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## Highly selective adsorption of ethylene over ethane in a MOF featuring the combination of open metal site and $\pi$ -complexation†

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**The introduction of the combination of open metal site (OMS) and  $\pi$ -complexation into MOF has led to very high ethylene–ethane adsorption selectivity at 318 K, as illustrated in the context of MIL-101–Cr–SO<sub>3</sub>Ag. The interactions with ethylene from both OMS and  $\pi$ -complexation in MIL-101–Cr–SO<sub>3</sub>Ag have been investigated by *in situ* IR spectroscopic studies and computational calculations, which suggest that  $\pi$ -complexation contributes dominantly to the high ethylene–ethane adsorption selectivity.**

The separation of ethylene–ethane mixtures represents an important industrial process, and is also considered as one of the most challenging chemical separations in the large scale because of the similar molecular sizes and volatilities between ethylene and ethane.<sup>1</sup> The current technology in industry is dictated by cryogenic distillation, which is cost and energy intensive due to the requirement of high pressure and low temperature.<sup>2</sup> Among several alternative approaches<sup>3,4</sup> under development for energy-efficient ethylene–ethane separation at higher temperatures (at or above room temperature), adsorptive separation using porous solid materials has attracted particular attention.<sup>5</sup>

Due to their high surface areas, tunable pore sizes, and functionalizable pore surfaces as well as the amenability of design and modular nature, metal–organic frameworks (MOFs)<sup>6</sup> have been recently explored as a new type of porous solid materials for hydrocarbon separation,<sup>7</sup> including the separation

of ethylene–ethane mixtures.<sup>8</sup> Extensive efforts have been devoted to the creation of open metal sites (OMSs) in MOFs to enhance the selectivity of ethylene over ethane, due to the stronger interactions of ethylene with OMSs compared with ethane.<sup>8a</sup> Recently, we demonstrated that a Ag(I) ion functionalized porous aromatic framework (PAF) exhibited exceptional ethylene–ethane adsorption selectivity as a result of the formation of  $\pi$ -complexation between ethylene molecules and Ag(I) ions.<sup>9</sup> We speculate that if such a kind of  $\pi$ -complexation can be coupled with OMSs into MOFs, the adsorption selectivity of ethylene over ethane can be further enhanced in MOFs because of the strong interactions with ethylene from both  $\pi$ -complexation and OMSs. In this contribution, we report the introduction of the combination of OMSs and  $\pi$ -complexation into MOF for the first time, as exemplified in the context of MIL-101–Cr–SO<sub>3</sub>Ag, which demonstrates exceptional ethylene–ethane adsorption selectivity at 318 K, surpassing benchmark porous solid materials of zeolites, MOFs and PAFs. The interactions with ethylene from both OMSs and  $\pi$ -complexation have been investigated using *in situ* IR spectroscopic studies and computational calculations.

MIL-101–Cr–SO<sub>3</sub>Ag was afforded *via* Ag(I) ion exchange of the sulphonic acid functionalized MIL-101–Cr (MIL-101–Cr–SO<sub>3</sub>H), which was prepared using the method reported in the literature<sup>10</sup> (Scheme 1). The powder X-ray diffraction studies show that the patterns of MIL-101–Cr–SO<sub>3</sub>Ag are consistent with those of MIL-101–Cr–SO<sub>3</sub>H (Fig. S1, ESI<sup>†</sup>), indicating the maintenance of structural integrity during the Ag(I) exchange process. N<sub>2</sub> gas sorption isotherms collected at 77 K (Fig. S2, ESI<sup>†</sup>) reveal Brunauer–Emmett–Teller (BET) surface areas of 1570 m<sup>2</sup> g<sup>−1</sup> and 1374 m<sup>2</sup> g<sup>−1</sup> for MIL-101–Cr–SO<sub>3</sub>H and MIL-101–Cr–SO<sub>3</sub>Ag, respectively. The decreasing surface area should be presumably due to the introduction of Ag(I) ions. The presence of Ag(I) in MIL-101–Cr–SO<sub>3</sub>Ag was confirmed using X-ray photoelectron spectroscopy (XPS) analysis, which shows the silver signals at a binding energy of 368.8 eV and 374.8 eV (Fig. S3, ESI<sup>†</sup>) corresponding to the peaks of Ag3d<sub>5/2</sub> and Ag3d<sub>3/2</sub>, respectively. Inductively coupled plasma mass spectrometry (ICP-MS) suggests that ~51% SO<sub>3</sub>H were exchanged into SO<sub>3</sub>Ag.

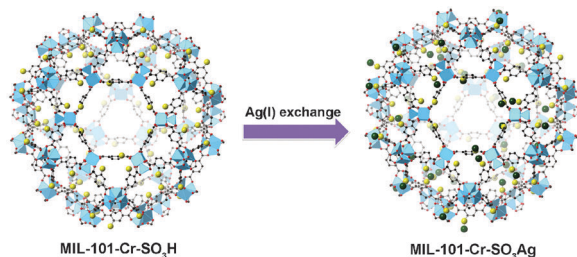
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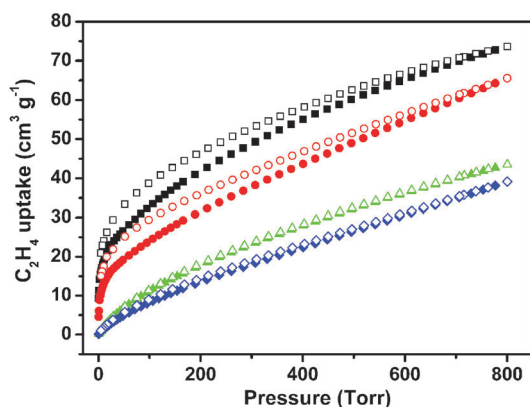
† Electronic supplementary information (ESI) available: Detailed methods for catalyst preparation, measurements, analysis and catalytic process. See DOI: 10.1039/c4cc09774b



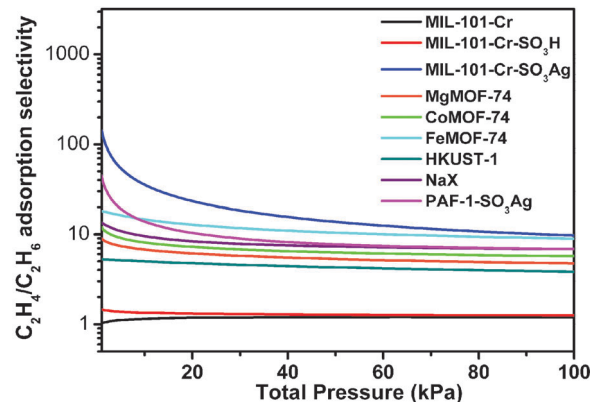
**Scheme 1** Schematic illustration of Ag(I) exchange in MIL-101-Cr-SO<sub>3</sub>H to afford MIL-101-Cr-SO<sub>3</sub>Ag.

