

Beyond Crystal Engineering: Significant Enhancement of C₂H₂/CO₂ Separation by Constructing Composite Material

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Supporting Information

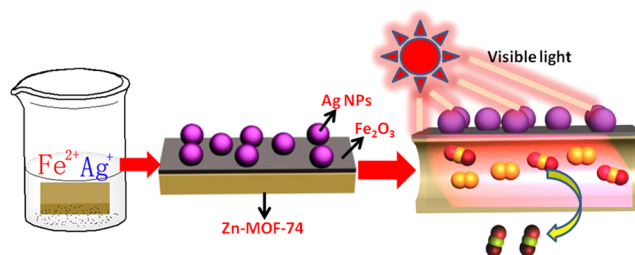
ABSTRACT: Different from the established crystal engineering method for enhancing gas-separation performance, we demonstrate herein a distinct approach. In contrast to the pristine MOF (metal–organic framework) material, the C₂H₂/CO₂ separation ability for the resultant Ag NPs (nanoparticle)@Fe₂O₃@MOF composite material, estimated from breakthrough calculations, is greatly enhanced by 2 times, and further magnified up to 3 times under visible light irradiation.

The rich potential of metal–organic frameworks (MOFs) for separating a wide variety of gaseous mixtures is the subject of intensive research in the published literature.^{1–4} In particular, some difficult separations such as C₂H₂/CO₂ and C₂H₂/C₂H₄ mixtures, mainly due to their comparable size and physical nature, are highly interesting but remain a challenging task.^{5–10} To this end, several approaches based on crystal engineering techniques relying on precise molecule design have been attested to show outstanding separation performance;^{5–10} however, there is still no report by using simple physical or chemical methods, especially using light,^{11,12} to enhance gas separation, which inherently is expected to enable general applicability beyond crystal engineering techniques.

To seek a possible solution, we draw a protocol, as shown in Scheme 1. The considerations are listed as follows. (i) Ag NPs can give a selective reaction with C₂H₂ to generate π -complexation formation¹³ and thus afford preferable adsorption to C₂H₂. (ii) The Ag NP is one of the best NPs to render a plasmon-driven photothermal effect.¹⁴ To meet the industrial demand of large-scale production, we herein launched a modified coprecipitation method to prepare Ag NPs@MOF composites in a rapid and in situ manner. After carrying out C₂H₂ and CO₂ adsorption studies, we found that the C₂H₂/CO₂ separation ability in the resultant Ag NPs@Fe₂O₃@MOF materials is significantly enhanced, relative to the pristine MOF material.

In the literature, the coprecipitation method has been developed to prepare oxide-supported noble-metal catalysts such as Ag, Au, Pd, or Pt@Fe₂O₃ composites, due to its convenience, low cost, and high-yield fabrication.¹⁵ However, we also note some limits for such methods such as additional high-temperature treatment above 400 °C that is beyond the heat endurance for most MOFs and reduction by hot hydrogen that would add potential danger. Very recently, we launched a surface-enriching method to give an in situ and rapid preparation

Scheme 1. A Draft of Modified Coprecipitation Method for Preparation of Ag NPs@Fe₂O₃@MOF Composite and Schematic Illustration of Photoinduced Enhancement of C₂H₂/CO₂ Separation, Where Due to a Preferential Adsorption of C₂H₂ over CO₂ from Ag NPs the Released Amount of Guest Molecule Caused by Plasmon-Driven Photothermal Effect under Visible Light Irradiation Is Different for C₂H₂ and CO₂ Molecules



of the Fe₂O₃@MOF composite, due to a unique surface reaction between Fe³⁺ and the MOF substrate.^{16,17} Further, the lower potential of Fe²⁺ (0.771 V), relative to Ag⁺ (0.799 V), agrees with the thermodynamic reduction of Ag⁺ to Ag⁰ by Fe²⁺ ions. Taking the above discussions into account, we propose here a modified coprecipitation method to prepare Ag NPs@Fe₂O₃@MOF composites (Scheme 1).

The materials were synthesized by stirring the solution of AgNO₃ and FeSO₄ in a ratio of 1:1 with the addition of 150 mg of Zn-MOF-74 within 1 min. Dependent on the different concentrations of AgNO₃ (100, 500, and 1000 ppm) in this reaction system, composites with a loading of 0.1 wt % Ag@2.2 wt % Fe₂O₃, 0.31 wt % Ag@3.3 wt % Fe₂O₃, and 0.44 wt % Ag@4.4 wt % Fe₂O₃ were obtained and are respectively named Ag@Fe₂O₃@Zn-MOF-74-I (*ab. I*), Ag@Fe₂O₃@Zn-MOF-74-II (*ab. II*), and Ag@Fe₂O₃@Zn-MOF-74-III (*ab. III*). The Ag NPs and Fe₂O₃ contents are determined by ICP-OES (inductively coupled plasma optical emission spectrometry).

