K\alpha$ radiation ($\lambda = 1.54184 \text{ \AA}$). The crystal was kept at 150 K during data collection. Using Olex2,⁴¹ the structure was solved with the Superflip⁴² structure solution program using charge flipping and refined with the ShelXL⁴³ refinement package using least-squares minimization. The CPT ligand is disordered over two positions (occupancy 0.5:0.5); this is because the triazolate and carboxylate parts of the ligand show similar coordination models and therefore can substitute for each other at the given site. Additionally, the disorder of the triazolate group leads to the carbon and nitrogen atoms sharing the same crystallographic positions with partial occupancies. All nonhydrogen atoms were refined with anisotropic displacement parameters. The hydrogen atoms on the ligands were placed in idealized positions and refined using a riding model. We employed PLATON⁴⁴ and SQUEEZE⁴⁵ to calculate the diffraction contribution of the solvent molecules and thereby produce a set of solvent-free diffraction intensities. The detailed crystallographic data and structure refinement parameters are summarized in Table S2 (CCDC 1882901).

Gas Adsorption Measurements. To remove all of the guest solvents in the framework, a fresh sample of **FJU-88** or **FJU-90** ($\sim 150 \text{ mg}$) was guest-exchanged with dry CH_3OH at least 10 times, filtered, and degassed at $60 \text{ }^\circ\text{C}$ until the outgas rate was $5 \text{ } \mu\text{mHg min}^{-1}$ prior to measurements. C_2H_2 , CO_2 , and N_2 adsorption isotherms were measured on Micromeritics ASAP 2020 HD88 surface area analyzer for the guest-free sample. An ice-water bath (slush) and a water bath were used for adsorption isotherms at 273 and 298 K, respectively. Pore size distribution (PSD) data was obtained from the 273 K CO_2 and 77 K N_2 adsorption isotherms based on the nonlocal density functional theory (NLDFT) model.⁴⁶

Column Breakthrough Experiments. The breakthrough experiments were carried out in a self-made dynamic mixed-gas breakthrough setup.^{47,48} A stainless steel column with inner dimensions of $\phi = 4 \times 150$ mm was used for sample packing. A microcrystalline sample with a particle size of 220–320 μm obtained via sieving was then packed into the column. The mixed-gas flow and pressure were controlled by using a pressure-control valve and a mass flow controller. Outlet effluent from the column was continuously monitored using gas chromatography (GC-2014, Shimadzu) with a thermal conductivity detector (TCD). The column packed with sample was first purged with a flow of He (50 mL min^{-1}) for 1 h at room temperature. The mixed-gas flow rate during the breakthrough process is 2 mL min^{-1} using 50/50 (v/v) $\text{C}_2\text{H}_2/\text{CO}_2$ at room temperature (298 K). After the breakthrough experiment, the sample was regenerated under vacuum.

On the basis of the mass balance, the gas adsorption capacities can be determined as follows

$$q_i = \frac{C_i V}{22.4 m} \int_0^t \left(1 - \frac{F}{F_0}\right) dt \quad (1)$$

where q_i is the equilibrium adsorption capacity of gas i (mmol g^{-1}), C_i is the feed gas concentration, V is the volumetric feed flow rate (mL min^{-1}), t is the adsorption time (min), F_0 and F are the inlet and outlet gas molar flow rates, respectively, and m is the mass of the adsorbent (g).

RESULTS AND DISCUSSION

Solvothermal reaction of HCPT and Tripp with $\text{CoCl}_2 \cdot 6\text{H}_2\text{O}$ in the mixed DMA/ H_2O solution at 120°C for 1 day afforded orange polyhedral-shaped crystals of FJU-90 (Figure S1). Single-crystal X-ray diffraction analysis revealed that FJU-90 crystallizes in the hexagonal $P6_3/mmc$ space group, the same as for prototypical MOF FJU-88. It is noteworthy that the $[\text{Co}_3(\mu_3\text{-OH})]$ unit in FJU-88 is a six-connected node, while the unit becomes nine-connected in FJU-90 because the three axial positions were occupied by the pyridyl groups from the Tripp ligands (Figure 1a). Notably, compared with FJU-88, the PSP has resulted in a significant decrease in the window size of the trigonal bipyramidal cage from $12.0 \times 9.4 \text{ \AA}^2$ to $5.4 \times 5.1 \text{ \AA}^2$ (taking into account the van der Waals radii of the atoms, Figure S2). Simultaneously, the original 1D cylindrical channel along the crystallographic c axis (with an aperture size of $10.1 \times 10.1 \text{ \AA}^2$) has been divided by the Tripp partitions (at an interval of ca. 9.5 \AA) into numerous uniform interconnected pore cavities, which displays the potential for enhanced confinement effects and multiple-point adsorption (dual functionalities), especially for C_2H_2 with acidic H atoms (Figure 1b).⁴⁹ Topologically, if the Tripp ligand and the $[\text{Co}_3(\mu_3\text{-OH})]$ unit are simplified as 3- and 9- c nodes, respectively, then the 3D framework of FJU-90 exhibits a (3,9)-connected network with a point symbol of $(4^3)(4^{21}6^{15})$ (nia-d topology),⁵⁰ which is notably rigid as compared to the original 6- c network (acs topology, Figure 1c). Without considering the guest solvent molecules, the total accessible volumes in FJU-90 are estimated to be 62%, slightly lower than for the prototypical structure (72%), as calculated by PLATON software, which is reasonable considering the space occupancy of Tripp ligands. Obviously, the pore volume after the pore space partition approach is still higher than those of many other highly selective MOF adsorbents.^{11,16,51}

The phase purities of the prepared bulk products were verified by a comparison of the experimental and simulated powder X-ray diffraction (PXRD) patterns and further confirmed by thermogravimetric analysis and elemental

analysis (Figures S6, S7, and S9). Notably, the thermal stability of FJU-90 (up to 300°C) is significantly higher than for original FJU-88 (stable only below 50°C), as proven by the variable-temperature PXRD experiments (Figures S8 and S12). Furthermore, the PXRD result further confirmed that the structure of FJU-90 could be maintained after exposure to air for a month or soaking in water for 1 day, while FJU-88 is unstable after soaking in water for 10 min (Figures S7 and S11). To explore the permanent porosity, the two MOF samples were guest-exchanged with anhydrous CH_3OH at least 10 times and then degassed at 60°C under high vacuum to yield guest-free phases FJU-88a and FJU-90a. The PXRD pattern of FJU-90a revealed that the structural integrity was fully preserved after activation, while FJU-88a loses its crystallinity, which further proves that the host framework after the insertion of the Tripp ligand is more robust and stable than the original one (Figures S7 and S9, details in the Supporting Information).

As shown in Figure 2, the 77 K N_2 adsorption isotherms of FJU-90a show fully reversible type-I behavior with a maximum

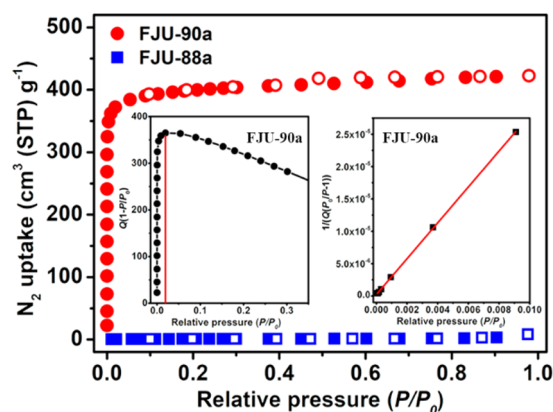


Figure 2. N_2 sorption isotherms (at 77 K) for FJU-88a and FJU-90a. (Inset) BET plots for FJU-90a.