The low-pressure ethylene–ethane sorption isotherms were collected at 296 K and 318 K. Compared with the pristine MIL-101-Cr-SO<sub>3</sub>H, the introduction of Ag(I) ion into MIL-101-Cr-SO<sub>3</sub>H results in a significant enhancement of ethylene adsorption capacity despite the decrease in surface area. Under 1 atm pressure, the ethylene uptake amounts increase from 42 cm<sup>3</sup> g<sup>-1</sup> at 296 K and 37 cm<sup>3</sup> g<sup>-1</sup> at 318 K for MIL-101-Cr-SO<sub>3</sub>H to 73 cm<sup>3</sup> g<sup>-1</sup> at 296 K and 63 cm<sup>3</sup> g<sup>-1</sup> at 318 K for MIL-101-Cr-SO<sub>3</sub>Ag (Fig. 1). Interestingly, in contrast to the ethylene adsorption, the uptake amounts of ethane at 296 K and 318 K for two samples are comparable (Fig. S4 and S5, ESI<sup>†</sup>), suggesting that the introduction of Ag(I) ions would not increase the ethane uptake capacity.

Ethylene–ethane adsorption selectivities were calculated using ideal adsorbed solution theory (IAST)<sup>11</sup> for MIL-101-Cr-SO<sub>3</sub>H and MIL-101-Cr-SO<sub>3</sub>Ag (Fig. 2). For an equimolar mixture of ethylene and ethane at 318 K, the adsorption selectivity ( $S_{\text{ads}}$ ) obtained for MIL-101-Cr-SO<sub>3</sub>Ag is 9.7 at 100 kPa, far exceeding that calculated for MIL-101-Cr-SO<sub>3</sub>H ( $S_{\text{ads}} = 1.2$ ). This result suggests the predominant contribution from Ag(I) ion in comparison with the OMS of Cr(III) to the enhancement of ethylene–ethane adsorption selectivity. The ethylene–ethane adsorption selectivity of MIL-101-Cr-SO<sub>3</sub>Ag at 318 K and 100 kPa is also significantly higher than those of the zeolite NaX,<sup>8b</sup> the MOFs<sup>8b</sup> CoMOF-74 [also known as (a.k.a.) Co<sub>2</sub>(dobdc)], MgMOF-74 [a.k.a. Mg<sub>2</sub>(dobdc)], CuBTC [a.k.a. HKUST-1] (Fig. 2), exhibiting ethylene–ethane selectivities of 6.8, 5.7, 4.7, and 3.8, respectively. It slightly surpasses the best



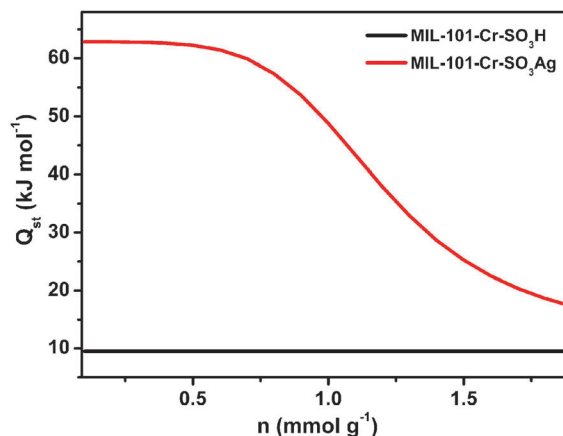
**Fig. 1** C<sub>2</sub>H<sub>4</sub> sorption isotherms of MIL-101-Cr-SO<sub>3</sub>Ag (black: 296 K; red: 318 K) and MIL-101-Cr-SO<sub>3</sub>H (green: 296 K; blue 318 K). Filled: adsorption; unfilled: desorption.



**Fig. 2** Comparison of the IAST calculations for C<sub>2</sub>H<sub>4</sub>–C<sub>2</sub>H<sub>6</sub> adsorption selectivities for MIL-101-Cr-SO<sub>3</sub>Ag with MIL-101-Cr-SO<sub>3</sub>H and other porous materials<sup>10</sup> at 318 K.

performance MOF of FeMOF-74 (a.k.a. Fe<sub>2</sub>(dobdc)) ( $S_{\text{ads}} = 8.9$ ) and PAF of PAF-1-SO<sub>3</sub>Ag<sup>9</sup> ( $S_{\text{ads}} = 6.9$ ). It is worth noting that the higher ethylene–ethane adsorption selectivities of MIL-101-Cr-SO<sub>3</sub>Ag compared to PAF-1-SO<sub>3</sub>Ag indicate the possible cooperative contribution from the OMS of Cr(III) to further boosting the ethylene–ethane adsorption selectivities for MIL-101-Cr-SO<sub>3</sub>Ag.

To provide a better understanding of the exceptional ethylene adsorption properties of MIL-101-Cr-SO<sub>3</sub>Ag, the isosteric heats of adsorption ( $Q_{\text{st}}$ ) were calculated using the Clausius–Clapeyron equation by differentiation of the dual Langmuir–Freundlich fits of the isotherms at two different temperatures,<sup>7c,8b</sup> 296 K and 318 K with  $T$ -dependent parameters. As shown in Fig. 3, close to zero loading, the  $Q_{\text{st}}$  for ethylene in MIL-101-Cr-SO<sub>3</sub>Ag is 63 kJ mol<sup>-1</sup>, remarkably higher than that of MIL-101-Cr-SO<sub>3</sub>H (10 kJ mol<sup>-1</sup>). These results highlight the role of introducing Ag(I) ions in further boosting the interactions with ethylene molecules that stem from the formation of the  $\pi$ -complexation bonding between the d orbital of Ag(I) and the  $\pi^*$  orbital of carbon–carbon double bonds in ethylene.<sup>12</sup> In contrast to the high  $Q_{\text{st}}$  for ethylene, MIL-101-Cr-SO<sub>3</sub>Ag shows a significantly lower  $Q_{\text{st}}$  for ethane with a value of 16 kJ mol<sup>-1</sup> (Fig. S6, ESI<sup>†</sup>);



**Fig. 3** The isosteric heats of adsorption,  $Q_{\text{st}}$  of C<sub>2</sub>H<sub>4</sub> for MIL-101-Cr-SO<sub>3</sub>H, and MIL-101-Cr-SO<sub>3</sub>Ag.