Morphologies of the resulted samples were characterized by both scanning electron microscopy (SEM, Figure S1a, b, and c) and transmission electron microscopy (TEM, Figure S1d, e, and f). It is clear that Ag NPs and Fe₂O₃ are successfully loaded on the surface of Zn-MOF-74, and the content of Ag NPs and Fe₂O₃ increases along with the increasing concentration of AgNO₃. The

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TEM images show near-spherical Ag NPs with a size of ~ 20 nm. A close examination using high-resolution TEM (HRTEM, Figure S1g, h, and i) confirms a crystalline character with a lattice spacing of 0.25 nm, comparable with the typical lattice fringe of Ag NPs (d_{111}).¹⁸ Note that, as shown in Figure S1i, a multilevel structure with an obvious outline is observed in the resulted Ag@Fe₂O₃@Zn-MOF-74-III samples, suggesting the coprecipitation of Ag NPs with Fe₂O₃, rather than direct enrichment of Ag NPs on the MOF substrate during the generation of such products.

The loading of Ag NPs and Fe₂O₃ is further confirmed by XPS (X-ray photoelectron spectroscopy) and powder X-ray diffraction (PXRD). The spectra of Ag 3d show the 3d_{3/2} and 3d_{5/2} signals at 374.5 and 368.5 eV (Figure S2), respectively, belonging to a typical character of metallic (zerovalent) silver,¹⁸ while the XPS spectra of Fe 2p displays four peaks, Fe 2p_{2/3}, Fe 2p_{1/2}, and their satellites, centering at 711.5, 718.7, 725.2, and 733.8 eV (Figure S3), respectively, in accordance with the electronic state of α -Fe₂O₃.^{16,17} In the PXRD patterns (Figure 1a), not only

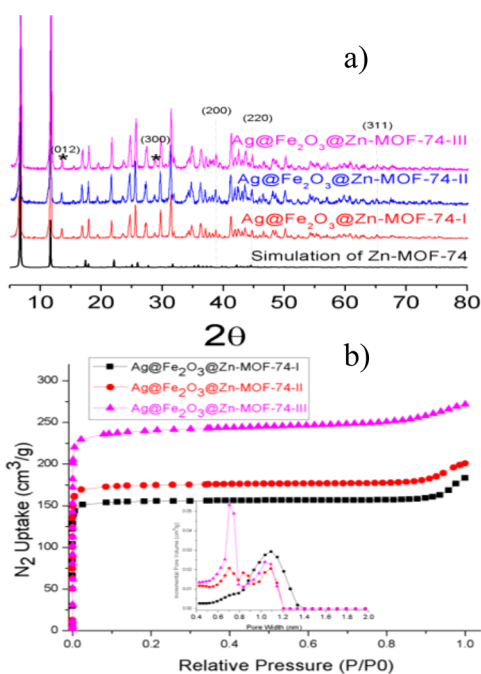


Figure 1. (a) Simulated PXRD patterns of Zn-MOF-74 and experimental PXRD patterns of samples I, II, and III. The highlight by “*” and dashed present characteristic Bragg peaks of α -Fe₂O₃ and Ag NPs, respectively. (b) N₂ adsorption isotherms of samples I, II, and III at 77 K. The insert is their pore size distribution.

Bragg peaks observed in the resulted samples match well with the simulated data of Zn-MOF-74, suggesting good maintenance of the MOF substrate, but also some detectable signs characterized to be Ag NPs such as (200), (220), and (311)¹⁸ and α -Fe₂O₃ such as (012) and (300) are observed.^{16,17} Their porosities are investigated by N₂ adsorption at 77 K, and the results are shown in Figure 1b, giving a microporous type I curve. BET surface areas are 597, 689, and 936 cm²/g, respectively, comparable with the reported value (747 cm²/g)¹⁹ for Zn-MOF-74. The pore size distributions of these materials are also analyzed, comparable with the reported value in Zn-MOF-74.¹⁹ Furthermore, their light absorbencies are tested by UV-vis spectra (Figure S4). In contrast to the pristine Zn-MOF-74, the samples with increasing Ag content afford significantly increased absorbability at 400–800 nm, due to a characteristic contribution from Ag NPs.¹⁴