N_2 uptake of $420 \text{ cm}^3 \text{ g}^{-1}$ at 1 bar, while FJU-88a basically takes up no N_2 , which is ascribed to the collapse of the porous structures after activation. The corresponding pore volume in FJU-90a is $0.65 \text{ cm}^3 \text{ g}^{-1}$, which is slighter lower than the theoretical value of $0.74 \text{ cm}^3 \text{ g}^{-1}$ (calculated from the crystal structure) due to the insufficient filling of N_2 on the irregular pore surfaces of FJU-90a (Figure S4) but still higher than those of many other MOF sieves for gas separation.^{11,16,51} The Brunauer–Emmett–Teller (BET) surface area of FJU-90a is up to $1572 \text{ m}^2 \text{ g}^{-1}$ as calculated from the N_2 adsorption isotherms, which is comparable to that of CPM-233 ($1320 \text{ m}^2 \text{ g}^{-1}$)³¹ but higher than that of Co-MOF1-tpt ($826 \text{ m}^2 \text{ g}^{-1}$)⁵² in the same type MOFs. The pore-size distribution (PSD) of FJU-90a was analyzed by using the 273 K CO_2 and 77 K N_2 isotherms based on the NLDFT model, which show narrow pore cavity size distributions with centers at 5.8 and 8.6 \AA (Figure S14), which are close to the cavity sizes determined from the crystal structure.

Next, we collected the gas sorption isotherms of C_2H_2 and CO_2 for FJU-88a and FJU-90a at 273 and 298 K under 1 bar (Figure 3a) to explore their abilities for gas adsorption and separation. Owing to the high porosity, suitable pore space, and potential O basic sites, remarkable C_2H_2 uptake was observed in FJU-90a, with the adsorbed amounts of 216 and

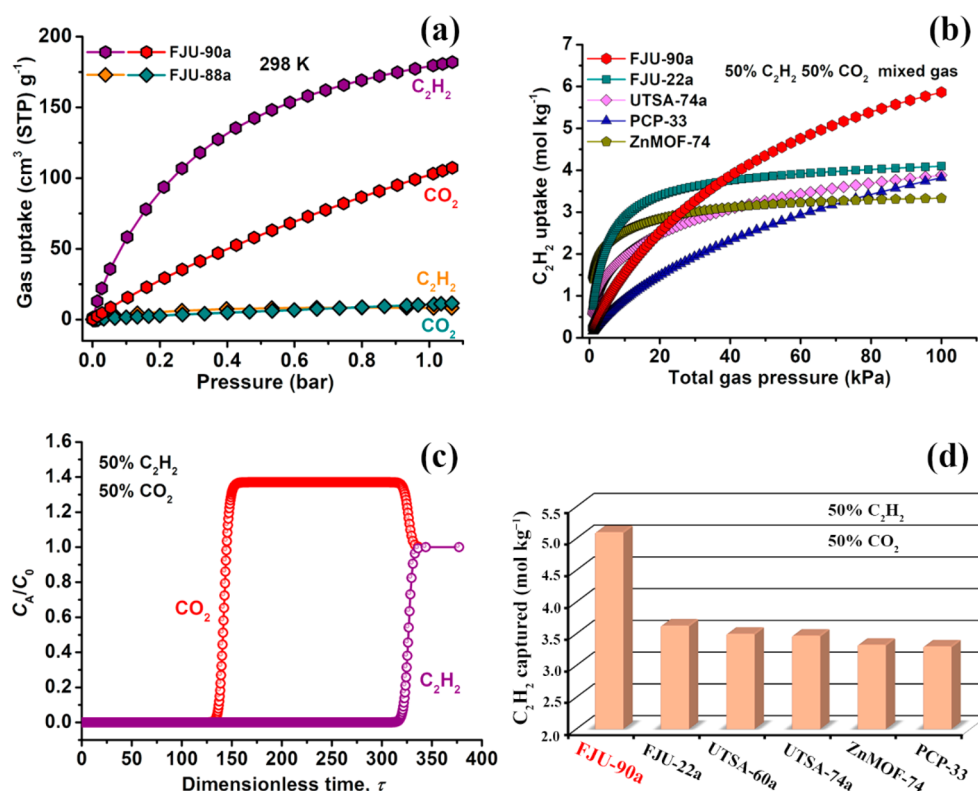


Figure 3. (a) C₂H₂ and CO₂ single-component adsorption isotherms of FJU-88a and FJU-90a at 298 K under 1 bar. (b) Comparison of the IAST calculations of the C₂H₂ uptake of FJU-90a versus those of previously reported best-performing materials for equimolar C₂H₂/CO₂ mixtures. (c) Transient breakthrough simulations for the separation of equimolar C₂H₂/CO₂ mixtures using FJU-90a at 298 K, with a partial pressure of 50 kPa for each. (d) The C₂H₂ gravimetrically captured productivity of FJU-90a in comparison to that of the best-performing MOF materials reported to date and the productivity values of these MOFs were calculated from the simulated column breakthrough curves.

180 cm³ (STP) g⁻¹ at 273 and 298 K, and 1 bar, respectively, which are systematically higher than that of FJU-88a under similar conditions (Figure S13, details in the Supporting Information). Notably, the C₂H₂ uptake capacity in FJU-90a under ambient conditions is higher than those in many renowned MOFs with a high density of open metal sites, such as ZJU-60a (150 cm³ g⁻¹),⁵³ ZnMOF-74 (122 cm³ g⁻¹),⁵⁴ PCP-33 (122 cm³ g⁻¹),⁵⁵ and UTSA-74a (104 cm³ g⁻¹),²¹ and slightly lower than those for MFM-188a (232 cm³ g⁻¹),⁵⁶ FJI-H8 (224 cm³ g⁻¹),⁵⁷ and HKUST-1 (201 cm³ g⁻¹).⁵⁸ However, what is noteworthy is that the CO₂ uptake value of 103 cm³ g⁻¹ in FJU-90a is remarkably lower than that of C₂H₂ under similar conditions.

To assess the adsorption enthalpies of C₂H₂ and CO₂ in FJU-90a, the coverage-dependent isosteric heat of adsorption (Q_{st}) was calculated with the adsorption isotherms at 273 and 298 K and fitted with the dual-Langmuir isotherm model. As shown in Figure S16, the obtained Q_{st} value for C₂H₂ (25.1 kJ mol⁻¹) is obviously higher than that for CO₂ (20.7 kJ mol⁻¹), indicative of the stronger affinity of FJU-90a toward C₂H₂. We note that the Q_{st} value of C₂H₂ in FJU-90a is notably lower than for some famous MOF materials with a high density of open metal or F sites, for example, HKUST-1 (39 kJ mol⁻¹),⁵⁹ FeMOF-74 (47.5 kJ mol⁻¹),⁵⁹ and SIFSIX-2-Cu-i (41.9 kJ mol⁻¹).¹¹ These data highlight that FJU-90a is a promising candidate for the separation of C₂H₂/CO₂ with a lower regeneration energy requirement for C₂H₂. In addition, to help understand the unique adsorption behavior of FJU-90a for C₂H₂ and CO₂, we implemented dispersion-corrected density-functional theory (DFT-D) calculations.⁶⁰ Our results show

that overall the calculated static C₂H₂ and CO₂ binding strengths in FJU-90a are modest, <40 kJ mol⁻¹ (Figure S17; in contrast, the reported static gas binding energies in some SIFSIX MOFs are >50 kJ mol⁻¹).^{11,51} Comparing the two different gases in FJU-90a, the calculated C₂H₂ binding affinity is clearly stronger than that of CO₂ because of the larger electrostatic interactions (between the charge on the framework and the distributed charge on the gas molecule) and strong HC≡C-H...O hydrogen bonding interactions. This accounts for the higher Q_{st} and uptake capacity of C₂H₂ observed experimentally. Furthermore, the DFT-D calculations further demonstrated that the pore space partition approach is feasible for constructing MOFs featuring dual functionalities for separating the C₂H₂/CO₂ mixture.