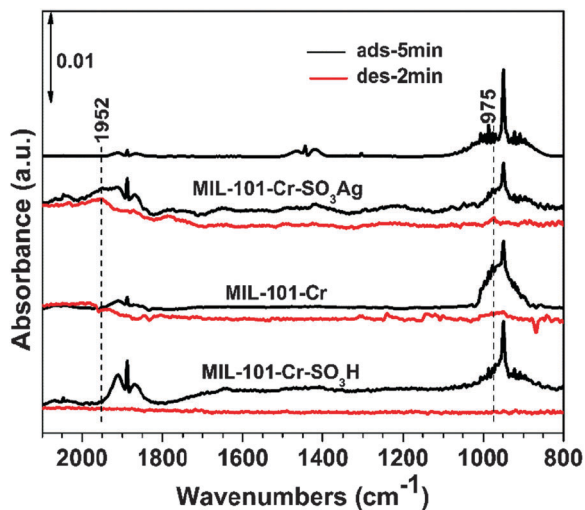


Fig. 4 IR spectra from ethylene adsorption and desorption on MIL-101-Cr, MIL-101-Cr-SO<sub>3</sub>H and MIL-101-Cr-SO<sub>3</sub>Ag at room temperature. IR spectrum from gas phase ethylene is also shown for reference.

thus validating that MIL-101-Cr-SO<sub>3</sub>Ag featuring the combination of OMS and  $\pi$ -complexation can selectively adsorb ethylene over ethane thereby resulting in high ethylene-ethane adsorption selectivities particularly at a relatively high temperature of 318 K.

*In situ* IR measurements of ethylene adsorption at room temperature gave further insight into the nature of interactions between ethylene molecules and the Ag(I) ions in MIL-101-Cr-SO<sub>3</sub>Ag. As shown in Fig. 4, the appearance of IR features at 975 cm<sup>-1</sup> corresponds to the ethylene adsorption on the surface of porous materials. MIL-101-Cr-SO<sub>3</sub>Ag exhibits a stronger ethylene interaction than that of MIL-101-Cr and MIL-101-Cr-SO<sub>3</sub>H, which is evidenced by the complete disappearance of ethylene IR features at 975 cm<sup>-1</sup> for the two compared samples after room temperature desorption in helium purge gas. The extra IR features at 1952 cm<sup>-1</sup> (combination mode of -CH<sub>2</sub> wagging), not observed on the MIL-101-Cr and MIL-101-Cr-SO<sub>3</sub>H, further confirm stronger ethylene interactions on MIL-101-Cr-SO<sub>3</sub>Ag. The blue-shift of the -CH<sub>2</sub> wagging mode can be attributed to the combinative d- $\pi$  and d- $\pi^*$  interaction between Ag and ethylene,<sup>13-16</sup> as a result of the formation of  $\pi$ -complexation between the ethylene and Ag(I) ions in MIL-101-Cr-SO<sub>3</sub>Ag.

To further understand the interactions of ethylene-Ag(I) ion and ethylene-Cr(III) OMS, we used electronic structure calculations to estimate the bond length between ethylene and Ag(I) as well as the bond length between ethylene and Cr(III). A (C<sub>6</sub>H<sub>3</sub>(CO<sub>2</sub>)<sub>2</sub>)SO<sub>3</sub>Ag cluster was considered for this calculation since it is expected that MIL-101-Cr-SO<sub>3</sub>Ag contains this moiety. Starting with the sulfonyl terephthalate unit, a silver ion was placed in proximity to the oxygen atoms of the sulfonate group. The Ag(I) ion was optimized to an energetically favorable position within the cluster. Afterwards, an optimized ethylene molecule was placed in proximity to the Ag(I) ion in the (C<sub>6</sub>H<sub>3</sub>(CO<sub>2</sub>)<sub>2</sub>)SO<sub>3</sub>Ag cluster. The optimization of the C<sub>2</sub>H<sub>4</sub>-Ag(I) interaction was executed using the DFT method. It was observed that the distances between the Ag(I) ion and the

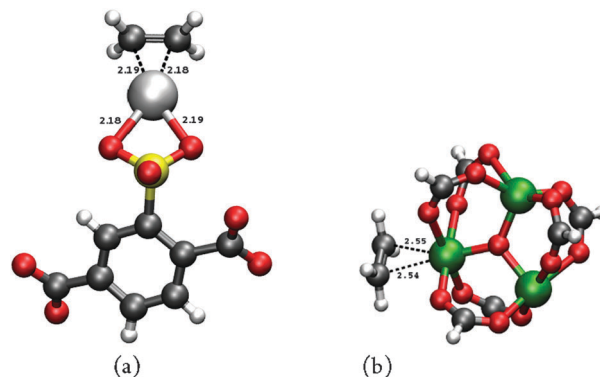


Fig. 5 The optimized position of an ethylene molecule within (a) (C<sub>6</sub>H<sub>3</sub>(CO<sub>2</sub>)<sub>2</sub>)SO<sub>3</sub>Ag and (b) [Cr<sub>3</sub>O(O<sub>2</sub>CH)<sub>6</sub>]<sup>+</sup> clusters.

carbon atoms of the C<sub>2</sub>H<sub>4</sub> molecule were found to be 2.18 and 2.19 Å (Fig. 5a). A similar calculation was performed between the ethylene molecule and the Cr(III) OMSs, and the optimized C<sub>2</sub>H<sub>4</sub>-Cr(III) distances were observed to be 2.54 and 2.55 Å (Fig. 5b). These results suggest that the interactions between ethylene and Ag(I) are much stronger than those between Cr(III) OMSs and they should contribute dominantly to the high adsorption selectivity of MIL-101-Cr-SO<sub>3</sub>Ag for ethylene-ethane.

Given the reasonable accuracy of simulated breakthrough characteristics as validated by recent investigations,<sup>7c,8a,b</sup> we carried out breakthrough simulations for C<sub>2</sub>H<sub>4</sub>-C<sub>2</sub>H<sub>6</sub> mixtures in a fixed bed to demonstrate the feasibility of producing 99.95% + pure C<sub>2</sub>H<sub>4</sub> in a Pressure Swing Adsorption (PSA) operation. The simulated breakthrough curves of Fig. S9 (ESI<sup>†</sup>) show transient breakthrough of an equimolar C<sub>2</sub>H<sub>4</sub>-C<sub>2</sub>H<sub>6</sub> mixture in an adsorber bed packed with MIL-101-Cr-SO<sub>3</sub>Ag. During the adsorption cycle, C<sub>2</sub>H<sub>6</sub> at purities > 99% can be recovered for a certain duration of the adsorption cycle as indicated by the arrow in Fig. S10 (ESI<sup>†</sup>). In addition, ethylene of 99.95% + purity, required as feedstock to the polymerization reactor, can also be recovered during the time interval indicated by the arrow in Fig. S11 (ESI<sup>†</sup>) in the desorption cycle.