To confirm our concept, we carried out systemic gas-adsorption studies on these resultant composites. The C₂H₂ and CO₂ adsorption in the dark at 293 K is measured and shown in Figure S5. The C₂H₂ uptake capacity at 100 kPa is 135, 146, and 150 cm³/g for materials I, II, and III, respectively. In comparison to the pristine Zn-MOF-74 giving 124 cm³/g,²⁰ it is clear that increasing the Ag content benefits the enhancement of C₂H₂ uptake with the biggest increase up to 21%. As expected, the opposite trend is observed for CO₂ uptake, and materials I, II, and III only afford 100, 117, and 115 cm³/g of CO₂ uptake at 100 kPa, respectively, less than corresponding value of 120 cm³/g for Zn-MOF-74.²⁰ Accordingly, the difference between C₂H₂ and CO₂ adsorption, as shown in Figure S5, is 35, 29, and 35 cm³/g, respectively. Notably, the value (35 cm³/g) is almost 9 times bigger than that observed for pristine Zn-MOF-74 (just 4 cm³/g), indicative of large enhancement of C₂H₂ selectivity over CO₂ via Ag loading. Most importantly, although a decrease in both C₂H₂ and CO₂ adsorption capacity is observed for these Ag-loaded materials due to the plasmon-driven photothermal effect under visible light irradiation, however, some discrepancy for such a decrease is also observed. And thereby the difference in C₂H₂ and CO₂ adsorption is increased to be 37, 35, and 39 cm³/g, respectively, strongly suggesting that such a plasmon-driven photothermal effect enables distinct release for various guest molecules and further enhances adsorption selectivity.

To confirm the above claim, the C₂H₂/CO₂ selectivity for the materials I, II, and III in the dark and Vis is estimated by ideal adsorbed solution theory (IAST) calculations.²⁰ In contrast to the selectivity ($S_{\text{ads}} = 2.61$) of Zn-MOF-74 at 100 kPa and room temperature, the selectivity for the Ag-loaded materials is improved to be 2.88, 3.21, and 3.33 in the dark and further increased up to 4.35, 4.37, and 4.73 under Vis irradiation, respectively (Figure 2a and b). In this regard, materials III under Vis irradiation afford the highest adsorption selectivity, almost 2 times bigger than that for Zn-MOF-74. Such selectivity is also compared with UTSA-74,²⁰ one of the best established candidates for C₂H₂/CO₂ separation. We note that the selectivity of Ag@Fe₂O₃@Zn-MOF-74-III under Vis is lower than that of UTSA-74. However, as stressed in the literature,²¹ C₂H₂/CO₂ separations in fixed bed adsorbers are also dictated by C₂H₂ uptake capacities. Figure 2c and d present the IAST calculations of the C₂H₂ uptake capacity for a 50:50 C₂H₂/CO₂ mixture at 293 K for materials I, II, and III in the dark and in the Vis, Zn-MOF-74, and UTSA-74, respectively. Generally speaking, the C₂H₂ uptake capacity increases with increasing content of Ag. The highest C₂H₂ uptake capacity is achieved with materials III under a Vis trigger; its uptake capacity is compared in Figure 2d with UTSA-74 and Zn-MOF-74, significantly higher, by 2 times, than that of UTSA-74 and Zn-MOF-74.

The performance of industrial fixed bed adsorbers is dictated by a combination of adsorption selectivity and uptake capacity.²¹ To properly weigh the selectivity and capacity metrics for evaluation of materials I, II, and III in the application of C₂H₂/CO₂ separation, we performed transient breakthrough simulations using the simulation methodology described in the literature.²⁰ Figure 2e presents the transient breakthrough simulations for separation of an equimolar C₂H₂/CO₂ mixture with partial pressures of 50 kPa by materials III under Vis. During the initial transience, the effluent gas contains pure CO₂, and this continues until C₂H₂ starts breaking through because its uptake capacity has been reached.

Longer breakthrough times of C₂H₂ are desirable because it reduces the frequency of regenerations. Regeneration costs are