To address C₂H₂/CO₂ mixture separations, the well-defined approach of the ideal adsorbed solution theory (IAST)⁶¹ is employed to evaluate the adsorption selectivity and uptake capacity at different pressures. Figure 3b presents IAST calculations of the C₂H₂ uptake capacity as a function of the total gas pressure, and Figure S22 provides a comparison of the adsorption selectivity of the binary equimolar C₂H₂/CO₂ mixture in FJU-90a with those of the other four MOFs at 298 K. We note that the IAST selectivity of FJU-90a (4.3) is slightly lower than that of benchmark material UTSA-74a (8.2) and comparable to other famous MOFs, and more importantly, the C₂H₂ uptake value in FJU-90a is remarkably higher than those of other best-performing MOFs under 100 kPa.

To accurately assess the combined effects of the adsorption selectivity and uptake capacity, we performed the transient breakthrough simulations by using the previously reported

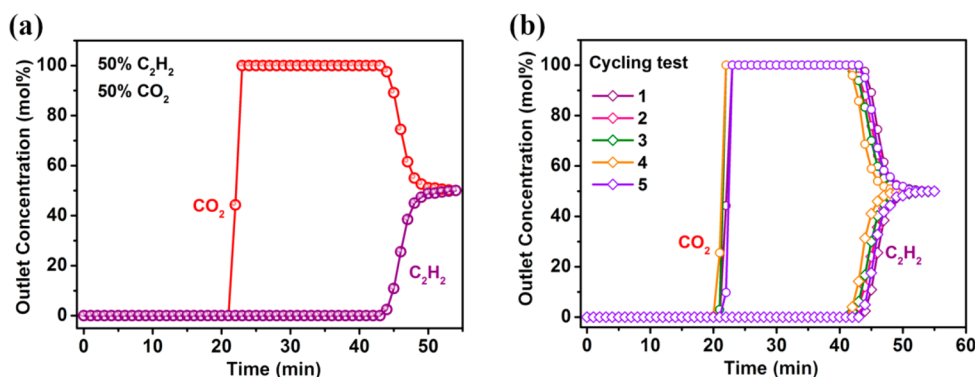


Figure 4. Experimental breakthrough curves for (a) an equimolar C_2H_2/CO_2 mixture and (b) a cycling test of the equimolar C_2H_2/CO_2 mixture in a packed column with **FJU-90a** at 298 K and 1 bar.

simulation methodology.⁶² As shown in Figure 3c, CO_2 eluted first, and this continued for a remarkable time until C_2H_2 broke through as its saturated uptake in **FJU-90a**. Therefore, the simulation results demonstrate that **FJU-90a** is one of the promising candidates for addressing the challenge of C_2H_2/CO_2 mixture separation.

Furthermore, Figure 3d displays a comparison of C_2H_2 captured productivity ($mol\ kg^{-1}$, based on the simulated column breakthrough) for **FJU-90a** with other best-performing MOFs (including **UTSA-74a**,²¹ **FJU-22a**,⁶³ **PCP-33**,⁵⁵ **Zn-MOF-74**,⁵⁴ and **ZJU-60a**⁵³). It was worth noting that the separation performance (selectivity and productivity) for C_2H_2/CO_2 mixtures in **FJU-90a** is systematically higher than that of **ZnMOF-74**. The C_2H_2 volumetric productivity in **FJU-90a** ($4.16\ mol\ L^{-1}$) is slightly lower than for benchmark material **UTSA-74a** ($4.86\ mol\ L^{-1}$); however, **FJU-90a** exhibits the highest gravimetric productivity with a value of $5.10\ mol\ kg^{-1}$, which is much higher than for **UTSA-74a** ($3.47\ mol\ kg^{-1}$). Therefore, the outstanding C_2H_2/CO_2 separation performance of **FJU-90a** should be attributed to the combination of high C_2H_2 uptake capacity and moderate adsorption selectivity.

Acetylene (C_2H_2) is an essential chemical feedstock for modern petrochemical products such as acrylic acid derivatives, vinyl chloride, plastics, and rubber.⁶⁴ However, CO_2 as an impurity always exists in the production process of acetylene. To further evaluate the actual separation performance of the C_2H_2/CO_2 mixture in **FJU-90a**, we carried out laboratory-scale fixed-bed breakthrough experiments under ambient conditions in which the C_2H_2/CO_2 (50/50) gas mixture flowed over a packed column at a total flow rate of $2\ mL\ min^{-1}$. Figure 4a shows that **FJU-90a** can achieve a highly efficient separation of C_2H_2/CO_2 mixtures. CO_2 was first eluted and then quickly approached a pure grade without detectable C_2H_2 , whereas C_2H_2 was retained in the packed column for a remarkable time until its saturated uptake and breakthrough. The dynamic C_2H_2 capture productivity, calculated on the basis of the breakthrough curve, was found to be $1.87\ mol\ kg^{-1}$. For practical industrial applications, the ideal adsorbent should have good recyclability. Thus, we implemented five C_2H_2/CO_2 dynamic breakthrough experiments under the current operating conditions, and the results showed that **FJU-90a** maintained the same retention time and acetylene uptake capacity as the initial one (Figure 4b). Further investigations of **FJU-90a** with larger gas flow or ultralow gas concentration also showed outstanding separation performance for challenging C_2H_2/CO_2 mixtures. Moreover,

FJU-90a retained its stability after the breakthrough cycling test (Figures S23–S26, details in the Supporting Information).

In summary, we have successfully realized a microporous MOF (**FJU-90**) with dual functionality for highly selective C_2H_2/CO_2 separation through the pore space partition (PSP) strategy. The partitioning of the tripyridine ligands not only improves the framework stability but also reduces the pore aperture sizes for the enhanced sieving effect for gas separation. Notably, **FJU-90a** exhibits both a moderately high C_2H_2 uptake capacity and adsorption selectivity, affording new benchmark C_2H_2 captured productivity with respect to C_2H_2/CO_2 (50%:50%) separation under ambient conditions. This work represents an outstanding example of the PSP strategy for rationally designing microporous MOF materials for challenging gas separation/purification, thus significantly facilitating this very active ongoing research.

■ ASSOCIATED CONTENT

📄 Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/jacs.9b00232.

Additional structural figures, FTIR spectrum, TGA curves, PXRD patterns, gas adsorption isotherms, and breakthrough curves (DOCX)
FJU-90 (CIF)

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Notes

The authors declare no competing financial interest.

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Supporting Information

Pore Space Partition within a Metal-Organic Framework for Highly Efficient C₂H₂/CO₂ Separation

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Fitting of pure component isotherms

The experimentally measured loadings for C₂H₂, and CO₂ at 273 K, and 298 K in **FJU-90a** were fitted with the dual-Langmuir isotherm model

$$q = q_{A,sat} \frac{b_A p}{1 + b_A p} + q_{B,sat} \frac{b_B p}{1 + b_B p} \quad (1)$$

The Langmuir parameters for each site is temperature-dependent

$$b_A = b_{A0} \exp\left(\frac{E_A}{RT}\right); \quad b_B = b_{B0} \exp\left(\frac{E_B}{RT}\right) \quad (2)$$

Table S1. Dual-site Langmuir fit parameters for C₂H₂, and CO₂ in **FJU-90a**.

	Site A			Site B		
	$q_{A,sat}$ mol kg ⁻¹	b_{A0} Pa ⁻¹	E_A kJ mol ⁻¹	$q_{B,sat}$ mol kg ⁻¹	b_{B0} Pa ⁻¹	E_B kJ mol ⁻¹
C ₂ H ₂	10.4	1.62×10 ⁻⁹	24	0.6	6.81×10 ⁻⁹	27
CO ₂	17.7	1.52×10 ⁻⁹	19	0.3	7.65×10 ⁻¹⁰	28

Isosteric heat of adsorption

The binding energy of C₂H₂ and CO₂ is reflected in the isosteric heat of adsorption, Q_{st} , defined as

$$Q_{st} = RT^2 \left(\frac{\partial \ln p}{\partial T} \right)_q \quad (3)$$

IAST calculations of adsorption selectivity

In order to compare the C₂H₂/CO₂ separation performance of MOFs, IAST calculations of mixture adsorption were performed. For separation of a binary mixture of components A and B, the adsorption selectivity is defined by

$$S_{ads} = \frac{q_A/q_B}{y_A/y_B} \quad (4)$$

where the q_A , and q_B represent the molar loadings, expressed in mol kg⁻¹, within the MOF that is in equilibrium with a bulk fluid mixture with mole fractions y_A , and $y_B = 1-y_A$. The molar loadings, also called *gravimetric uptake capacities*, are usually expressed with the units mol kg⁻¹. The IAST calculations of 50/50 mixture adsorption taking the mole fractions $y_A = 0.5$ and $y_B = 1-y_A = 0.5$ for a range of pressures up to 100 kPa and 298 K were performed.