In summary, we have demonstrated the introduction of open metal site (OMS) and  $\pi$ -complexation into MOF, affording MIL-101-Cr-SO<sub>3</sub>Ag as an efficient adsorbent for separation of ethylene-ethane. MIL-101-Cr-SO<sub>3</sub>Ag exhibits significantly higher ethylene-ethane adsorption selectivity at 318 K than benchmark zeolites, MOFs and PAFs reported in the literatures. The high ethylene-ethane adsorption selectivity of MIL-101-Cr-SO<sub>3</sub>Ag are mainly attributed to the  $\pi$ -complexation between Ag(I) ions and the double bond of ethylene molecules, which is reflected in the high isosteric heats of adsorption of C<sub>2</sub>H<sub>4</sub> and evidenced using *in situ* IR spectroscopy studies and computational calculations. In addition, the possible cooperative contribution from the OMS of Cr(III) to further enhancing the ethylene-ethane adsorption selectivities have been proved by the higher ethylene-ethane adsorption selectivities of MIL-101-Cr-SO<sub>3</sub>Ag compared to PAF-1-SO<sub>3</sub>Ag. The feasibility of MIL-101-Cr-SO<sub>3</sub>Ag for producing 99.95% + pure C<sub>2</sub>H<sub>4</sub> in a PSA operation has also been demonstrated by breakthrough simulations. Our strategy of introducing dual functional sites into

MOF to afford high ethylene–ethane adsorption selectivities particularly above room temperature paves a new way for developing MOFs for energy-saving ethylene–ethane and other olefin/paraffin separations.

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## Electronic Supplementary Information

### Highly Selective Adsorption of Ethylene over Ethane in a MOF Featuring the Combination of Open Metal Site and $\pi$ -Complexation

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## **Experimental Details**

All Starting materials, reagents, and solvents were purchased from commercial sources (Aldrich, Alfa, Fisher and Acros) and used without further purification.

### **Synthesis of MIL-101-Cr-SO<sub>3</sub>H**

MIL-101-Cr-SO<sub>3</sub>H was synthesized according to the procedures reported the literature.<sup>1</sup>

### **Synthesis of MIL-101-Cr-SO<sub>3</sub>Ag**

To the 15 ml CH<sub>3</sub>CN/H<sub>2</sub>O (1:1) solution, 100 mg MIL-101-Cr-SO<sub>3</sub>H and 100 mg AgBF<sub>4</sub> were added. The mixture was stirred under room temperature for 12 h, and then the solid was collected by filtration followed by washing with CH<sub>3</sub>CN and water. The whole process was performed carefully under dark place. This exchanged process was conducted for three times, and then dried at 110 °C for further test. ICP: Cr: 11%; Ag: 11.6%.

## **Characterization Details**

PXRD data were collected on a Rigaku D/max 2550 Powder X-ray Diffractometer. N<sub>2</sub>, C<sub>2</sub>H<sub>4</sub>, and C<sub>2</sub>H<sub>6</sub> gas sorption isotherms were collected on a Micrometrics ASAP2020 Surface Area Analyzer. Elemental analyses were performed on a Perkin-Elmer 2400 element analyzer. XPS measurements were performed on an ESCALAB 250 X-ray photoelectron spectroscopy, using Mg K $\alpha$  X-ray as the excitation source.

## **In situ IR experiments**

IR spectra of ethylene adsorption were collected using a Thermo Nicolet Nexus 670 spectrometer in diffuse reflectance mode (DRIFTS). The MIL-101-Cr-SO<sub>3</sub>Ag sample, ca. 5 mg, was treated in a DRIFTS cell (HC-900, Pike Technologies) at 423 K in helium (30 mL/min) for 1 hour to removal water and other adsorbates. The sample was then cooled down to room temperature for ethylene adsorption. The adsorption was conducted by flowing 10% ethylene/He (30 mL/min) over the sample for 5 min and then desorption was done in flowing helium. IR spectra were recorded continuously to follow the surface changes during the adsorption and desorption process. All reported IR spectra are difference spectra referenced to

a background spectrum collected at room temperature after pre-treatment but prior to ethylene adsorption.

### **Fitting of pure component isotherms**

The measured experimental isotherm data for C<sub>2</sub>H<sub>4</sub>, and C<sub>2</sub>H<sub>6</sub> on MIL-101-Cr-SO<sub>3</sub>Ag were fitted with the dual-Langmuir-Freundlich isotherm model

$$q = q_{A,s} \frac{b_A p^{V_A}}{1 + b_A p^{V_A}} + q_{B,s} \frac{b_B p^{V_B}}{1 + b_B p^{V_B}} \quad (1)$$

For fitting of the corresponding isotherms for C<sub>2</sub>H<sub>6</sub> on MIL-101-Cr-SO<sub>3</sub>Ag, a simpler 1-site Langmuir-Freundlich model was of adequate accuracy. The fit parameters for C<sub>2</sub>H<sub>4</sub>, and C<sub>2</sub>H<sub>6</sub> are specified in Table S1. Fig. S7 presents a comparison of the experimentally determined component loadings for C<sub>2</sub>H<sub>4</sub>, and C<sub>2</sub>H<sub>6</sub> on MIL-101-Cr-SO<sub>3</sub>Ag at 296 K with the isotherm fits using parameters specified in Table 0. The fits are excellent over the entire range of pressures.

The pure component isotherm data for MIL-101-Cr, and MIL-101-Cr-SO<sub>3</sub>H could be fitted with single site Langmuir-Freundlich model; the fit parameters are provided in Table S2, and Table S3, respectively.

### **Calculations of adsorption selectivity**

The selectivity of preferential adsorption of C<sub>2</sub>H<sub>4</sub> (component 1) over C<sub>2</sub>H<sub>6</sub> (component 2) in a mixture containing 1 and 2, can be formally defined as

$$S_{ads} = \frac{q_1/q_2}{p_1/p_2} \quad (2)$$

In equation (2),  $q_1$  and  $q_2$  are the component loadings of the adsorbed phase in the mixture. The calculations of  $S_{\text{ads}}$  are based on the use of the Ideal Adsorbed Solution Theory (IAST) of Myers and Prausnitz.<sup>2</sup>

### Isosteric heats of adsorption

The isosteric heat of adsorption,  $Q_{\text{st}}$ , were calculated using the Clausius-Clapeyron equation by differentiation of the dual-Langmuir-Freundlich fits of the isotherms at two different temperatures, 296 K and 318 K with  $T$ -dependent parameters.