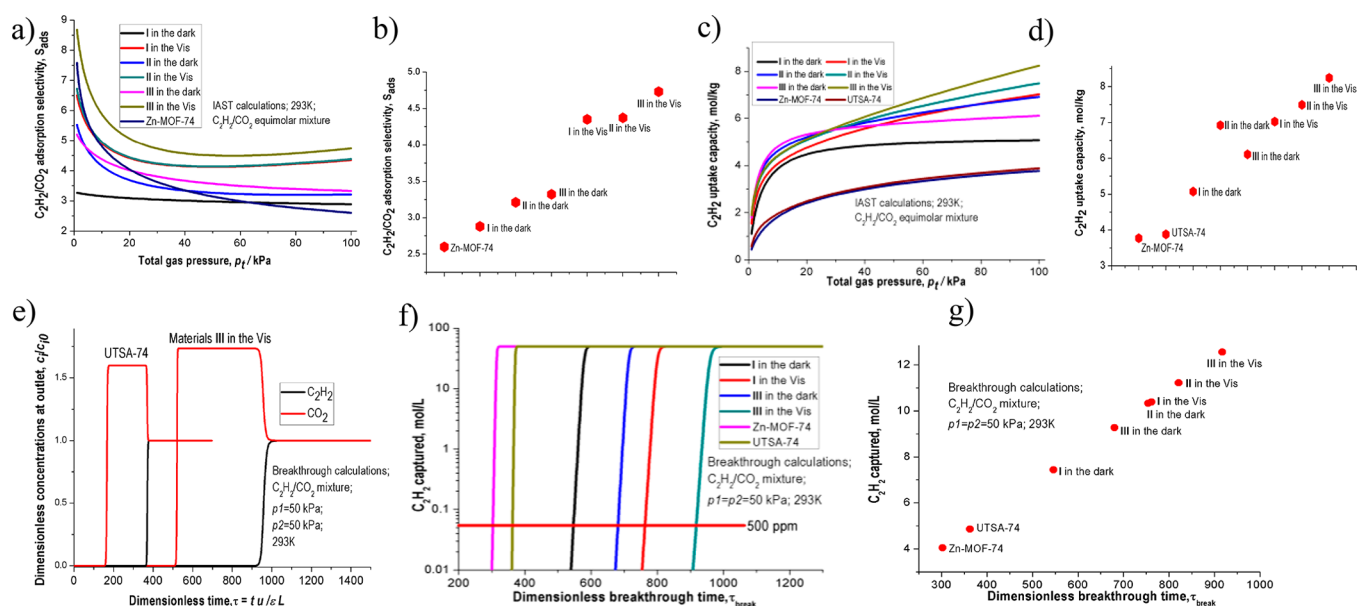


Figure 2. (a) IAST calculations of the adsorption selectivity, S_{ads} , for separation of 50/50 $\text{C}_2\text{H}_2/\text{CO}_2$ mixture at 293 K for materials I, II, and III in the dark and Vis, and Zn-MOF-74, respectively. (b) A comparison of S_{ads} for these materials at 293 K and 100 kPa. (c) IAST calculations of the C_2H_2 uptake capacity for 50/50 $\text{C}_2\text{H}_2/\text{CO}_2$ mixture at 293 K for materials I, II, and III in the dark and Vis, UTSA-74, and Zn-MOF-74, respectively. (d) A comparison of IAST calculations of the C_2H_2 uptake capacity for these materials at 293 K and 100 kPa. (e) Transient breakthrough simulations for separation of equimolar $\text{C}_2\text{H}_2/\text{CO}_2$ mixture with partial pressures of 50 kPa each using materials III in the Vis and UTSA-74. (f) Comparison of % C_2H_2 in the exit gas from packed beds plotted as a function of the dimensionless time using materials I and III in the dark and Vis, Zn-MOF-74, and UTSA-74. (g) Comparison of the moles of C_2H_2 captured per liter of material during the interval for which the product gas is 99.95% CO_2 , plotted as a function of the dimensionless breakthrough time, τ_{break} .

the major contributors to energy use in fixed bed operations. We note that the breakthrough of C_2H_2 for UTSA-74 occurs at a dimensionless time that is half the value of that for materials III under Vis. The reason, as evidenced from Figure 2c, is that the C_2H_2 uptake capacity of materials III under Vis is about 1 times higher than that of UTSA-74.

A comparison of % C_2H_2 in the exit gas for beds packed with materials I, II, and III in the dark and Vis, plotted as a function of the dimensionless time, is also calculated, where the breakthrough times are longer with increasing Ag content, because the C_2H_2 uptake capacity increases with increasing content of Ag (Figure 2f). Moreover, a similar comparison among materials I, II, and III in the dark and Vis, UTSA-74, and Zn-MOF-74 is presented as Figure 2f and g. Notably, even in the dark, the breakthrough times with materials I are significantly higher than with UTSA-74, and Zn-MOF-74. As described in the literature,²⁰ the impurity level of acetylene in the gas mixture exiting the fixed-bed packed with materials I, II, and III in the dark and Vis, UTSA-74, and Zn-MOF-74 is calculated. We define the breakthrough time, τ_{break} , as the time at which the exit gas contains $<0.05\% = 500$ ppm of C_2H_2 . The amount of C_2H_2 captured during the time interval $0 - \tau_{\text{break}}$ can be determined from a material balance and is expressed as moles of C_2H_2 captured per liter of framework material against τ_{break} . Accordingly, the values of τ_{break} have the following hierarchy, Zn-MOF-74¹⁵ < UTSA-74¹⁵ < materials I in the dark < ... < materials III in the Vis, strongly suggesting superior application in $\text{C}_2\text{H}_2/\text{CO}_2$ separation for these Ag-loaded materials, especially these in the Vis trigger. Note that our performance also exceeds other reported porous materials such as HOF-3,²² ZJU-60a,²³ PCP-33,²⁴ and [Mn(bdc)(dpe)].²⁵

In conclusion, we have shown a highly effective and facile method beyond crystal engineering to enhance the gas-

separation ability of MOF. The results show that loading Ag on Zn-MOF-74 helps to increase C_2H_2 adsorption capacity, leading to enhanced $\text{C}_2\text{H}_2/\text{CO}_2$ adsorption selectivity and separation performance. Meanwhile, the plasmon-driven photo-thermal effect under visible light irradiation further enhances $\text{C}_2\text{H}_2/\text{CO}_2$ adsorption selectivity and separation performance, demonstrating a potentially low energy strategy by using visible light as a driving force for modulating gas separation.