Transient breakthrough simulations

The performance of industrial fixed bed adsorbers is dictated by a combination of adsorption selectivity and uptake capacity. For a proper comparison of various MOFs, we perform transient breakthrough simulations using the simulation methodology described in the literature.^{1,2} For the breakthrough simulations, the following parameter values were used: length of packed bed, $L = 0.3$ m; voidage of packed bed, $\varepsilon = 0.4$; superficial gas velocity at inlet, $u = 0.04$ m/s. The transient breakthrough simulation results are presented in terms of a dimensionless time, τ , defined as

$$\tau = \frac{tu}{\varepsilon L}.$$

During the initial transience, the effluent gas contains pure CO₂ and this continues until C₂H₂ starts breaking through because its uptake capacity in the MOF has been reached.

During a certain time interval, $\Delta\tau$, pure CO₂ can be recovered in the gas phase. As in previous works,^{3,4} [ENREF 7](#) we set the purity of CO₂ to 99.95%. The MOFs are compared on the basis of the moles of 99.95% pure CO₂ produced per kg of adsorbent material.

If τ_{break} is the breakthrough time for C₂H₂, during the time interval 0 to τ_{break} , C₂H₂ is captured. The gravimetric C₂H₂ capture capacity, expressed in mol/kg, can be determined from a material balance.



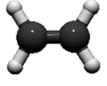
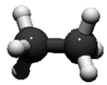

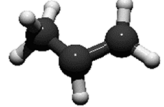
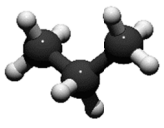
Density-Functional Theory Calculations. Our First-principles density-functional theory (DFT) calculations were performed using the Quantum-Espresso package.⁵ A semi-empirical addition of dispersive forces to conventional DFT⁶ was included in the calculation to account for van der Waals interactions. We used Vanderbilt-type ultrasoft pseudopotentials and the generalized gradient approximation (GGA) with the Perdew-Burke-Ernzerhof (PBE) exchange correlation. Due to the orientational disorder of the ligand, direct calculation on the **FJU-90** crystal structure is unfeasible. Therefore, we adopted simplified cluster models to evaluate the gas binding on the metal center. The metal center was cleaved from the periodic crystal structure of **FJU-90**, and put in a hexagonal, $20\text{\AA}\times 20\text{\AA}\times 20\text{\AA}$ supercell. The cluster model thus has a chemical formula of $[\text{Co}_3(\mu_3\text{-OH})(\text{HTrz})_3(\text{BA})_3(\text{Py})_3]^{2+}$, where HTrz = 1,2,4-triazole, BA = Benzoic acid, and Py = pyridine. Given that the $\mu_3\text{-OH}$ group could possible point to two different directions, two corresponding cluster models were built (mode A and mode B). For this cluster system, a cutoff energy of 544 eV and a $2\times 2\times 2$ k -point mesh (generated using the Monkhorst-Pack scheme) were found to be enough for total energy to converge within 0.01 meV/atom. The cluster model (with “+2” charge) was first fully optimized with respect to atomic coordinates. For gas adsorption, various possible binding configurations were considered and fully relaxed. The lowest-energy structures were identified as the optimal binding structures. To obtain the gas binding energies, a single gas molecule placed in a supercell with the same cell dimensions was also relaxed as a reference. The static binding energy (at $T = 0$ K) was calculated using: $E_B = E(\text{MOF}) + E(\text{gas}) - E(\text{MOF}+\text{gas})$.

Table S2. Crystallographic Data and Structural Refinement Summary.

Compound name	FJU-90
CCDC	1882901
Empirical formula	C ₄₇ H ₃₃ Co ₃ N ₁₃ O ₇ Cl ₂
Formula weight	1139.55
Temperature (K)	150
Crystal system	hexagonal
Space group	<i>P6₃/mmc</i>
<i>a</i> (Å)	16.90034(16)
<i>b</i> (Å)	16.90034(16)
<i>c</i> (Å)	18.7622(2)
α (°)	90
β (°)	90
γ (°)	120
Volume (Å ³)	4640.94(10)
<i>Z</i>	2
<i>D_c</i> (g cm ⁻³)	0.816
μ (mm ⁻¹)	4.431
F(000)	1084.0
Crystal size (mm ³)	0.15×0.15×0.25
Radiation	Cu-K α (λ = 1.54184Å)
Goodness-of-fit on F ²	1.069
Final <i>R</i> indexes [<i>I</i> >= 2 σ (<i>I</i>)] ^(a)	R ₁ = 0.0615, wR ₂ = 0.1727
Final <i>R</i> indexes [all data] ^(a)	R ₁ = 0.0655, wR ₂ = 0.1791

$$(a) R_1 = \frac{\sum ||F_o| - |F_c||}{\sum |F_o|}; wR_2 = \left[\frac{\sum w(|F_o|^2 - |F_c|^2)^2}{\sum w(F_o^2)} \right]^{1/2}$$

Table S3. Comparison of molecular sizes and physical properties of light hydrocarbons and CO₂.

Compounds	Ball and Stick model	Dimensions (Å ³)	Kinetic Diameter (Å)	Boiling point (K)
Carbon dioxide (CO ₂)		3.19×3.34×5.36	3.3	194.7
Acetylene (C ₂ H ₂)		3.32×3.34×5.70	3.3	189.3
Ethylene (C ₂ H ₄)		3.28×4.18×4.84	4.2	169.5
Ethane (C ₂ H ₆)		3.81×4.08×4.82	4.4	184.6
Propyne (C ₃ H ₄)		4.01×4.16×6.51	4.2	250.0
Propylene (C ₃ H ₆)		4.16×4.65×6.44	4.7	225.6
Propane (C ₃ H ₈)		4.02×4.52×6.61	5.1	231.1

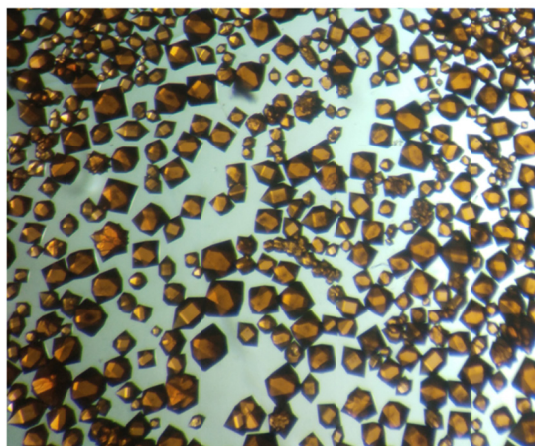


Figure S1. Optical photograph of the as-synthesized crystals of FJU-90.