### Simulations of C<sub>2</sub>H<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> breakthroughs in packed beds

In order to demonstrate the feasibility of producing 99.95%+ pure C<sub>2</sub>H<sub>4</sub> in a Pressure Swing Adsorption (PSA) we carried out breakthrough simulations for C<sub>2</sub>H<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> mixtures in a fixed bed of length  $L$ , packed with MIL-101-Cr-SO<sub>3</sub>Ag that has a framework density  $\rho = 700 \text{ kg/m}^3$ ; see schematic in Fig. S8. The voidage of the fixed bed was chosen  $\varepsilon = 0.75$ .

Assuming plug flow of the binary gas mixture through the fixed bed maintained under isothermal conditions at 296 K, the partial pressures in the gas phase at any position and instant of time are obtained by solving the following set of partial differential equations for each of the species  $i$  in the gas mixture.<sup>3-9</sup>

$$\frac{1}{RT} \frac{\partial p_i(t, z)}{\partial t} = -\frac{1}{RT} \frac{\partial (v(t, z) p_i(t, z))}{\partial z} - \frac{(1-\varepsilon)}{\varepsilon} \rho \frac{\partial \bar{q}_i(t, z)}{\partial t}; \quad i = 1, 2, \dots, n \quad (3)$$

In equation (3),  $t$  is the time,  $z$  is the distance along the adsorber,  $\rho$  is the framework density,  $\varepsilon$  is the bed voidage,  $v$  is the interstitial gas velocity, and  $\bar{q}_i(t, z)$  is the *spatially averaged* molar loading within the crystallites of radius  $r_c$ , monitored at position  $z$ , and at time  $t$ . If the values of intra-crystalline diffusivities are large enough to ensure that



intra-crystalline gradients are absent and the entire crystallite particle can be considered to be in thermodynamic equilibrium with the surrounding bulk gas phase at that time  $t$ , and position  $z$  of the adsorber

$$\bar{q}_i(t, z) = q_i(t, z) \quad (4)$$

The molar loadings  $q_i$  are calculated on the basis of adsorption equilibrium with the bulk gas phase partial pressures  $p_i$  at that position  $z$  and time  $t$ . The adsorption equilibrium can be calculated on the basis of the IAST. After discretization of the fixed bed into 100-200 slices, Equations (3) and Equation (4) need to be solved simultaneously using robust numerical procedures that are described in detail in the published literature.<sup>10</sup> The breakthrough simulation methodology has been rigorously tested and validated using a variety of experimental data on breakthroughs.<sup>10</sup>

The breakthrough characteristics for any component is essentially dictated by the characteristic contact time  $\frac{L}{v} = \frac{L\varepsilon}{u}$  between the crystallites and the surrounding fluid phase. It is common to use the dimensionless time,  $\tau = \frac{tu}{L\varepsilon}$ , obtained by dividing the actual time,  $t$ , by the characteristic time,  $\frac{L\varepsilon}{u}$  when plotting simulated breakthrough curves as has been done in Fig. S9.<sup>10,11</sup>

Let us first consider the adsorption phase of the PSA operations. Fig. S9 shows transient breakthrough of an equimolar  $C_2H_4/C_2H_6$  mixture in an adsorber bed packed with MIL-101-Cr-SO<sub>3</sub>Ag. The inlet gas is maintained at partial pressures  $p_1 = p_2 = 50$  kPa. The more poorly adsorbed saturated alkane breaks through earlier and can be recovered in nearly pure form. From the gas phase concentrations at the exit of the adsorber, we can determine the %  $C_2H_6$ ; this information is presented in Fig. S10. During the adsorption cycle,  $C_2H_6$  at

purities > 99% can be recovered for a certain duration of the adsorption cycle indicated by the arrow in Fig. S10.

Once the entire bed is in equilibrium with the partial pressures  $p_1 = p_2 = 50$  kPa, the desorption, “blowdown” cycle is initiated, by applying a vacuum or purging with inert gas. Fig. S11 shows %C<sub>2</sub>H<sub>4</sub> in the outlet gas of an adsorber bed packed with MIL-101-Cr-SO<sub>3</sub>Ag in the desorption cycle. For production of ethylene as feedstock for polymerization purposes, the required purity level is 99.95%+ can be recovered during the time interval indicated by the arrow in Fig. S11.

## Notation

$b_A$	dual-Langmuir-Freundlich constant for species $i$ at adsorption site A, $\text{Pa}^{-V_i}$
$b_B$	dual-Langmuir-Freundlich constant for species $i$ at adsorption site B, $\text{Pa}^{-V_i}$
$c_i$	molar concentration of species $i$ in gas mixture, $\text{mol m}^{-3}$
$c_{i0}$	molar concentration of species $i$ in gas mixture at inlet to adsorber, $\text{mol m}^{-3}$
$L$	length of packed bed adsorber, m
$p_i$	partial pressure of species $i$ in mixture, Pa
$p_t$	total system pressure, Pa
$q_i$	component molar loading of species $i$ , $\text{mol kg}^{-1}$
$q_{\text{sat},A}$	saturation loading of site A, $\text{mol kg}^{-1}$
$q_{\text{sat},B}$	saturation loading of site B, $\text{mol kg}^{-1}$
$\bar{q}_i(t)$	<i>spatially averaged</i> component molar loading of species $i$ , $\text{mol kg}^{-1}$
$R$	gas constant, $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$
$S_{\text{ads}}$	adsorption selectivity, dimensionless
$t$	time, s
$T$	absolute temperature, K
$u$	superficial gas velocity in packed bed, $\text{m s}^{-1}$
$v$	interstitial gas velocity in packed bed, $\text{m s}^{-1}$
$z$	distance along the adsorber, and along membrane layer, m

### *Greek letters*

$\varepsilon$	voidage of packed bed, dimensionless
$\nu$	exponent in dual-Langmuir-Freundlich isotherm, dimensionless
$\rho$	framework density, $\text{kg m}^{-3}$
$\tau$	time, dimensionless

### *Subscripts*

$i$	referring to component $i$
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A referring to site A

B referring to site B

**Table S1.** Dual-Langmuir-Freundlich fits for C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> at 296 K in MIL-101-Cr-SO<sub>3</sub>Ag.