■ ASSOCIATED CONTENT

📄 Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.inorgchem.8b00341.

Material involved in synthesis and additional figures (PDF)

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Notes

The authors declare no competing financial interest.

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Supporting information

Beyond Crystal Engineering: Significant Enhancement of C₂H₂/CO₂ Separation by Constructing Composite Material

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Experimental detail.

Synthesis of Zn-MOF-74. A mixture of Zn(NO₃)₂·6H₂O (0.0604 g, 0.203 mmol), 2,5-dihydroxy terephthalic acid (0.0191 g, 0.096 mmol), N,N-dimethylformamide (DMF) (2ml), isopropyl alcohol (0.1 mL) and H₂O (2 mL) was placed in a closed 25 ml Teflon reactor and heated at 105°C for 1200 min, in turn cooled to room temperature, produced brown needle-shaped crystals were got and dried in 71 % yield (based on Zn) at room temperature.

Synthesis of materials I, II and III. 150 mg Zn-MOF-74 samples were added into a solution (H₂O, 10 mL) containing 1 mL FeSO₄ (100 ppm, 500 ppm, and 1000 ppm, respectively) and 1 mL AgNO₃ (100 ppm, 500 ppm, and 1000 ppm, respectively) to stir for one minute at room temperature and ambience, then the resulted solid samples were separated by centrifugal separation, and washed three times by distilled water, next dried naturally.

Materials and general methods.

All the reagents used in this work are purchased from Alfa without any purification. X-ray powder diffraction were collected by a Bruker AXSD8 Discover powder diffractometer at 40 kV, 40 mA for Cu K α , ($\lambda = 1.5406\text{\AA}$). The simulated powder patterns were calculated by Mercury 1.4. The purity of the bulk products were determined

by comparison of the simulated and experimental PXRD patterns. SEM measurements were carried out using a Oxford X-max microscope. XPS experiments were performed in a Theta probe (Thermo Fisher) using monochromated Al K α x-rays at $h\nu=1486.6$ eV.

The gas sorption isotherms were collected on a Belsorp-max. Ultrahigh-purity-grade (>99.999%) C₂H₂ and CO₂ gases were used in this adsorption measurement. To maintain the experimental temperatures liquid nitrogen (77 K), and water bath (293 K) were used respectively.

Before carrying out adsorption experiments, the as-synthesized samples (150 mg) were immersed in CH₃OH for three days, then degassed automatically in Belsorp-max at 60°C for 24 h to generate the activated samples.

The adsorption data in the dark is obtained based on the samples enwrapped by foil at the exterior, while the adsorption data in the Vis is obtained based on the samples with continuous Vis irradiation.

The Vis irradiation is carried out by Mejiro Genossen MVL-210 (3.5 W/cm²). The distance between the light source and samples is about 80 cm.

Fitting of pure component isotherms.

The pure component isotherm data for C₂H₂ measured at 293 K in these Ag@Fe₂O₃@Zn-MOF-74 materials, in the dark and Vis, were fitted with the dual-site Langmuir model

$$q = q_{A,sat} \frac{b_A p}{1 + b_A p} + q_{B,sat} \frac{b_B p}{1 + b_B p} \quad (1)$$

The pure component isotherm data for CO₂ measured at 293 K in these Ag@Fe₂O₃@Zn-MOF-74 materials, in the dark and Vis,, were fitted with the single-site Langmuir model

$$q = q_{sat} \frac{b_A p}{1 + b_A p} \quad (2)$$

The fitted parameter values are presented in Table 1, and Table 2.

Table S1. Dual-site Langmuir parameter fits for C₂H₂ and single-site Langmuir parameter fits for CO₂ in these Ag@Fe₂O₃@Zn-MOF-74 materials in the dark.

$q = q_{A,sat} \frac{b_A p}{1 + b_A p} + q_{B,sat} \frac{b_B p}{1 + b_B p}$		Site A		Site B	
		$q_{A,sat}$ mol/kg	b_A Pa ⁻¹	$q_{B,sat}$ mol/kg	b_B Pa ⁻¹
Materials I	C ₂ H ₂	7.0	3.93×10 ⁻⁴		

Materials II	C ₂ H ₂	10.0	7.38×10 ⁻⁶	6.0	9.19×10 ⁻⁴
Materials III	C ₂ H ₂	6.9	7.37×10 ⁻⁴	5.0	4.11×10 ⁻⁶
Materials I	CO ₂	7.4	1.13×10 ⁻⁴		
Materials II	CO ₂	9.2	1.02×10 ⁻⁴		
Materials III	CO ₂	8.8	1.07×10 ⁻⁴		

Table S2. Dual-site Langmuir parameter fits for C₂H₂ and single-site Langmuir parameter fits for CO₂ in these Ag@Fe₂O₃@Zn-MOF-74 materials with Vis light.