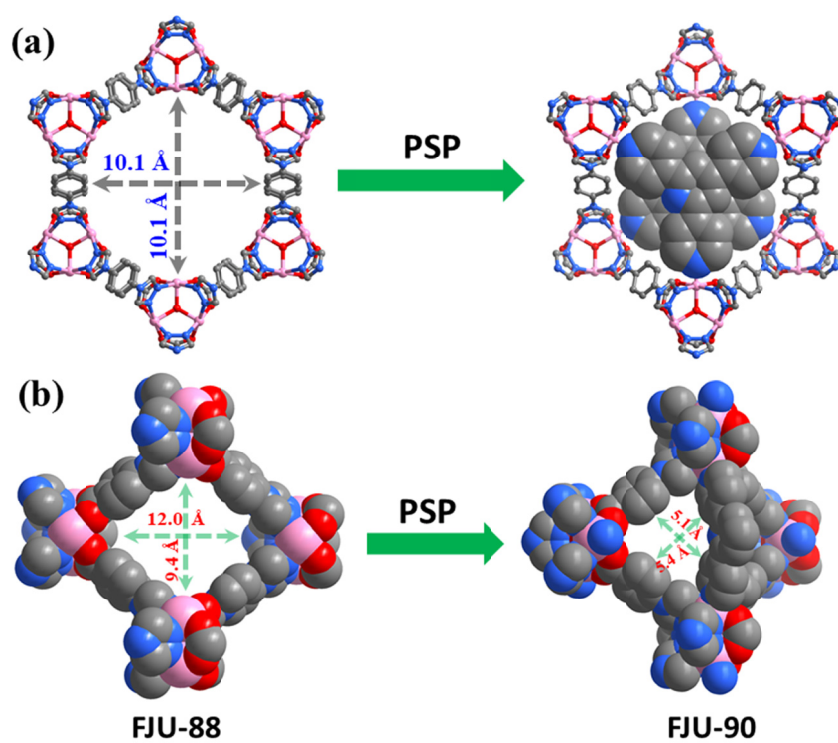


Figure S2. (a) Top and (b) side view of the pore geometry and aperture sizes before and after pore space partition (PSP).

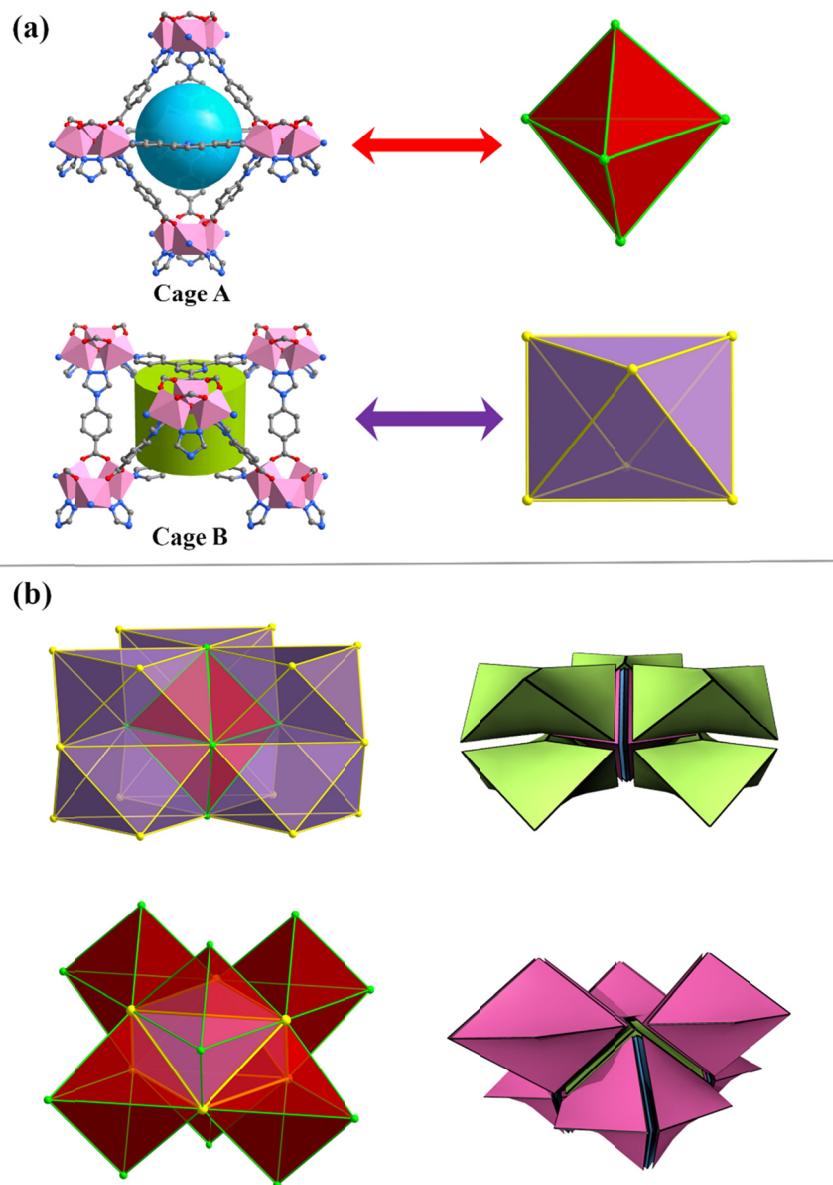


Figure S3. (a) The structure of the trigonal bipyramidal (Cage A) and trigonal antiprism (Cage B) (The hydrogen atoms are omitted from the structure for clarity) in **FJU-90**. (b) Cage A is linked by six Cage B through sharing six triangle faces; Cage B is linked by six Cage A by sharing six triangle faces (two Cage B within the top and bottom have been omitted for clarity); the corresponding Tiling network is displayed on the right.

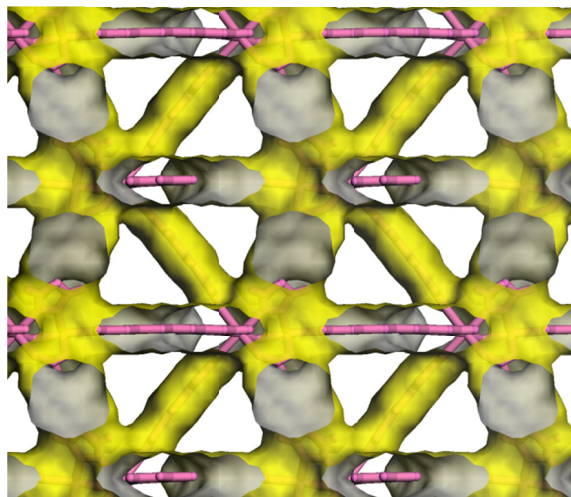


Figure S4. Pore surfaces of as-synthesized **FJU-90** viewed along the a -axis.

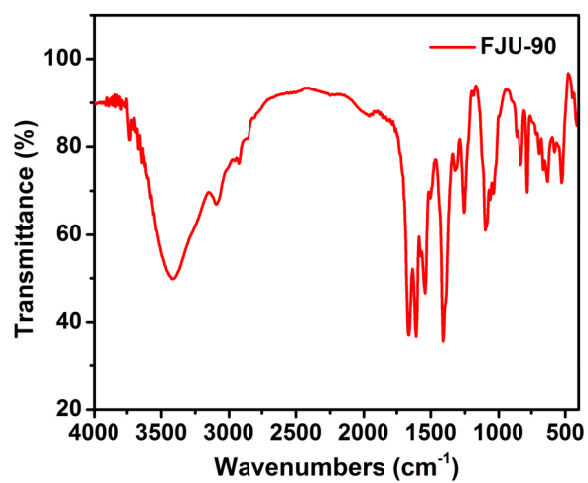


Figure S5. FT-IR spectrum of **FJU-90**.

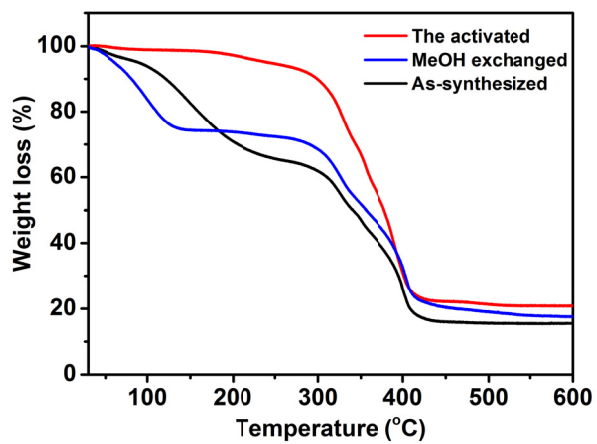


Figure S6. The TGA curves of **FJU-90**.