*T*-dependent fits for 296 K and 318 K isotherm data

$$b_A = b_{A0} \exp\left(\frac{E_A}{RT}\right); \quad b_B = b_{B0} \exp\left(\frac{E_B}{RT}\right)$$

	Site A				Site B			
	$q_{A,\text{sat}}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>\nu_i</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$\nu_A$ dimensionless	$q_{B,\text{sat}}$ mol kg <sup>-1</sup>	$b_{B0}$ Pa <sup>-<math>\nu_i</math></sup>	$E_B$ kJ mol <sup>-1</sup>	$\nu_B$ dimensionless
C <sub>2</sub> H <sub>4</sub>	2.3	6.22×10 <sup>-6</sup>	22	0.35	3.3	4.01×10 <sup>-9</sup>	6	1.46
C <sub>2</sub> H <sub>6</sub>	8.3	7.06×10 <sup>-8</sup>	13.6	0.84				

**Table S2.** Langmuir-Freundlich fits for C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> in MIL-101-Cr.

	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_i</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless
C <sub>2</sub> H <sub>4</sub>	5.2	1.83×10 <sup>-11</sup>	35.4	0.95
C <sub>2</sub> H <sub>6</sub>	7.5	2.47×10 <sup>-7</sup>	10	0.9

**Table S3.** Langmuir-Freundlich fits for C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> in MIL-101-Cr-SO<sub>3</sub>H.

	$q_{A,sat}$ mol kg <sup>-1</sup>	$b_{A0}$ Pa <sup>-<math>v_i</math></sup>	$E_A$ kJ mol <sup>-1</sup>	$v_A$ dimensionless
C <sub>2</sub> H <sub>4</sub>	6.7	1.31×10 <sup>-6</sup>	7.8	0.82
C <sub>2</sub> H <sub>6</sub>	6.3	1.2×10 <sup>-7</sup>	13	0.85

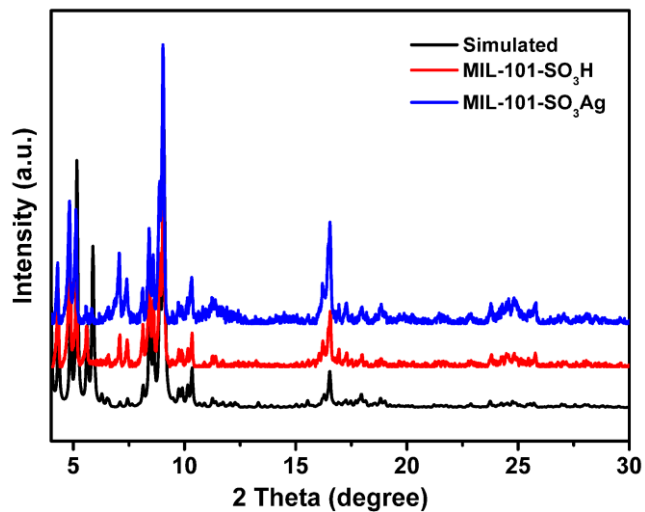
**The investigation of interaction between ethylene and Ag<sup>+</sup> or open metal sites.**

Electronic structure calculations were performed to investigate the interaction between ethylene and Ag<sup>+</sup> ion. A (C<sub>6</sub>H<sub>3</sub>(CO<sub>2</sub>)<sub>2</sub>)SO<sub>3</sub>Ag cluster was considered for this calculation since it is expected that MIL-101-Cr-SO<sub>3</sub>Ag contains this moiety. Starting with the sulfonyl terephthalate unit, a silver ion was placed in proximity to the oxygen atoms of the sulfonate group. The Ag<sup>+</sup> ion was optimized to an energetically favorable position within the cluster. The optimization was performed using density functional theory (DFT) with the well-known B3LYP functional. For this calculation, the 6-31G\* basis set was used for all C, H, O, and S atoms, whereas the aug-cc-pVDZ-PP basis set<sup>12</sup> was used for Ag since a very large basis set was required to treat the inner electrons of this many-electron species. The optimized position for the Ag<sup>+</sup> ion was discovered to be 2.18 Å from one RSO<sub>3</sub><sup>-</sup> oxygen atom and 2.19 Å from another oxygen atom.

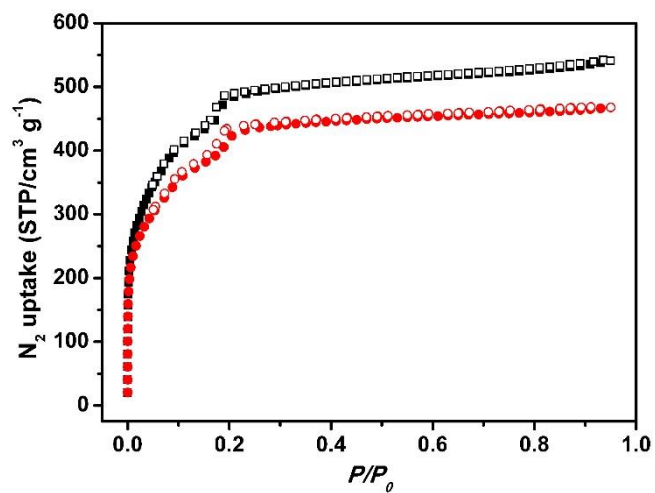
Afterwards, an optimized ethylene molecule was placed in proximity to the Ag<sup>+</sup> ion in the (C<sub>6</sub>H<sub>3</sub>(CO<sub>2</sub>)<sub>2</sub>)SO<sub>3</sub>Ag cluster. The optimization of the C<sub>2</sub>H<sub>4</sub>-Ag<sup>+</sup> interaction was executed

using DFT using the same functional and basis sets for all atoms as described above. It was observed that the  $C_2H_4$  molecule adsorbed closely to the  $Ag^+$  ion in the cluster. The distances between the  $Ag^+$  ion and the carbon atoms of the  $C_2H_4$  molecule were found to be 2.18 and 2.19 Å. These distances are representative of a strong physisorption interaction. Note, the  $C(C_2H_4)-Ag^+$  distances calculated in this work are notably shorter than the distances that were observed for the interaction between a silver ion and the unsaturated carbon atoms of a propylene molecule from previous work.<sup>13</sup>