$q = q_{A,sat} \frac{b_A p}{1 + b_A p} + q_{B,sat} \frac{b_B p}{1 + b_B p}$		Site A		Site B	
		$q_{A,sat}$ mol/kg	b_A Pa ⁻¹	$q_{B,sat}$ mol/kg	b_B Pa ⁻¹
Materials I	C ₂ H ₂	10.3	1.07×10 ⁻⁵	4.9	9.17×10 ⁻⁴
Materials II	C ₂ H ₂	12.0	9.36×10 ⁻⁶	5.2	1.07×10 ⁻³
Materials III	C ₂ H ₂	30.0	3.63×10 ⁻⁶	5.0	1.22×10 ⁻³
Materials I	CO ₂	8.0	8.19×10 ⁻⁵		
Materials II	CO ₂	8.4	9.21×10 ⁻⁵		
Materials III	CO ₂	9.0	7.09×10 ⁻⁵		

IAST calculations of adsorption selectivities.

We consider the separation of binary C₂H₂/CO₂ mixtures. The adsorption selectivity for C₂H₂/CO₂ separation is defined by

$$S_{ads} = \frac{q_1/q_2}{p_1/p_2} \quad (3)$$

q_1 , and q_2 are the molar loadings in the adsorbed phase in equilibrium with the bulk gas phase with partial pressures p_1 , and p_2 .

Transient breakthrough simulations.

Transient breakthrough of C₂H₂/CO₂ mixtures in fixed bed adsorbers.

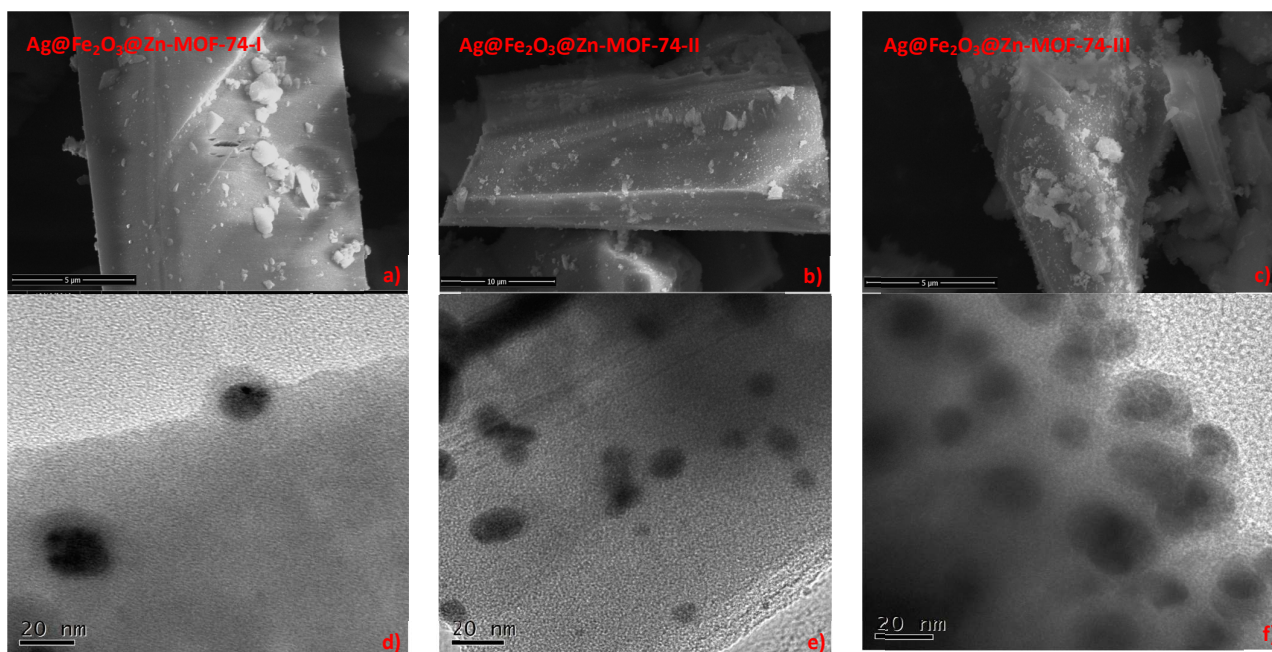
For the breakthrough simulations, the following parameter values were used: length of packed bed, $L = 0.3$ m; voidage of packed bed, $\varepsilon = 0.4$; superficial gas velocity at inlet, $u = 0.04$ m/s.

The total bulk gas phase is at setted temperature and 100 kPa. The partial pressures of C₂H₂, and CO₂ in the inlet feed gas mixture are, respectively, $p_1 = 50$ kPa, $p_2 = 50$ kPa. The transient breakthrough simulation results are

presented in terms of a *dimensionless* time, τ (x -axis), defined by dividing the actual time, t , by the characteristic time, $\frac{L\varepsilon}{u}$. The y -axis is the dimensionless concentrations at the outlet of the adsorber, normalized with respect to the inlet feed concentrations.