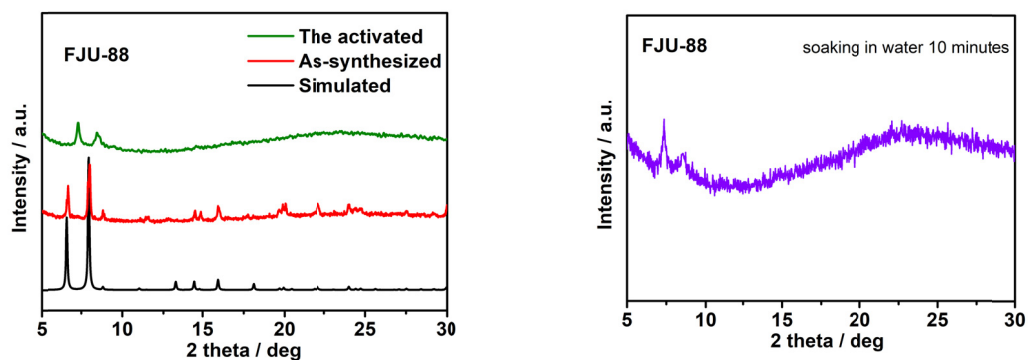


Figure S7. The powder X-ray diffraction patterns for **FJU-88**.

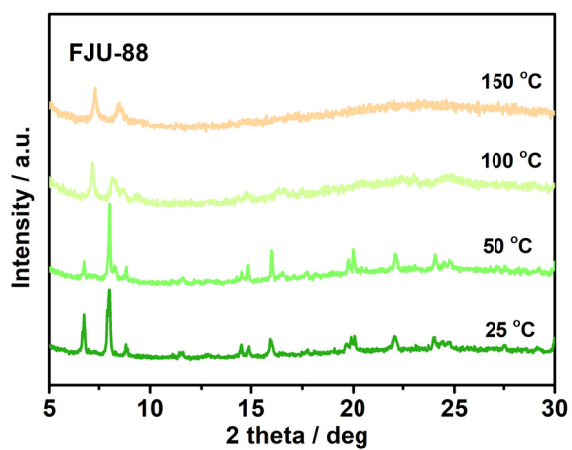


Figure S8. Variable-temperature powder X-ray diffraction patterns for **FJU-88**.

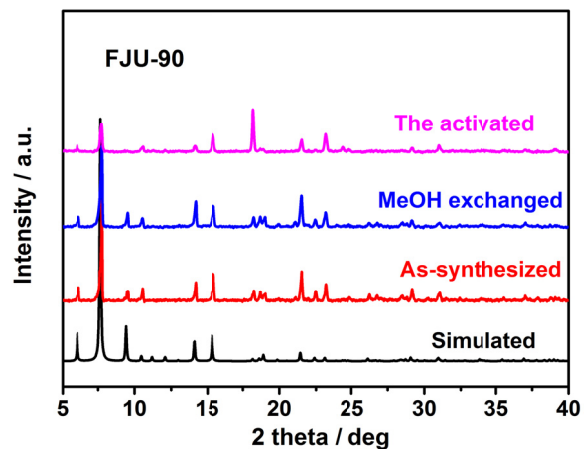


Figure S9. The powder X-ray diffraction patterns for **FJU-90** showing good agreement with simulated one for as-synthesized, MeOH exchanged and the activated samples.

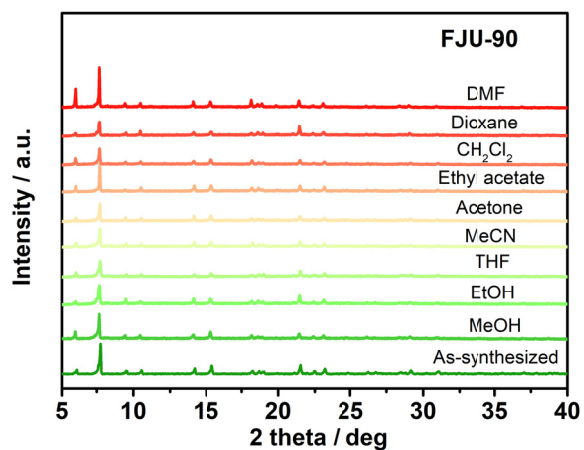


Figure S10. Powder X-ray diffraction patterns of **FJU-90** after soaking in various organic solvents.

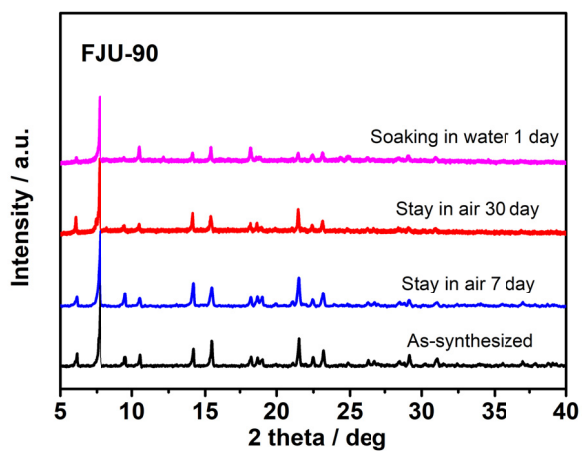


Figure S11. Powder X-ray diffraction patterns of FJU-90 stay in the air and soaking in the water.

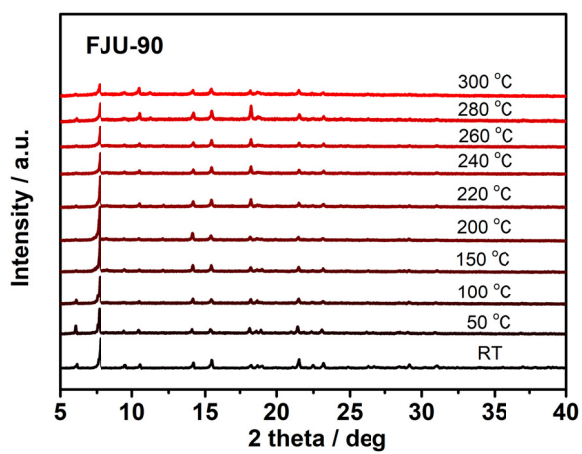


Figure S12. Variable-temperature powder X-ray diffraction patterns for FJU-90.

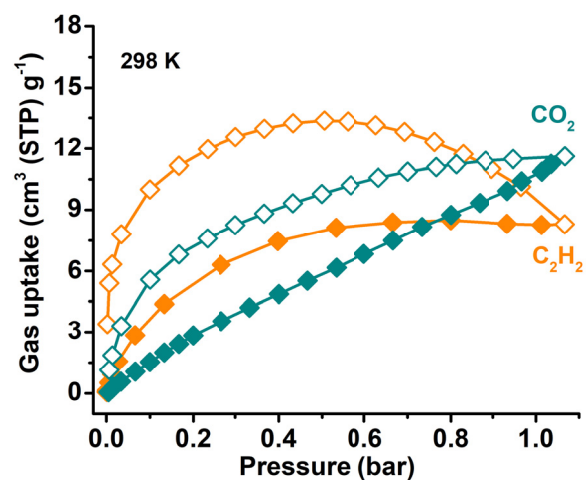


Figure S13. FJU-88a single-component adsorption (solid) and desorption (open) isotherms of C₂H₂ and CO₂ at 298 K and under 1 bar.