A similar calculation was performed to examine the interaction between ethylene and an open-metal  $Cr^{3+}$  ion. A  $[Cr_3O(O_2CH)_6]^+$  cluster, taken from the crystal structure of MIL-101-Cr, was used for this calculation. The SBKJC VDZ ECP<sup>14</sup> basis set was assigned to Cr for the calculations. This is a smaller basis set than what was used for Ag since Cr does not have as many electrons as Ag. A  $C_2H_4$  molecule was placed in the vicinity of one of the  $Cr^{3+}$  ions and the molecule was relaxed using the same DFT methods as implemented above. The calculations revealed that the  $C_2H_4$  molecule is further away from the  $Cr^{3+}$  ion as compared to the  $Ag^+$  ion. Indeed, the optimized  $C(C_2H_4)-Cr^{3+}$  distances were observed to be 2.54 and 2.55 Å. This signifies a weaker interaction compared to the aforementioned  $C(C_2H_4)-Ag^+$  distances. All calculations were performed using the NWChem software.<sup>15</sup>

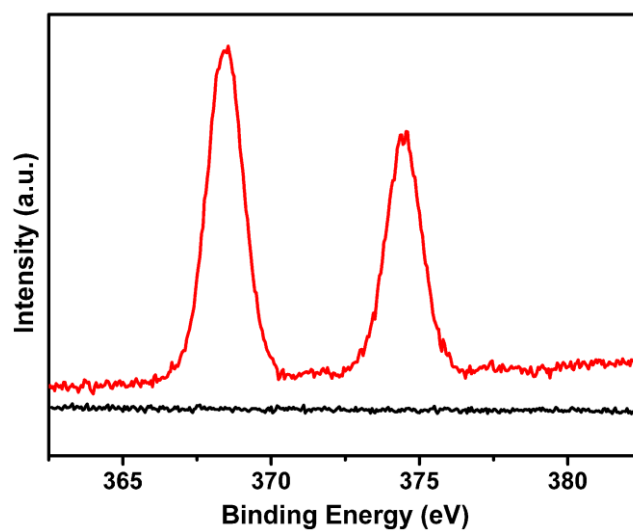


**Fig. S1.** Comparison of XRD of simulated MIL-101-Cr-SO<sub>3</sub>H (black), MIL-101-Cr-SO<sub>3</sub>H (red), and MIL-101-Cr-SO<sub>3</sub>Ag (blue).

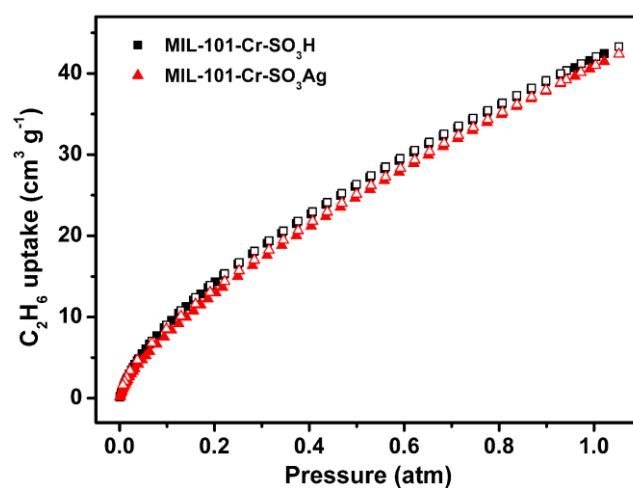


**Fig. S2.** Comparison of N<sub>2</sub> sorption MIL-101-Cr-SO<sub>3</sub>H (black), MIL-101-Cr-SO<sub>3</sub>Ag (red).

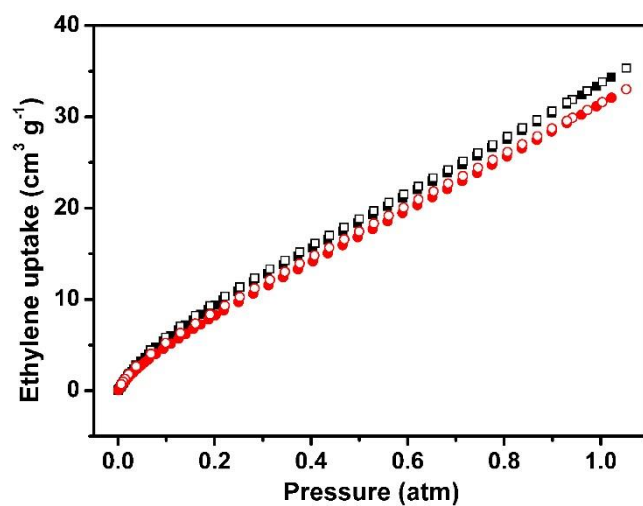




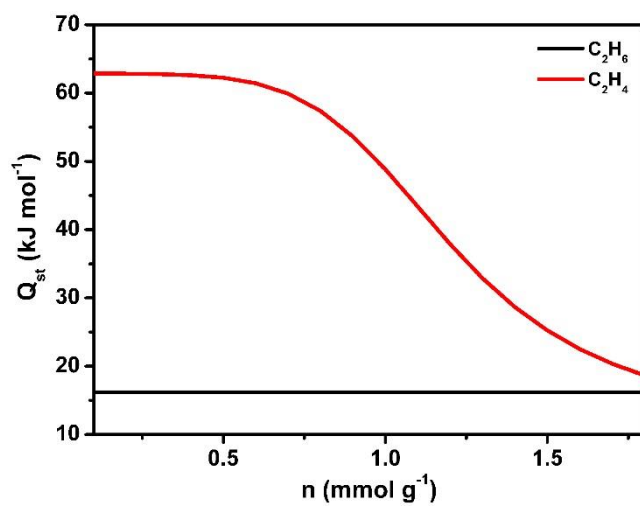
**Fig. S3.** Comparison of Ag(I) XPS of MIL-101-Cr-SO<sub>3</sub>H (black) and MIL-101-Cr-SO<sub>3</sub>Ag (red).



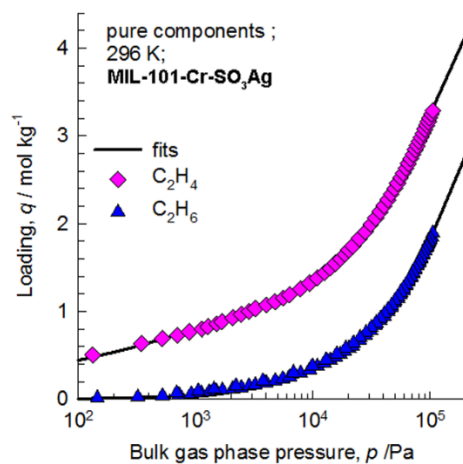
**Fig. S4.** Comparison of ethane sorption isotherms of MIL-101-Cr-SO<sub>3</sub>H (black), and MIL-101-Cr-SO<sub>3</sub>Ag (red) at 296 K.