Table S3. Breakthrough calculations for separation of 50/50 C₂H₂/CO₂ mixture.

	Dimensionless breakthrough time τ_{break}	C ₂ H ₂ adsorbed during 0 - τ_{break} (mol L ⁻¹)
Materials I in the Vis	762	10.39
Materials II in the Vis	821	11.22
Materials III in the Vis	917	12.56
Materials I in the dark	546	7.44
Materials II in the dark	754	10.33
Materials III in the dark	680	9.28
UTSA-74	362	4.86
Zn-MOF-74	303	4.06



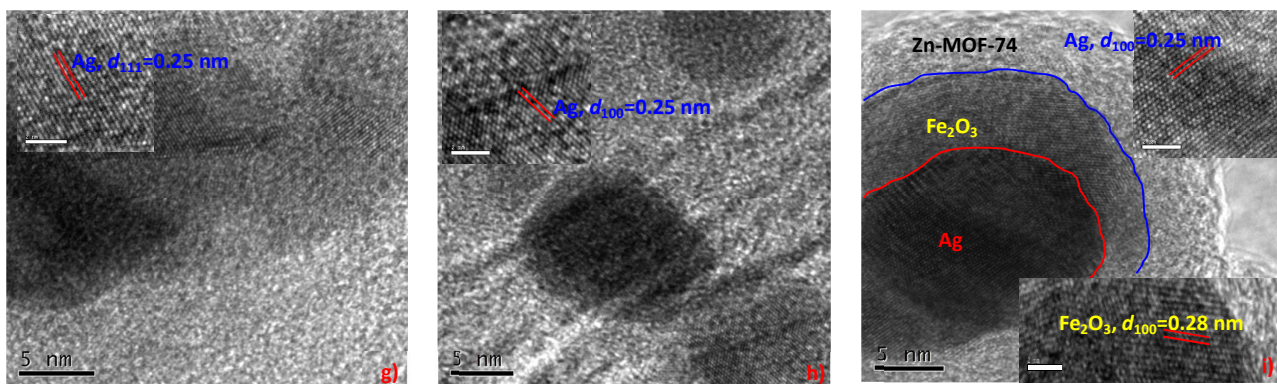


Figure S1. SEM images of a) samples I, b) samples II, and c) samples III. TEM images of d) samples I, e) samples II, and f) samples III. HRTEM images of g) samples I, h) samples II, and i) samples III. The inserts are corresponding FFT images.

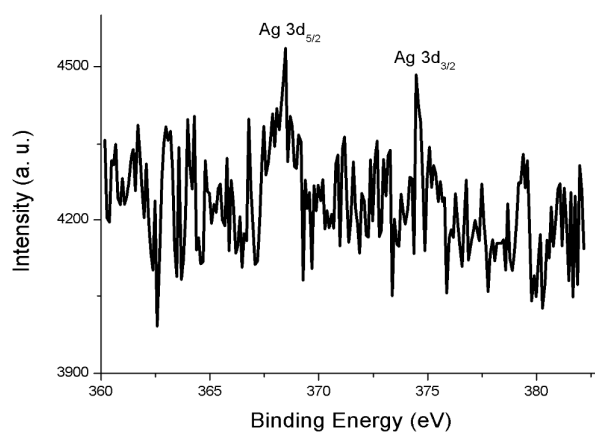


Figure S2. XPS spectroscopy of Ag@Fe₂O₃@Zn-MOF-74-III. Ag_{3d} for Ag NPs in the present composite.

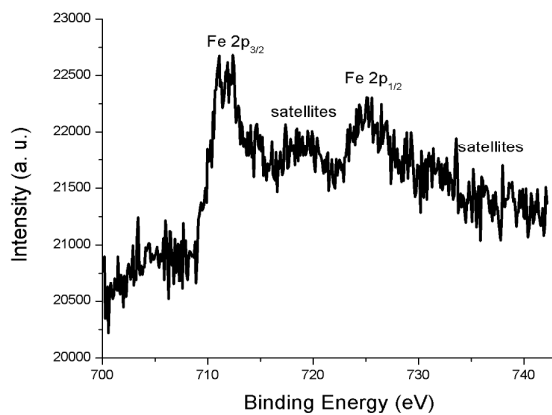


Figure S3. XPS spectroscopy of Ag@Fe₂O₃@Zn-MOF-74-III. Fe_{2p} for Fe₂O₃ in the present composite.