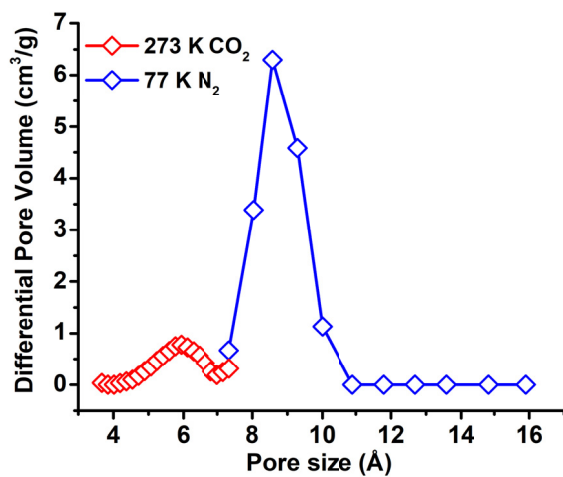


Figure S14. Pore size distribution of FJU-90a calculated by 273 K CO₂ and 77 K N₂ isotherms based on the NLDFT model.

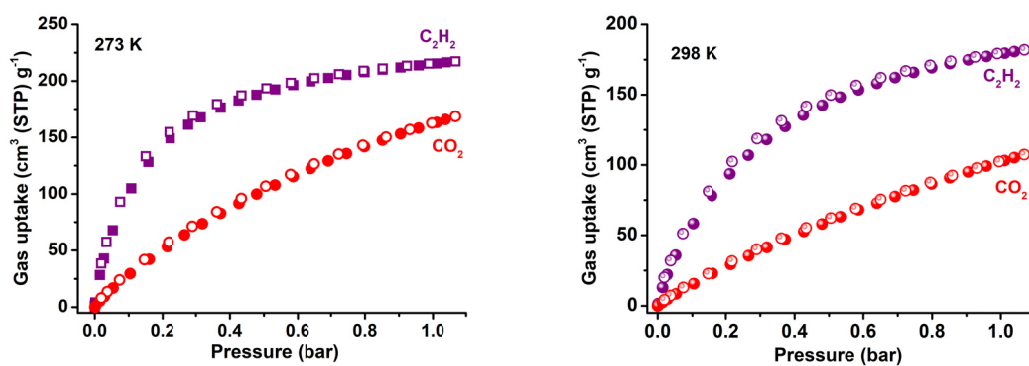


Figure S15. FJU-90a single-component adsorption (solid) and desorption (open) isotherms of C_2H_2 and CO_2 at 273 K and 298 K and under 1 bar.

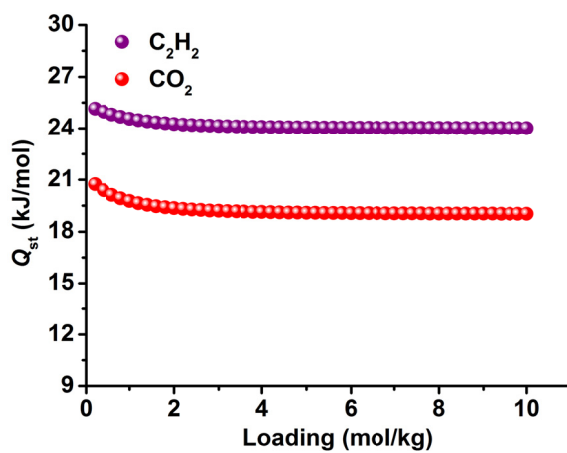


Figure S16. Heats of adsorption of both C_2H_2 and CO_2 in FJU-90a.

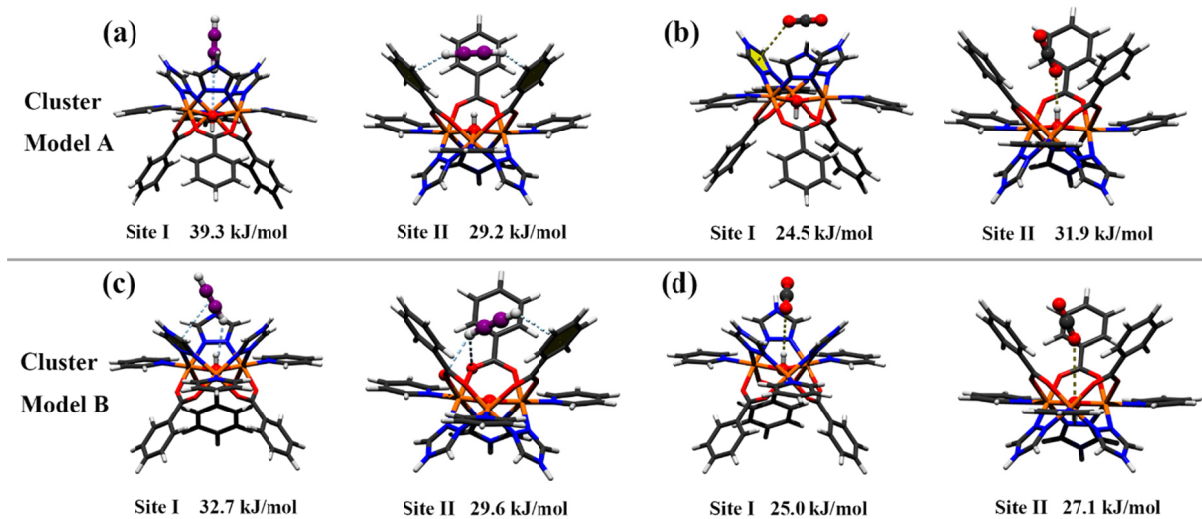


Figure S17. The DFT-calculated adsorption configurations of (a, c) C_2H_2 and (b, d) CO_2 around the metal center in FJU-90a, using a cluster model. (Cobalt, oxygen, nitrogen, carbon, and hydrogen atoms are in orange, red, blue, dark gray and white, respectively.)

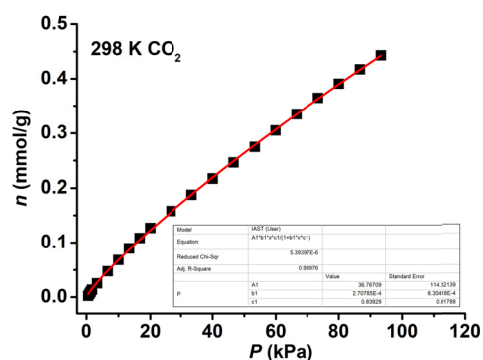
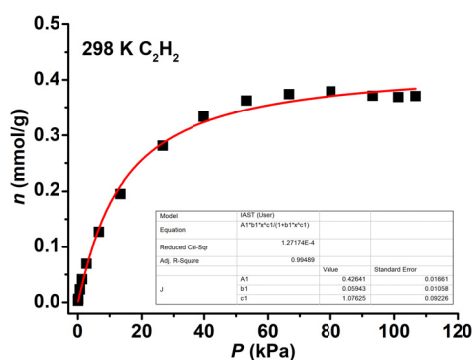


Figure S18. The graphs of the Single-site Langmuir-Freundlich equations fit for adsorption of C₂H₂ and CO₂ on FJU-88a at 298 K.

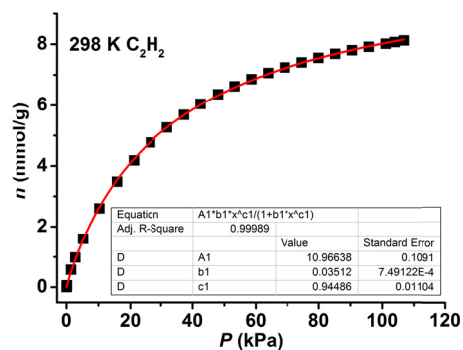
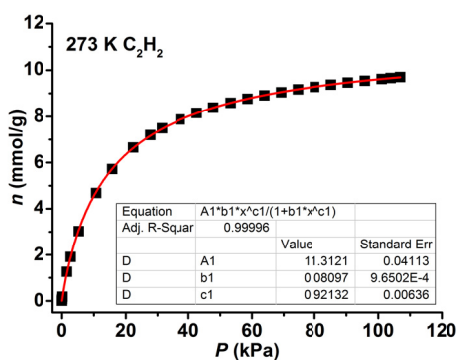


Figure S19. The graphs of the Single-site Langmuir-Freundlich equations fit for adsorption of C₂H₂ on FJU-90a at 273 and 298 K.