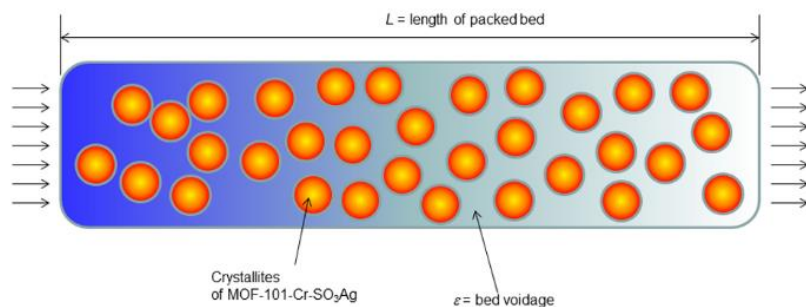
**Fig. S5.** Comparison of ethane sorption isotherms of MIL-101-Cr-SO<sub>3</sub>H (black), and MIL-101-Cr-SO<sub>3</sub>Ag (red) at 318 K.



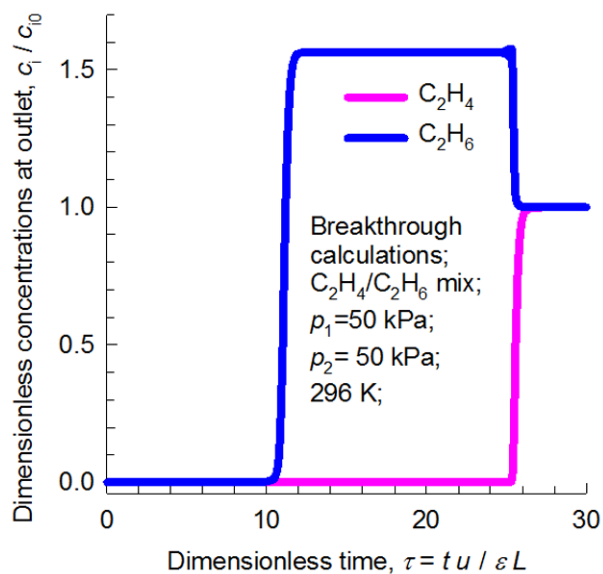
**Fig. S6.** Comparison of isosteric heats of adsorption for ethylene (red) and ethane (black) in MIL-101-Cr-SO<sub>3</sub>Ag.



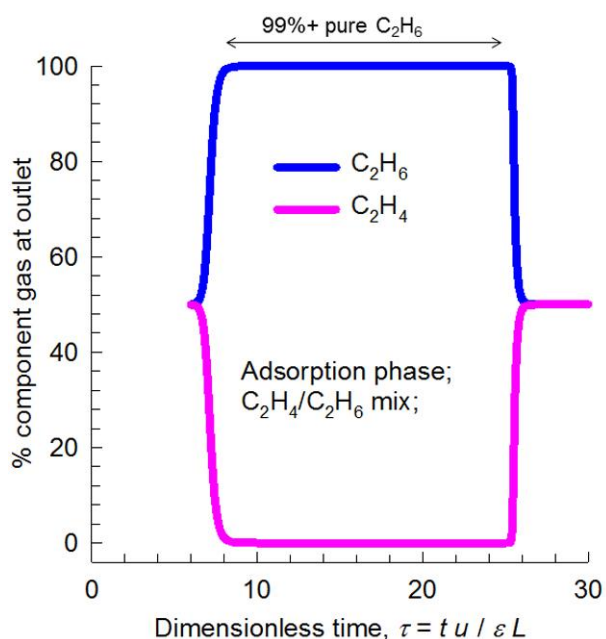
**Fig. S7.** Comparison of the experimentally determined component loadings for  $C_2H_4$ , and  $C_2H_6$  on MIL-101-Cr-SO<sub>3</sub>Ag at 296 K with the isotherm fits using parameters specified in Table S1.



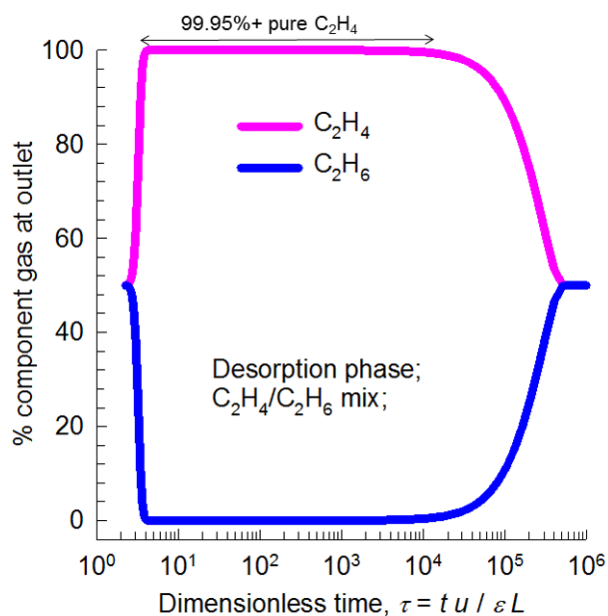
**Fig. S8.** Schematic of a packed bed adsorber. The parameter values used in the simulations presented here are:  $L = 0.12$  m; voidage of bed,  $\varepsilon = 0.75$ ; interstitial gas velocity,  $v = 0.003$  m/s, superficial gas velocity,  $u = 0.00225$  m/s.



**Fig. S9.** Transient breakthrough of an equimolar  $C_2H_4/C_2H_6$  mixture in an adsorber bed packed with MIL-101-Cr- $SO_3Ag$  in the adsorption phase of a PSA operation. The inlet gas is maintained at partial pressures  $p_1 = p_2 = 50$  kPa, at a temperature of 296 K.



**Fig. S10.** %  $C_2H_6$  in the outlet gas of an adsorber bed packed with MIL-101-Cr- $SO_3Ag$  in the adsorption cycle. The inlet gas is maintained at partial pressures  $p_1 = p_2 = 50$  kPa, at a temperature of 296 K.



**Fig. S11.** % C<sub>2</sub>H<sub>4</sub> in the outlet gas of an adsorber bed packed with MIL-101-Cr-SO<sub>3</sub>Ag in the desorption cycle. The contents of the bed, that is equilibrated at partial pressures  $p_1 = p_2 = 50$  kPa, at a temperature of 296 K is purged by inert gas. For the calculations presented in the graph, the inert gas is not included in the calculation of the % compositions.

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