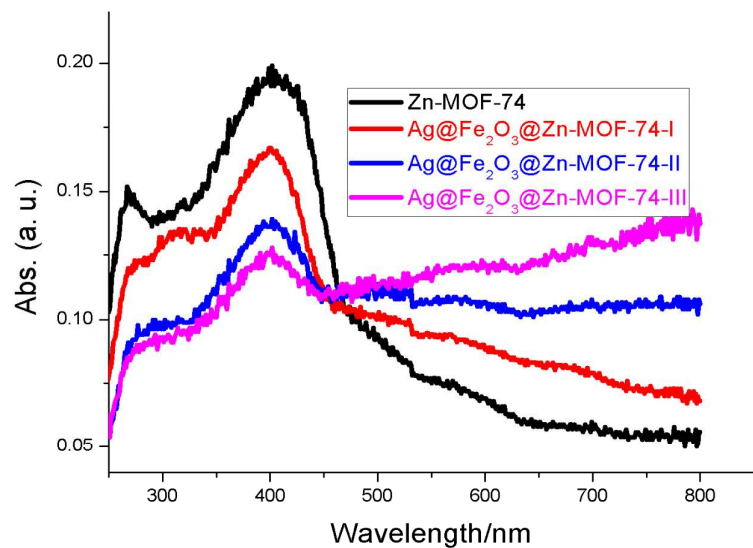
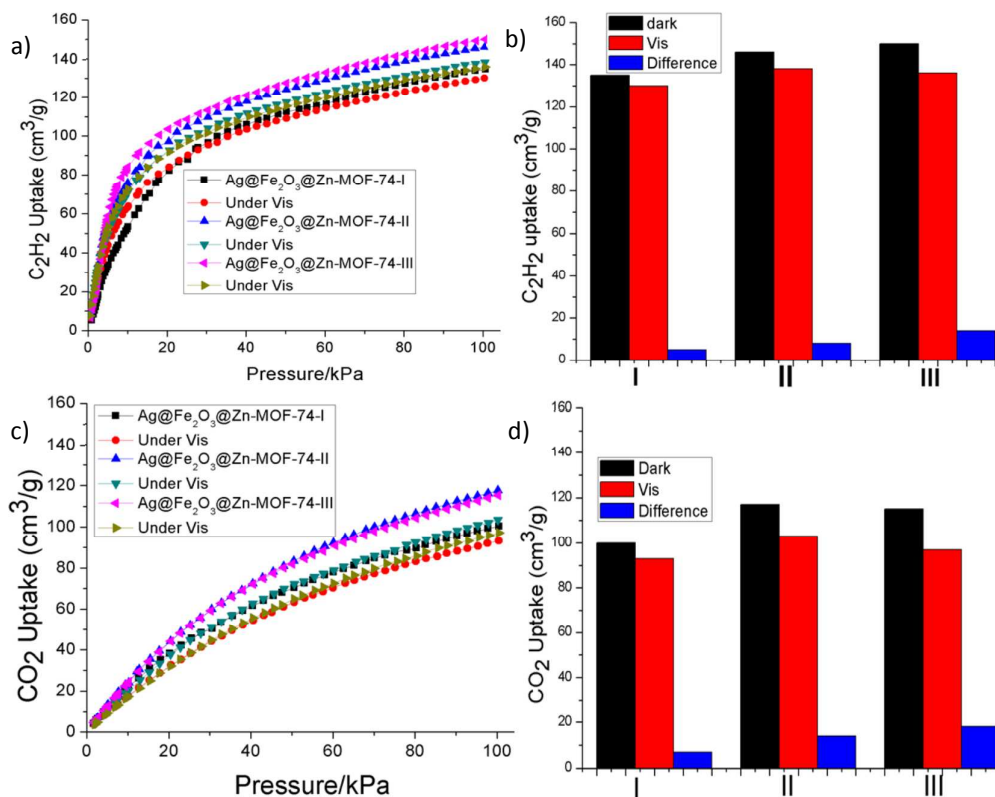


Figure S4. The UV-Vis spectra of Zn-MOF-74, and samples **I**, **II**, and **III** in the solid.



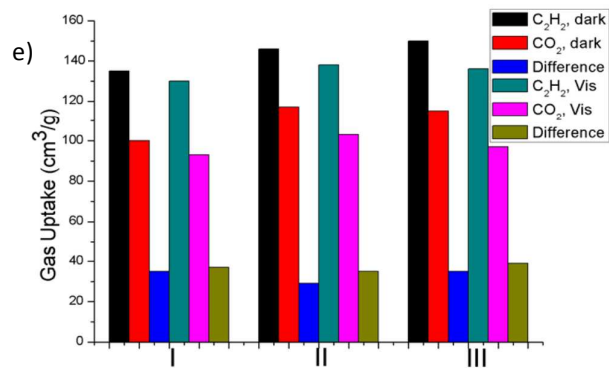


Figure S5. a) The C₂H₂ adsorption isotherms of materials **I**, **II**, and **III** in the dark and Vis; b) histogram of C₂H₂ uptake capacity at 293K and 100 kPa in the dark and Vis, as well as the difference between them; c) the CO₂ adsorption isotherms of materials **I**, **II**, and **III** in the dark and Vis; d) histogram of CO₂ uptake capacity at 293K and 100 kPa in the dark and Vis, as well as the difference between them; e) histogram of both C₂H₂ and CO₂ uptake capacity at 293K and 100 kPa in the dark and Vis, as well as the difference between them.