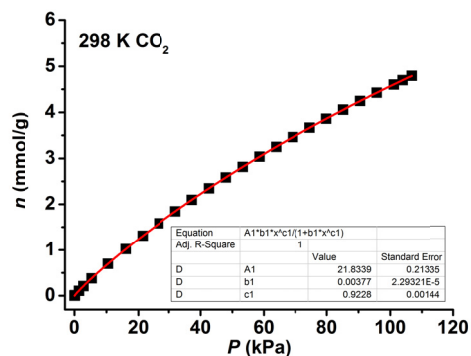
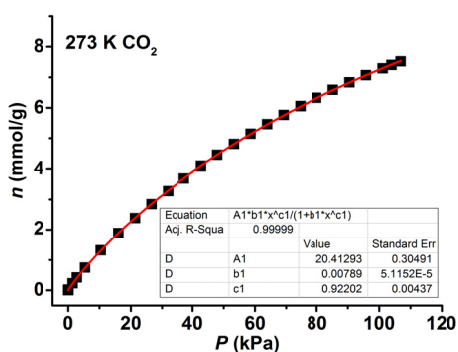


Figure S20. The graphs of the Single-site Langmuir-Freundlich equations fit for adsorption of CO₂ on FJU-90a at 273 and 298 K.

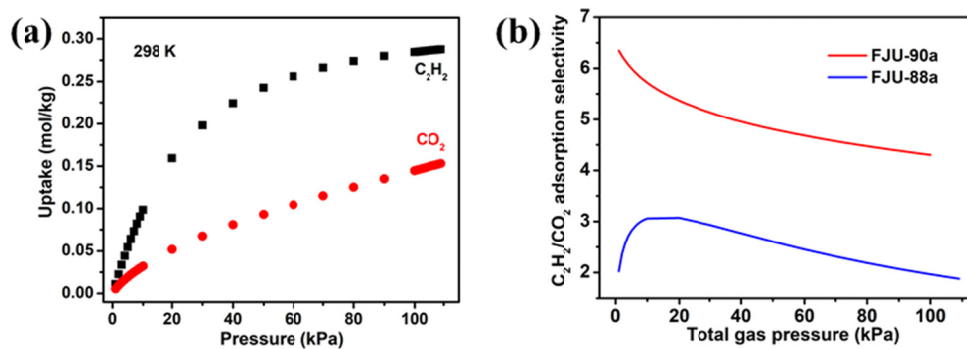


Figure S21. (a) IAST calculations of mixture adsorption isotherms of **FJU-88a** for equimolar C_2H_2/CO_2 gas mixtures at 298 K. (b) IAST adsorption selectivity for equimolar C_2H_2/CO_2 mixture in **FJU-88a** and **FJU-90a** at 298 K.

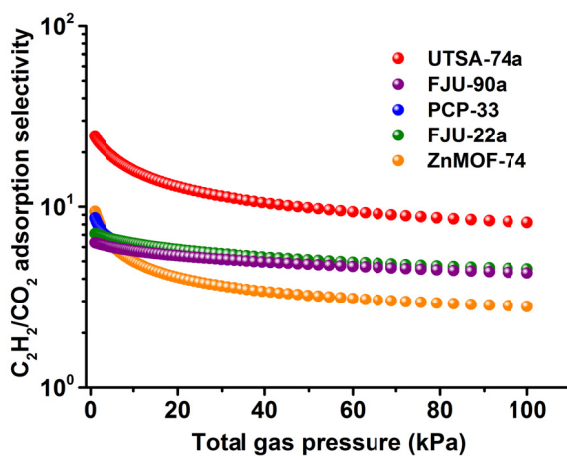


Figure S22. IAST adsorption selectivity of C_2H_2/CO_2 in an equimolar mixture among **FJU-90a** and other MOFs at 298 K.

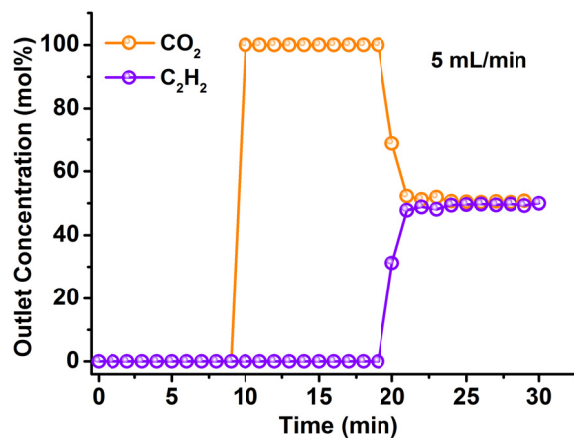


Figure S23. Experimental column breakthrough curve for equimolar C₂H₂/CO₂ mixtures (298 K, 1 bar, gas flow: 5 mL/min) in a fixed-bed packed with **FJU-90a**.

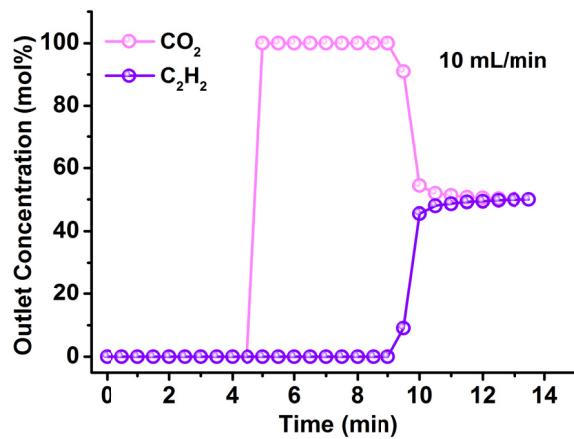


Figure S24. Experimental column breakthrough curve for equimolar C₂H₂/CO₂ mixtures (298 K, 1 bar, gas flow: 10 mL/min) in a fixed-bed packed with **FJU-90a**.

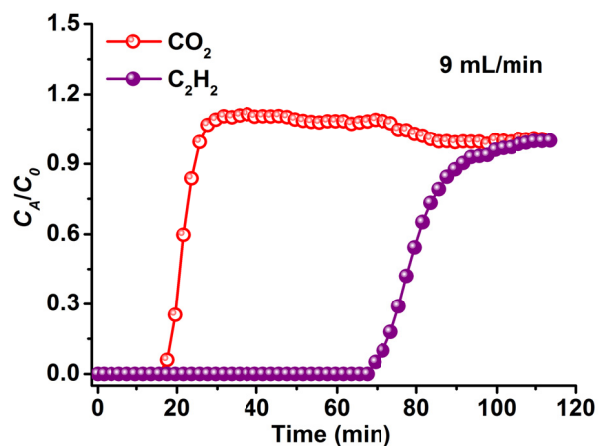


Figure S25. Experimental column breakthrough curve for $C_2H_2/CO_2/He$ (5/5/90, v/v/v) mixtures (298 K, 1 bar, gas flow: 9 mL/min) in a fixed-bed packed with **FJU-90a**.

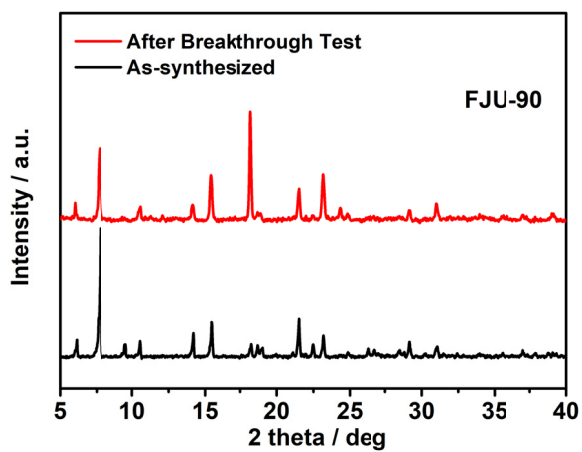


Figure S26. PXRD patterns of **FJU-90** after breakthrough tests.

Supplementary References

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